REVISED AERMOD MODELING REPORT

Copper World / Pima County, AZ

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1. EXECUTIVE SUMMARY

Copper World, Inc. (Copper World), a subsidiary of Hudbay Minerals Inc. (Hudbay), is seeking approval of an Arizona Department of Environmental Quality (ADEQ) Air Quality Class II Synthetic Minor Permit for the Copper World Project (Project) in Pima County, Arizona. A Class II Synthetic Minor Source Permit application was submitted to ADEQ on October 21, 2022, along with an air quality modeling report.

The permit application submitted in October 2022 included a detailed development plan for the Copper World Project. Mineral resources will be developed on both the west and east sides of the Santa Rita mountains east of Green Valley, Arizona. This includes a portion of the Rosemont deposit located on the east side of the Santa Rita mountains. All processing facilities associated with the Project are proposed to occur on the west side of the mountains near Helvetia, Arizona. The Copper World Project operations will occur entirely on land privately owned and controlled by Copper World, Inc.

This revised air quality modeling report documents the methodology and results of the air quality impact analyses prepared in support of the Class II Synthetic Minor Source Permit application. This modeling analysis was developed following applicable portions of the ADEQ guidance document: Air Quality Modeling Guidelines for Arizona Air Quality Permits, November 2019 (ADEQ Guidance) and the Environmental Protection Agency (EPA) Guideline on Air Quality Models (Guidelines, 40 CFR Part 51, Appendix W, May 2017) as well as in direct consultation with ADEQ.

Revisions to the June 2024 modeling analyses presented in this July 2024 report are summarized as follows:

- Replacement of the on-site May 2023-April 2024 CWP Met-2 Station meteorological data processed with the 'wet' surface moisture conditions and partial turbulence data (sigma-theta) with the on-site May 2023-April 2024 CWP Met-2 Station meteorological data processed with the 'average' surface moisture conditions and removal of sigma-theta data.

Previous revisions to modeling analyses submitted to ADEQ in June 2024 include:

- Replacement of the 2016-2020 Tucson airport meteorological data with the on-site May 2023-April 2024 CWP Met-2 Station meteorological data.
- An updated emission inventory and modeled emission rates for all modeled years and both sets of model runs (CWP Met-2 Station meteorological data and East Side on-site meteorological data) to reflect an update to emission factors which use wind speed data in the emission factor calculation.
  - The emission factors were previously calculated using the 2016-2020 Tucson airport wind speed data; the emission factors are now calculated using the on-site CWP Met-2 Station wind speed data.
- Update of all model runs to the most recent version of AERMOD (version 23132).
- Compilation of all receptors (near grid and 10K grid) into single model runs.

Previous revisions to modeling analyses submitted to ADEQ in March 2024 include:

- An updated emission inventory and modeled emission rates for all modeled years reflecting the removal of tailpipe emissions.
- Revised $PM_{2.5}$ background concentrations calculated from 2019-2021 monitored data.
- Removal of dry depletion from particulate model runs unless needed for NAAQS compliance.
- Revised MERPS analysis to reflect project impacts below the ozone significant impact level (SIL).

Previous revisions to modeling analysis submitted to ADEQ in January 2024 include:

- An updated emission inventory and modeled emission rates for Year 2 reflecting the following:
  - Correction to the emission factor used to calculate particulate emissions from the CAT 6060 mining shovel. The CAT 6060 will have a Tier 4 engine; the previous calculation incorrectly used the Tier 1 emission factor for particulate; it has been corrected to use the Tier 4 emission factor.
  - Correction to the calculation of annual $PM_{2.5}$ emissions for the Santa Rita Rd model area sources. The previous calculation used the maximum lb/hr emission rate instead of converting the ton/yr emission rate to lb/hr. It has been corrected to use the ton/yr converted to lb/hr emission rate.
- An updated emission inventory and modeled emission rates for Years 8 and 14 reflecting the following:
  - Correction to the emission factor used to calculate particulate emissions from the CAT 6060 mining shovel. The CAT 6060 will have a Tier 4 engine; the previous calculation incorrectly used the Tier 1 emission factor for particulate; it has been corrected to use the Tier 4 emission factor.
- Updated Meteorological Sensitivity analysis evaluating the impact of the following meteorological variables on Model Year 8 model results: ambient air temperature, cloud cover, and surface characteristics (albedo, bowen ratio and surface roughness), to reflect the following:
  - Correction to the emission factor used to calculate particulate emissions from the CAT 6060 mining shovel. The CAT 6060 will have a Tier 4 engine; the previous calculation incorrectly used the Tier 1 emission factor for particulate; it has been corrected to use the Tier 4 emission factor.

Previous revisions to the modeling analysis submitted to ADEQ in October 2023 include:

- An updated emission inventory and modeled emission rates for Year 2 reflecting the maximum mining rate, as described in **Sections 6 and 7**.
- An updated emission inventory and modeled emission rates for Year 14 reflecting the maximum mining rate, as described in **Sections 6 and 7**.
- A new emission inventory and model for Year 8 reflecting the operational characteristics and maximum mining rate for Year 8, as described in Sections **6 and 7**.
- Use of mine plan derived short-term maximum emission rates for pollutants with 24-hr or shorter averaging periods, as described in **Section 7.2**. This applies to Year 2, Year 8, and Year 14.
- Revised modeling methodologies to account for volume source exclusion zones at waste rock facilities and tailings storage facilities (TSFs), as described in **Section 6.7.2**.
- Revision to the modeled haul road emissions to ensure that the haul road lengths used for emissions calculations are consistent with the modeled haul road lengths and the tailpipe emissions associated with haul trucks are appropriately allocated across the haul roads, pits and waste rock facilities.
- Revision to the starting point of 'Combined Haul Road 1-2' in Model Year 8 to the intersection of the 'BT Haul Road' and 'Combined Haul Road 7-8'.
- Revised methodology for modeling blasting emissions such that the area of the blasting volume sources is consistent with the surface areas used to develop the emissions calculations.
- Revised methodology for modeling blasting emissions such that blasting volume sources are concentrated into a single area within the pit when demonstrating compliance with the NAAQS.
- Revised modeling accounting for emissions from delivery and product shipment associated with the Copper World Project on Santa Rita Road for all model years and description of modeling methodology to account for volume source exclusion zone along the roadway, as described in **Section 6.7.3**.
- Ambient air impact assessments for Years 8 and 14 using on-site meteorological data collected for the Rosemont Copper Project to evaluate the impact of the subset operations east of the ridgeline of the Santa Rita Mountains, as described in **Section 5.3.2 and Section 4.1.1.1**.
- Meteorological Sensitivity analysis evaluating the impact of the following meteorological variables on Model Year 8 model results: ambient air temperature, cloud cover, and surface characteristics (albedo, bowen ratio and surface roughness), as described in **Section 5.3.1 and Table 5-1**.

- Revision to the ambient air boundary to include a single additional parcel in the footprint of the Rosemont Pit.

2. INTRODUCTION

2.1 Facility Description

Operations associated with the Copper World Project include: (a) open-pit mining from six (6) pit areas that will include drilling, blasting, loading, stockpiling, and hauling of sulfide and oxide ore and development rock (waste rock); (b) primary crushing and stockpiling of sulfide and oxide crushed ore; (c) stockpile reclaim; (d) milling and flotation of sulfide ore; (e) heap leaching of oxide ore; (f) tailings thickening and placement in a "conventional" storage facility; (g) concentrate leaching and precious metals recovery; (h) optional copper concentrate dewatering and preparation for shipment; (i) moly concentrate drying and bagging, (j) solvent extraction and electro-winning (SX-EW) and copper cathode production from copper concentrate and oxide leach circuits; and (k) a sulfuric acid plant.

Secondary processes include: (a) fuel burning equipment; (b) reagent systems; (c) storage tanks; (d) organic reagent use; (e) an analytical metallurgical laboratory; and (f) the use of mobile support vehicles.

The production schedule was developed from detailed mining sequence plans. The mine sequencing provides detailed information through year 15. The annual maximum mining rate for Sulfide Ore is 21.9 million tons per year (M TPY) starting in Year 5 and continuing until the end of Year 14. The maximum yearly movement of waste rock is 51.1M TPY occurring in Year 10. Additionally, the mining and hauling of Oxide Ore peaks in Years 6-8 at 16.425M TPY. Although ore and waste rock quantities vary annually, the primary contributor to offsite emissions impacts are directly linked to the distance traveled by the mine vehicle fleet. The vehicle miles traveled (VMTs) for the mine fleet increases to a maximum rate (in-pit and out of pit) in Year 14 and a maximum rate of out of pit VMT concurrent with the maximum mining rate in Year 8 of the mine life. As a result, these years represent the maximum mine emissions profile and maximum potential for adverse ambient impacts.

Although Year 14 and Year 8 represent the maximum potential for overall ambient impacts, they also represent a larger geographic area of operational development. As a result, a further assessment of impacts was generated for review during the first five years of Project development. Although annual mining rates would be lower during this time frame, operations would be geographically constrained to multiple pits on the west and central portions of the mine property. Based on a review of the geographic location of proposed mine activities, and the maximum mining rates, it was determined that Year 2 would represent the maximum potential for impacts during the early mine development period.

During all periods of the mine development, ore mining will occur via conventional open-pit mining techniques including drilling, blasting, loading, hauling, and unloading. Waste rock will be transported by haul trucks for placement in waste rock storage areas (termed waste rock facility, or WRF). Upon arrival at the processing plant area (Plant Site), sulfide ore will be crushed and transferred via conveyor to the mill for further processing. Oxide ore will either be crushed and conveyed to the heap leach pad (HLP) or directly trucked and placed on the HLP. Temporary ore stockpiling at the processing area may also occur to provide stability to the processing plant. The molybdenum concentrate from the milling and flotation operation will be shipped off-site for further processing. The copper concentrate will be processed onsite in a concentrate leach circuit, with the recovery of copper occurring in a Solvent Extraction and Electrowinning (SX-EW) plant. However, modeling has also assumed concurrent conventional handling (dewatering and shipment) of copper concentrate to ensure a conservative assessment.

2.2 Site Description

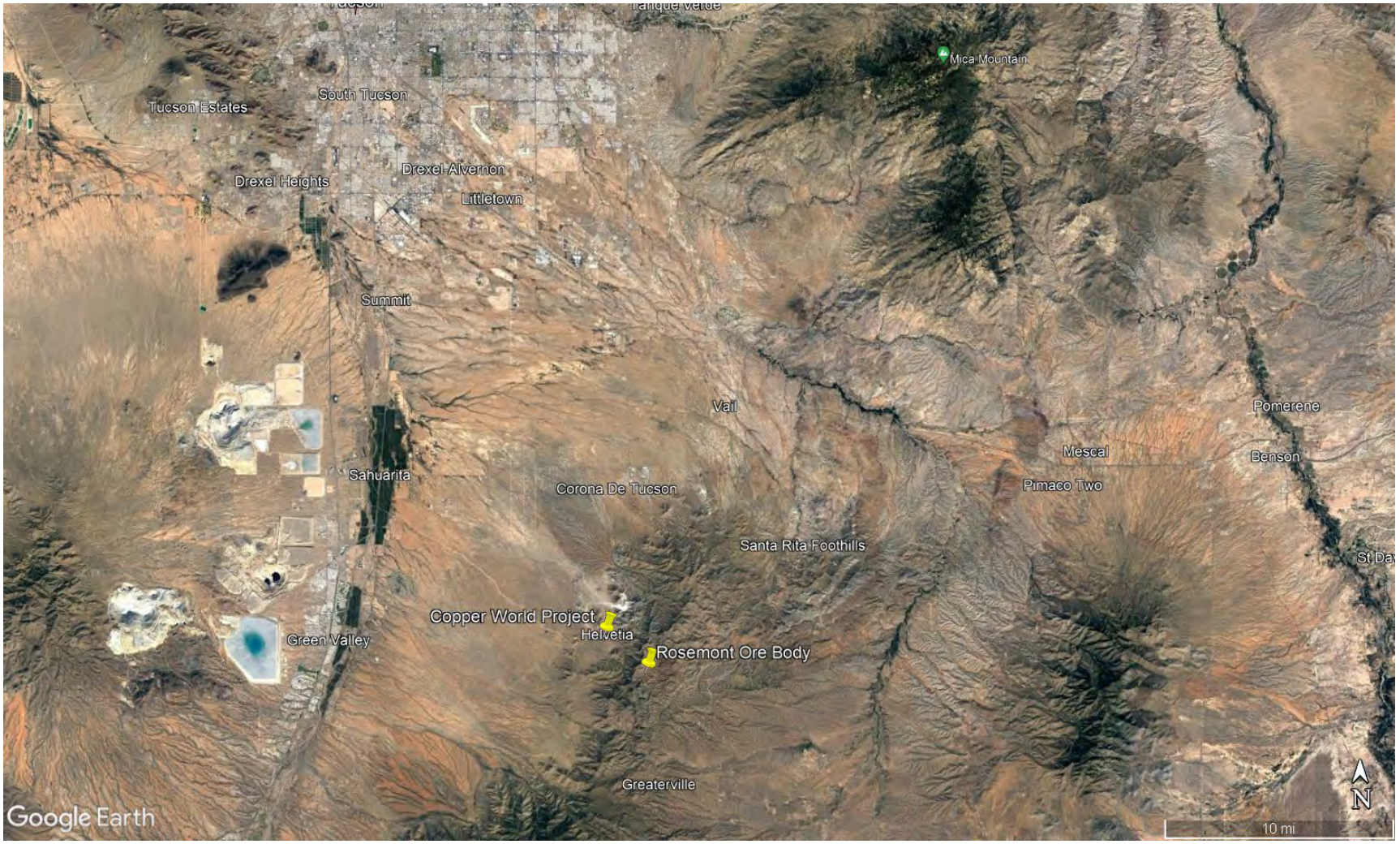
The Copper World Project will be located in Pima County, approximately 28 miles southeast of Tucson, Arizona as shown in **Figure 2-1**. Regionally, the facility location is in the Sonoran Desert Section of the Basin and Range Physiographic Province, which is characterized by northerly trending, fault block mountains separated by broad, down-faulted valleys (see **Figure 2-1**). Elevations in the Copper World Project area range from about 3,600 to over 6,300 feet above mean sea level (amsl). Detailed mine layout figures for Year 2, Year 8 and Year 14 have been included in **Appendix A** for review.

The Year 14 mine layout depicts the primary mine pit (Rosemont Pit ore deposit) located on the east side of the Santa Rita Mountains and the proposed Copper World Project Processing Facility, heap leach and tailings located on the west side, including the location of hauling and WRF features. Additionally, the Year 14 layout includes backfilling of the Broadtop Butte Pit with waste rock from the Rosemont Pit. The Broadtop Butte Pit is located between the Rosemont Pit and the Copper World Pit.

For Year 8, the mine layouts depict two primary mine pits (Broadtop Butte Pit located west of the Santa Rita Mountains and Rosemont Pit located east of the Santa Rita Mountains), as well as two WRF locations, west of the Santa Rita Mountains. The WRF locations for Year 8 are located at the backfill locations of the Heavy Weight and Copper World pits. The layouts also include the haul road, heap leach, tailings and processing plant locations.

The Year 2 mine layout depicts the smaller early mine life pits (Peach, Elgin, Heavy Weight, and Copper World ore deposits), the processing plant, tailings, heap leach, haul road, and WRF locations.

Figure 2-1. General Location Map



3. REGULATORY STATUS

3.1 Source Designation

The Copper World Project development will be a non-categorical stationary source. The potential to emit of criteria pollutants from the facility will be below the New Source Review major source threshold of 250 tons/year. Therefore, the facility will not be subject to Prevention of Significant Deterioration (PSD) regulations. Additionally, the potential to emit hazardous air pollutants (HAPs) will be less than 10 tons/year for any individual (HAP), and less than 25 tons/year for all HAPs combined (fugitive and non-fugitive sources). Therefore, the facility will not be a major HAP source. The potential to emit criteria pollutants from the facility will also be less than the Title V source threshold of 100 tons per year.

The facility includes a categorical source (nested source) associated with a Sulfuric Acid Plant. The emissions for this nested source and associated processes (including fugitives) are required to be compared to a major source threshold of 100 tons per year. The emissions associated with the nested sources do not exceed the major source threshold. Consequently, the facility is proposed to operate under a Class II Permit issued by ADEQ. Proposed new facilities will exceed the Arizona permitting exemption thresholds; therefore, minor new source review (minor NSR) under A.A.C. R18-2-334 is required. Copper World is therefore submitting this modeling, demonstrating compliance with R18-2-334.

3.2 Area Classifications

The Project area is classified as "attainment" (meeting national standards) or unclassifiable/attainment for particulate matter less than 10 microns nominal aerodynamic diameter (PM_{10}), particulate matter less than 2.5 microns nominal aerodynamic diameter ($PM_{2.5}$), carbon monoxide (CO), sulfur dioxide (SO_2), nitrogen dioxide (NO_2), Lead (Pb) and ozone (O_3) (see 40 CFR Part 81.303).

3.3 Baseline Area

The Copper World Project is located within the Pima Intrastate Air Quality Control Region (AQCR), which encompasses Pima County. This AQCR represents the "baseline area" for PSD purposes. The Project, however, will not be subject to PSD regulations.

Although the Copper World Project is located in Pima County and would normally fall within the permitting jurisdiction of the Pima County Department of Environmental Quality, on August 1, 2022, the ADEQ asserted jurisdiction over the Copper World Project pursuant to A.R.S. 49-402. Accordingly, this application addressed ADEQ rules and guidance in addition to Pima County State Implementation Plan requirements.

4. AMBIENT DATA REQUIREMENTS

4.1 Background Concentrations

Criteria pollutants for which background concentrations (and dispersion modeling) were considered for the Copper World Project are PM_{10}, $PM_{2.5}$, NO_2, CO, and SO_2.[1] Because Copper World Project operations are primarily located on the west side of the Santa Rita mountains, a review of appropriate monitors was completed to assess background concentrations that are representative of the conditions that will occur at the location of maximum emissions impacts from the Project.

4.1.1 PM_{10}

Trinity Consultants reviewed PM_{10} data from all representative monitors within approximately 100km of the Copper World Project area from EPA's Air Quality System (AQS) database. Trinity Consultants considers the EPA AQS database a quality-assured data source for the analysis. The monitoring represents data collection on various scales, which provides a comprehensive picture of PM_{10} levels in the Tucson area. All of the monitors were established before 2019 and are currently monitoring PM_{10}. Monitoring data from the most recent three-year period (calendar year 2019-2021) were reviewed for the assessment of background.

Due to the proximity to the Copper World Project site and the monitor's designation as a "regional" monitor, the Corona De Tucson monitor was selected for the assessment of background for the Project. All of the Project's stationary emissions sources, as well as the Corona De Tucson monitor, are located on the west side of the Santa Rita Mountains. The monitor is located approximately 16.5 km from the Copper World Project stationary emissions sources.

In order to accurately assess the time-varying maximum background concentrations, maximum monthly 24-hr PM_{10} values were determined for each month and year from January 2019 to December 2021 (the three most recent full calendar years).[2] The calculated values are included in **Table 4-1**.

Upon detailed review of the maximum monthly PM_{10} concentrations, it was determined that the data included concentrations that were influenced by natural high wind dust events that were eligible for removal using the guidelines included in the Technical Criteria Documents for Determination of Natural and Exceptional Events published on May 31, 2000, February 10, 2005 and December 12, 2005. A detailed analysis of the natural events concluded that seven data points should be removed from the assessment of background due to the influence of natural high wind dust events. The calculation of monthly backgrounds, and a detailed analysis of the natural event removal from the background concentrations, have been included in **Appendix B**. The removal of the seven data points results in replacement of the monthly background with the highest monthly value for a given month from one of the other years that was not influenced by a natural event. **Table 4-1** identifies (highlighted in yellow) the monthly maximums removed due to natural high wind dust events. The highest monthly value from the remaining years was used to assess the background concentration. The subsequent monthly PM_{10} background is included in the far-right column of **Table 4-1**.

[1] Lead background and dispersion modeing were not triggered for review based on the limited potential for lead emissions from the Project.

[2] This methodology was approved in consultation with ADEQ in preparation for the Project.

Table 4-1. Corona De Tucson Maximum Monthly 24-Hr PM_{10} Concentrations (µg/m³) Natural Event Removal Highlighted – Copper World Project

Month	2019	2020	2021	Post Natural Event Removal Monthly Maximum
January	13	19	63	19
February	11	40	24	40
March	32	24	32	32
April	40	21	60	40
May	31	29	21	31
June	24	29	40	40
July	24	28	52	28
August	28	39	16	39
September	14	53	32	53
October	58	64	30	30
November	56	61	39	39
December	17	30	27	30

4.1.1.1 PM_{10} Background – East of Santa Rita Mountains

For the assessment of particulate emissions generating processes located east of the ridgeline of the Santa Rita Mountains, a separate PM_{10} background concentration was utilized to characterize background conditions. PM_{10} measurements were completed east of the Santa Rita Mountain from June 2006 until June 2009. The monitoring program yielded a little over twelve quarters of background concentration data.

As required by the November 9, 2005 Revision to the Air Quality Models (40 CFR 51), the 24-hr PM_{10} background concentration was based on the average of the highest 24-hr concentrations recorded for each year. With respect to determination of this value, ambient PM_{10} monitoring commenced at the start of the 3rd quarter of 2006. Annual time periods are thus considered to represent the following time period: July of one year to June of the following year. A listing of the highest and second highest concentrations for the three-year period is tabulated in **Table 4-2**.

Table 4-2. PM_{10} Monitoring Results – East Side of Santa Rita Mountains

Year	Highest Concentration (µg/m³)	2nd Highest Concentration (µg/m³)
July 2006 – June 2007	71.3	27.0
July 2007 – June 2008	40.3	28.2
July 2008 – June 2009	31.6	21.2

The large difference between the highest measured value (71.3 µg/m³) and the second highest value (40.3 µg/m³) appears anomalous. Consequently, a statistical analysis was conducted on all data to determine its probability of occurrence. This documentation has been previously submitted to ADEQ for review and approval. The analysis indicates the probability of occurrence of the 71. µg/m³ is 5.5E-11. This low probability indicates that the concentration of 71.3 µg/m³ is an outlier to the distribution and should not be

used as a single value for setting the background concentration as it cannot be expected to recur. The value of 71.3 µg/m^3 was, however, included in the calculation of an averaged background concentration, resulting in an average 24-hr PM_{10} background value of 47.7 µg/m^3 which was used for the assessment of particulate impacts for those emissions sources located east of the Santa Rita Mountains.

4.1.2 NO_2

Nitrogen Dioxide, NO_2, is formed by the oxidation of nitric oxide (NO), which is a byproduct of combustion. The NO_2 monitoring sites in Arizona are located in urban areas (Phoenix and Tucson) and near major coal-fired electrical power plants (Springerville, Page, and Bullhead City). There are no monitoring sites in the immediate vicinity of the proposed Copper World Project. ADEQ previously operated a rural background NO_2 monitor at Alamo Lake State Park. This monitor was not directly impacted by urban areas or near field emissions sources beyond minor vehicle traffic and outboard motorboats. As a result, this monitor is representative of the proposed Copper World Project site. ADEQ recommended a NO_2 background concentration of 2.6 µg/m^3 which is the highest annual concentration based on 2014-2016 data from the Alamo Lake monitor. This value was used as the annual background NO_2 concentration. For the 1-hr NO_2 concentration, the highest recorded background concentration at the Alamo Lake site, measured during a three-year monitoring program (2014-2016), is 26.3 µg/m^3. This value was used as the 1-hr background NO_2 concentration.

Communication surrounding the background NO_2 selection with ADEQ is included in **Appendix C**.

4.1.3 CO

Carbon Monoxide, CO, is produced by the incomplete combustion of fuels with anthropogenic activities (automobiles, construction equipment, lawn and garden equipment, commercial and residential heating, etc.) and represents a major source of emissions. Consequently, the CO monitoring sites in Arizona are located exclusively in urban areas (Phoenix, Tucson, and Casa Grande). Thus, there are no representative monitoring stations to determine background CO concentrations at the Copper World Project site.

For modeling, ADEQ recommended using the EPA 2021 Design Value Report (https://www.epa.gov/air-trends/air-quality-design-values) for the Children's Park Ncore monitor for both 1-hr and 8-hr CO background concentrations. Therefore, values of 920 µg/m^3 and 575 µg/m^3 were used as the 1-hr and 8-hr background CO concentrations, respectively, for the Project.

Communication surrounding the background CO selection with ADEQ is included in **Appendix C**.

4.1.4 SO_2

Sulfur dioxide, SO_2, emissions from the Copper World Project operations will be produced from blasting operations and the sulfuric acid plant. Combustion of ultra-low sulfur diesel fuel in stationary engines and mobile vehicles will also produce SO_2. For modeling, ADEQ recommended using the EPA 2021 Design Value Report (https://www.epa.gov/air-trends/air-quality-design-values) and a value of 2.6 µg/m^3 for the Children's Park Ncore monitor for the 1-hr SO_2 background concentration. For the 3-hr SO_2 background concentration, ADEQ recommended using a value of 3.4 µg/m^3, which is the highest 3-hr average concentration from 2019-2021 from the Children's Park Ncore monitor.

Communication surrounding the background SO_2 selection with ADEQ is included in **Appendix C**.

4.1.5 $PM_{2.5}$

In the absence of any representative $PM_{2.5}$ monitoring station in the close vicinity of the Copper World Project site, ADEQ recommended using data from the Saguaro East National Park. Therefore, the background concentrations for the impact analysis are based on the 2019-2021 aerosol data from the Saguaro East National Park IMPROVE site. The 24-hr and annual average background $PM_{2.5}$ concentrations of 9.1 $\mu g/m^3$ and 3.9 $\mu g/m^3$, respectively, were calculated and utilized. The data analysis used to calculate these $PM_{2.5}$ values is included in **Appendix D.**

4.1.6 O_3 for Tier III 1-Hr NO_2 Processing and Assessment of Secondary O_3 Formation

Hourly background ozone data for the period May 2023 through April 2024 from the State and Local Air Monitoring Stations (SLAMS) Green Valley monitoring site was used (to coincide with the meteorological data period that was used for the dispersion modeling and discussed in **Section 5.3**). Based on mid-latitude westerly synoptic patterns, locations west of the proposed Copper World facility are more likely to represent "up-wind" background conditions; therefore, the Green Valley site data is the most representative of the conditions at the Copper World Project site. The data analysis utilized to calculate these O_3 values is included in **Appendix D.**

5. TOPOGRAPHY, CLIMATOLOGY AND METEOROLOGY

5.1 Regional Topography

The Copper World Project will be located in the Santa Rita Mountains which trend northeast to southwest, with elevations at the site ranging from about 3,600 feet to over 6,300 feet amsl (**Figure 2-1**). To the west of the mountains lies the broad Santa Cruz River Valley and to the east lies Davidson Canyon and Rillito Valley, bisected by Cienega Creek.

5.2 Regional Climatology

The climate of the area is semi-arid with precipitation varying with elevation and season. The 30-year normal (1971 to 2000) annual average precipitation for the Santa Rita Experimental Range station, located to the west of the Project site and the Santa Rita Mountain Range, is 23.41 inches (Western Regional Climate Center). Over this 30-year period, nearly half of the precipitation occurred in the months associated with the Arizona monsoon: July, August, and September. The least amount of precipitation occurred during the months of April, May, and June.

Temperatures regionally are moderate to extreme, with maximums and minimums also varying with elevation. The 30-year normal average monthly maximum temperatures at the Santa Rite Experimental Range station ranged from a low of 60.4 °F in January to a high of 93.3 °F in June. Average monthly minimum temperatures ranged from a low of 37.5 °F in December and January to a high of 66.8 °F in July.

5.3 Meteorological Data

5.3.1 Modeling Meteorological Data – Copper World Project

40 CFR Part 51, Appendix W at section 8.4 discusses the selection of "Meteorological Input Data". Subpart (b) dictates that:

> *"The meteorological data used as input to a dispersion model should be selected on the basis of spatial and climatological (temporal) representativeness as well as the ability of the individual parameters selected to characterize the transport and dispersion conditions in the area of concern. The representativeness of the measured data is dependent on numerous factors including, but not limited to: (1) The proximity of the meteorological monitoring site to the area under consideration; (2) the complexity of the terrain; (3) the exposure of the meteorological monitoring site; and (4) the period of time during which data are collected."*

It further clarifies at subpart (c) that:

> *"The meteorological data should be adequately representative and may be site specific data, data from a nearby National Weather Service (NWS) or comparable station, or prognostic meteorological data."*

Site-specific meteorological data has been collected west of the Santa Rita Mountains, the "area of concern" for impacts associated with the Copper World Project from the on-site CWP Met-2 Station meteorological station for the period of May 2023 through April 2024.

The on-site data were processed using AERMET version v23132. Surface characteristics were processed using AERSURFACE (v20060). Data processing was completed by ADEQ and the AERMET processing files were used by Trinity in the modeling analyses as provided by ADEQ.

5.3.2 Modeling Meteorological Data – Copper World Project – Activities East of The Ridgeline of The Santa Rita Mountains

In order to assess the pollutant transport conditions that occur east of the Santa Rita Mountains, modeling analyses of sources which are proposed to occur east of the primary ridgeline of the Santa Rita Mountains were modeled utilizing meteorological data acquired during onsite monitoring that occurred from March 2007-February 2009. These data were previously reviewed by ADEQ and approved for use in ADEQ permitting actions.

Based on revisions to the EPA meteorological pre-processor AERMET, ADEQ provided model ready meteorological files based on a re-processing of these onsite data using AERMET Version 21112. AERMET has subsequently been revised by EPA (Version 23132). The processing changes associated with the revision from 21112 to 23132 were reviewed and it was determined that the revisions would not influence model impacts. As a result, the existing model ready AERMET Version 21112 files were utilized for this assessment.

6. MODELING ANALYSIS DESIGN

6.1 Model Selection

An evaluation of the maximum ambient air quality impacts from the proposed Copper World Project was conducted using AERMOD version 23132. Trinity Consultants uses the enhanced version of AERMOD from BREEZE Software.

6.2 Model Input Defaults/Options

The recommended regulatory default options for AERMOD, as stated in the Guidelines, were used for the model runs. The regulatory default options in AERMOD include the use of stack-tip downwash, incorporation of the effects of elevated terrain, and calms and missing data processing routines.

The missing data processing routines included in AERMOD allow the model to handle missing meteorological data in the processing of short-term averages. The model treats missing meteorological data in the same way as the calms processing routine (i.e., it sets the concentration values to zero for that hour and calculates the short-term averages according to EPA's calms policy, as set forth in 40 CFR Part 51 Appendix W – Guideline on Air Quality Models). Calms and missing values are tracked separately to flag the short-term averages. An average that includes a calm hour is flagged with a "c", an average that includes a missing hour is flagged with an "m", and an average that includes both calm and missing hours is flagged with a "b". If the number of hours of missing meteorological data exceeds 10 percent of the total number of hours for a given model run, a cautionary message is written to the main output file, and the user is referred to Section 5.3.2 of On-site Meteorological Program Guidance for Regulatory Modeling Applications (EPA, 1987).

The May 2017 updates to 40 CFR Part 51 Appendix W – Guideline on Air Quality Models included the incorporation of the existing detailed screening option of the Ozone Limiting Method (OLM) and Plume Volume Molar Ratio Method (PVMRM) into the regulatory version of AERMOD. The OLM was used to evaluate the impact of NO_2 from the Copper World Project operations. The OLM involves an initial comparison of the estimated maximum NO_x concentration and the ambient ozone concentration to determine the limiting factor in the formation of NO_2. Total conversion is assumed if the ozone concentration is greater than the maximum NO_x concentration. If the NO_x concentration is greater than the ozone concentration, the formation of NO_2 is limited by the ambient ozone concentration. The method also uses a correction factor to account for the in-stack conversion of NO_x to NO_2.

For the assessment of the entire project using the on-site CWP Met-2 Station meteorological data, hourly background ozone data from May 2023 through April 2024 (to coincide with the meteorological data period used for the modeling) from the State and Local Air Monitoring Stations (SLAMS) Green Valley monitoring site was used. Based on mid-latitude westerly synoptic patterns, locations west of the proposed Copper World Project facility are more likely to represent an "up-wind" background; therefore, the Green Valley site is the most representative of the conditions at the Copper World Project site.

Additionally, for the assessment of sources east of the Santa Rita Mountains using the 2007-2009 onsite meteorological data, hourly background ozone data for March 2007 through February 2009 (to coincide with the meteorological data period) from the CASTNET Chiricahua National Monument site was used. These data were utilized to ensure consistency with previous regional permitting actions and to ensure the use of a dataset representative of the terrain and ambient conditions which occur east of the Santa Rita Mountains.

An in-stack ratio of 0.065 was used for stationary engines; this ratio is based on the average of similar engines found in EPA's NO_2/NO_x In-Stack Ratio (ISR) Database (https://www3.epa.gov/scram001/no2_isr_database.htm). The database was sorted by engine type, fuel, and engine capacity. The average of the ratios for reciprocating internal combustion (IC) diesel engines, rating in size from 400 kW to approximately 1900 kW, was used to calculate the average for use in the model. The data used to calculate the average is included in **Appendix E**. The ISR database was also reviewed to determine the ISR for the sulfuric acid plant and fire water pump; however no similar sources are included in the database. The EPA guidance issued on March 1, 2011 allows for a default ISR of 0.5 in the absence of more appropriate source-specific information. As such, an ISR of 0.5 was used for the sulfuric acid plant and fire water pump. The NO_2/NO_x ratio for blasting sources was based on field test data presented in *NO_X Emissions from Blasting Operations in Open-cut Coal Mining* (Attalla, et al, 2008). A maximum in-stack ratio of 0.08 (rounded to 0.10 for input in the model) was calculated based on ANFO blasting plume measurement results from blasting with ANFO. The Attalla, et al. paper is included in **Appendix E**.

6.3 Rural/Urban Classification

For modeling purposes, the rural/urban classification of an area is determined by either the dominance of a specific land use or by population data in the study area. Generally, if the sum of heavy industrial, light-moderate industrial, commercial, and compact residential (single and multiple family) land uses within a three-kilometer radius from the facility are greater than 50%, the area is classified as urban. Conversely, if the sum of common residential, estate residential, metropolitan natural, agricultural rural, undeveloped (grasses), undeveloped (heavily wooded) and water surfaces, land uses within a three-kilometer radius from the facility are greater than 50%, the area is classified as rural. Alternatively, the area is classified as urban if the population is greater than 750 persons per km^2.

As shown in the aerial photograph in **Figure 2-1**, rural land use in the area surrounding the proposed Copper World Project is much greater than 50%; thus, the rural classification was used in the modeling.

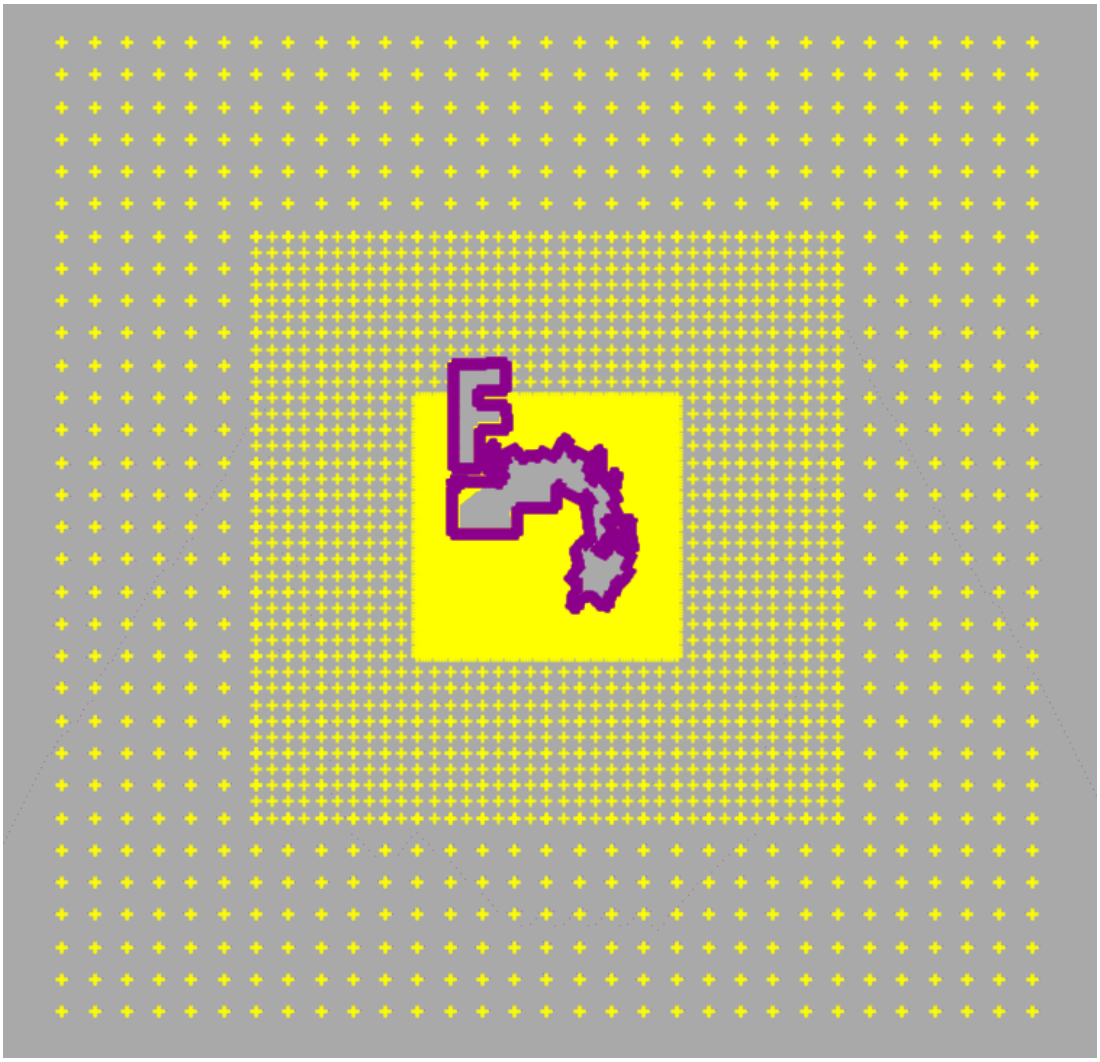
6.4 Receptor Network

Following ADEQ's Guidance, the receptor grid (see **Figure 6-1**) consisting of the following was used in the model:

- receptors spaced at 25 meters along the Process Area Boundary (PAB);
- receptors spaced at 100 meters from the PAB to 1 kilometer;
- receptors spaced at 500 meters from 1 kilometer to 5 kilometers; and
- receptors spaced at 1000 meters from 5 kilometers to 10 kilometers.

Additionally, as Helvetia/Santa Rita Road crosses the southwest portion of the facility site west of the processing plant, discrete receptors were placed along the roadway where the public may traverse the road. Finally, the proposed Public Access Restriction Plan for the site would allow ongoing access to neighboring landowners and roadway users. This access would occur along discrete roadway corridors, within a 50-75 ft setback along portions of the southwest boundary of the main mine boundary and within a 100 ft setback along portions of the southeast boundary along of the "F Block" tailings facility. A final 50 ft easement is also included for a driveway extending off Santa Rita Road. To account for these impact locations, discrete receptors along these access corridors were incorporated into the modeled receptor network.
No further receptors were placed within the contiguous outer boundary of Copper World's private land boundary, as this represents a public access limitation.

Figure 6-1. Copper World Project Receptor Layout



6.5 Receptor and Source Elevations

The U.S. Geological Survey (USGS) has developed a National Elevation Dataset (NED). The NED is a seamless mosaic of best-available elevation data. The primary initial data source is the 7.5-minute elevation data for the conterminous United States. Receptor elevations were determined from the NED 1/3 arc-second data obtained from the Multi-Resolution Land Characteristics Consortium (MRLC) in horizontal datum of NAD83 and vertical datum of NAVD88. The 7.5-minute Digital Elevation Data (DEM) provides coverage in 7.5 X 7.5-minute blocks. Each file provides the same coverage as a standard 1:24,000 scale quadrangle map.

The NED data was processed using the EPA terrain preprocessor known as AERMAP (User's Guide for the AERMOD Terrain Preprocessor (AERMAP), U.S. Environmental Protection Agency, Office of Air Quality Planning and Standards, Air Quality Assessment Division, Air Quality Monitoring Group, Research Triangle Park, North Carolina, EPA-454/B- 18-004, April 2018). AERMAP, like AERMET, is a preprocessor program

developed to process terrain data in conjunction with a layout of receptors and sources to be used in AERMOD.

For complex terrain situations, AERMOD captures the essential physics of dispersion in complex terrain and therefore needs elevation data that conveys the features of the surrounding terrain. In response to this need, AERMAP first determines the base elevation at each receptor or source. AERMAP then searches for the terrain height and location with the greatest influence on dispersion for each individual receptor. This height is referred to as the hill height scale. The base elevation and hill height scale data are produced by AERMAP as a file (or files) which are then inserted into an AERMOD input control file. The files produced by AERMAP for the modeling are included with this report (**Appendix F**).

Base elevations of all emissions sources were generated by AERMAP, except for sources that are impacted by significant material movement by the mining process (e.g., ore and waste rock haul roads, pits, and piles, etc.). In these cases, base elevations were derived from the detailed elevations taken from the Year 2, Year 8, and Year 14 mine layouts, as applicable.

6.6 Modeling Domain

The AERMAP terrain preprocessor requires the user to define a modeling domain. The modeling domain is the area containing all the receptors and sources being modeled with a buffer to accommodate any significant terrain elevations. Significant terrain elevations include all the terrain at or above a 10% slope from each receptor.

BREEZE's software automatically calculates the modeling domain based on the receptor grid used and identifies each 7.5-minute DEM quadrangle that must be used in AERMAP to meet the 10% slope requirement.

6.7 Source Characterization

A plan view map depicting the mine component layout for Year 2, Year 8, and Year 14 is included in **Appendix A**.

Preliminary plan views of the processing facility operations, which consists of the locations of the primary emissions sources and plant roads, are further included in **Appendix A**. This layout applies to Year 2, Year 8, and Year 14. A general description of each emissions source type and how each source was parameterized is presented below.

6.7.1 Point Sources

Point sources at the Copper World Project include dust collectors, emergency generators, and an emergency fire water pump. Emissions from these sources were modeled as individual point sources. Stack parameters for the point sources were based on design parameters and/or conservative estimated values. Emissions from emergency generators were included in the modeling even though most other operations would be shut down if the generators were needed. The point source emissions were modeled using the particle size distribution shown in Table E.5 of **Appendix G**.

6.7.2 Volume Sources

6.7.2.1 Road Sources

A refined road network was developed to depict the anticipated haul truck routes and dumping locations during each year of the mine plan. This is the basis of the emissions inventory used for Year 2, Year 8 and Year 14 modeling. Emissions due to haul road and general plant traffic on the unpaved road network were modeled as volume sources, with the exception of delivery and product shipment vehicle emissions along Santa Rita Rd as described below. The modeling parameters were based on guidance from ADEQ and the AERMOD User's Guide. The modeling parameters were set as follows:

- the volume height was set equal to 1.7 times the height of the vehicles generating the emissions;
- the initial vertical dimension was set equal to the volume height divided by 2.15;
- the release height was set equal to half of the volume height; and
- the initial lateral dimension was set to the width of the haul trucks plus 6 meters divided by 2.15 (the road was further divided into two lanes representing 2-way traffic).

The majority of emissions from the haul road network are due to large haul trucks. The height of the haul trucks obtained from the manufacturer's data (front canopy height, Caterpillar 793F Mining Truck) is 6.6 meters (21.6 feet). Thus, for each road source, the volume height was set to 11.22 meters (1.7 times the height of the vehicles generating the emissions), the initial vertical dimension was set to 5.22 meters (volume height divided by 2.15), and the release height was set to 5.61 meters (half of the volume height).

The haul truck width was estimated to be 8.31 meters (overall canopy width, Caterpillar 793F Mining Truck). Thus, the initial lateral dimension for each volume was set to 6.65 meters (14.31 meters [haul truck width of 8.31 meters plus 6 meters] divided by 2.15). The road sources were placed along the road network at approximately 25-meter intervals. The distribution of haul road emissions generated inside the pit versus outside the pit was taken into account when distributing haul road emissions generated by the haul trucks among the open pit and road sources.

The majority of the plant road emissions are due to smaller vehicles such as vehicles delivering miscellaneous consumables, reagents or fuels and lubricants. The height of a representative delivery vehicle was obtained from the manufacturer's data (Getman A64 Service Fuel vehicle) is 2.3 meters [7.4 feet]). Thus, for each plant road source, the volume height was set to 3.84 meters (1.7 times the height of the vehicles generating the emissions), the initial vertical dimension was set to 1.79 meters (volume height divided by 2.15), and the release height was set to 1.92 meters (half of the volume height). The delivery vehicle width was estimated to be 2.08 meters. Thus, the initial lateral dimension for each plant road volume source was set to 3.76 meters (8.08 meters [haul truck width of 2.08 meters plus 6 meters] divided by 2.15). The road sources were placed along the plant road network at approximately 25-meter intervals.

The haul road emissions were modeled using the particle size distribution shown in Table E.1 of **Appendix G**. Numerical allocation of emissions to the road sources for Year 2, Year 8, and Year 14 are detailed in the emissions calculation workbooks in **Appendix F**. Finally, haul road surface particulate emissions are proposed to be controlled by a mix of watering and chemical surfactant. The application of control was designed to ensure enhanced control on sections of the haul road network with the potential for offsite impacts. The road emission control strategy was designed to achieve 90% control on all processing plant roads. For the heavy haul road network, the distribution of proposed particulate control differs by roadway location with locations being designed to achieve either 90% or 95% particulate emissions control. The mine layouts in **Appendix A** include locations of the application of 90% or 95% particulate emissions controls for each modeled mine plan year.

6.7.2.2 Waste Rock Facilities

6.7.2.2.1 Year 2

Fugitive emissions associated with management of the single WRF were represented by a single volume source. The dimensions of the area were determined based on the Year 2 mine layout. The initial horizontal dimension was set to the length of the side of the WRF divided by 4.3. The initial vertical dimension was set to the height of the WRF divided by 2.15, and the release height was set to half of the WRF placement area height.

Mining activity in Year 2 would actually occur in two sequential phases with hauling of waste rock from the Peach Pit (PE2) and Elgin (PE1) pits (primarily the Elgin Pit), being transported to the haul road location for the Copper World Pit (haul road sources CW1/2, CW3/4 and CW5/6), to construct the Copper World roads prior to commencement of mining in the Copper World Pit. This would represent the transport of approximately 2.3 million tons of waste rock from the Elgin Pit to the Copper World Pit haul road prior to the movement of any material from the Copper World Pit. The Copper World Pit materials (ore and waste rock) represent 5.4 million tons of material. In order to assess the most conservative single modeled assessment for Year 2 operations, rather than separating the model into the two chronological phases, all waste rock from Elgin was routed to the Waste Rock Facility (inconsistent with the mine plan). The model was then run with concurrent mining and hauling of Copper World material and waste rock transport from the Elgin Pit to the WRF. This overstates the impacts of mining in Year 2 as it accounts for concurrent movement of waste rock from Elgin Pit and mining in Copper World Pit.

6.7.2.2.2 Year 8

Fugitive emissions associated with managing the Year 8 WRF areas were represented by a single volume source for each of the two active WRF placement areas. The dimensions of each WRF placement area (Waste Rock Piles C and D) were determined based on the Year 8 mine layout. The initial horizontal dimension was set to the length of the side of each WRF area divided by 4.3. The initial vertical dimension was set to the height of the WRF placement area divided by 2.15, and the release height was set to half of the WRF placement area height.

6.7.2.2.3 Year 14

Fugitive emissions associated with managing the Year 14 WRF areas were represented by a single volume source for each of the four active WRF placement areas. The dimensions of each WRF placement area (Waste Rock Piles C, D, F, and G) were determined based on the Year 14 mine layout. The initial horizontal dimension was set to the length of the side of each WRF area divided by 4.3. The initial vertical dimension was set to the height of the WRF placement area divided by 2.15, and the release height was set to half of the WRF placement area height. Once initial horizontal dimensions were developed for the Year 14 WRF areas, a review of volume source exclusion zones was completed for volume sources in close proximity to model receptors. For a WRF with volume source exclusion zones that interacted with model receptors, those WRF volume sources were divided into multiple smaller volume sources with the equivalent dimensions and emissions were distributed between the volume sources according to the number of smaller volume sources required.

6.7.2.3 Other Fugitive Particulate Sources

Other fugitive particulate emission sources that were modeled as volume sources include the following:

- Fugitive emissions from truck unloading at the sulfide Run of Mine (ROM) feed bin and oxide ROM feed bin (oxide present in Year 2 and Year 8 only) were represented by a single volume source. The side length was set to 12 meters (approximate width of dump pocket); therefore, the initial horizontal dimension was set to 2.79 meters (12/4.3). The vertical length was set to 1 meter (vertical drop of dump pocket). Consequently, the initial vertical dimension was set to 0.47 meters (1/2.15) and the release height was set to 0 meters (dump pocket is at grade level).

- Fugitive emissions from the sulfide and oxide rock breakers were represented by a single volume source each. The side length was set to 12 meters (approximate width of feed bin to mouth of rock breaker); therefore, the initial horizontal dimension was set to 2.79 meters (12/4.3). The vertical length was set to 1 meter (vertical drop of the feed bin). Consequently, the initial vertical dimension was set to 0.47 meters (1/2.15) and the release height was set to 0 meters. Further, because the rock breakers are only utilized in limited instances where material is not sufficiently fractured by blasting, the utilization rate and emissions from the rock breaker is limited.

- Fugitive emissions due to wind erosion from the sulfide coarse ore stockpile (present in Years 2, 8, and 14) and oxide coarse ore stockpile (present in Year 2 and Year 8 only) were represented by a single volume source. The side length of the sulfide coarse ore stockpile obtained from the map was 117 meters (average width of the stockpile); therefore, the initial horizontal dimension of the sulfide coarse ore stockpile was set to 27.2 meters (117/4.3). The side length of the oxide coarse ore stockpile obtained from the map was 119 meters (average width of the stockpile); therefore, the initial horizontal dimension of the sulfide stockpile was set to 27.7 meters (119/4.3). For both the sulfide and oxide coarse ore stockpiles, the vertical height was set to 12 meters (average stockpile height). Consequently, the initial vertical dimension will be set to 5.58 meters (12/2.15), and the release height will be set to 6 meters (half of the volume height of 12 meters).

- Fugitive emissions from truck unloading at the temporary ore stockpile (present in Years 2, 8, and 14) and truck unloading of oxide ROM ore at the HLP (present in Year 2 and Year 8 only) were each represented by a single volume source. The side length for each was set to 8.31 meters (approximate width of haul truck bed); therefore, the initial horizontal dimension was set to 1.93 meters (8.31/4.3). The vertical length was set to 1.3 meters (approximate dump clearance of haul truck). Consequently, the initial vertical dimension was set to 0.6 meters (1.3/2.15), and the release height was set to 0 meters (assume dump to ground level).

- Fugitive emissions due to wind erosion from the temporary ore stockpile were represented by a single volume source. The side length of the dump pad obtained from the map was 55 meters; therefore, the initial horizontal dimension of the temporary ore stockpile was set to 12.8 meters (55/4.3). The vertical height was set to 12 meters (average stockpile height). Consequently, the initial vertical dimension was set to 5.58 meters (12/2.15), and the release height was set to 6 meters (half of the volume height of 12 meters).

- Fugitive emissions due to wind erosion of the tailings storage area were represented by either two or three volume sources, depending on model year, in order to most adequately represent the polygon layout and orientation of the active tailings placement area. In Year 14, tailings will be placed in two separate tailings areas; TSF-1, located north of the plant/processing area, will consist of two placement areas (designated in the model as TSF-1N [north] and TSF-1S [south]) and TSF-2 located south of the plant/processing area. As volume sources were georeferenced in the model as squares, the use of three volume sources was chosen to represent the irregular shape of the tailings storage areas, which can be approximated by three square areas. The total active area of tailings placement at Year 14 was

determined to be approximately 2,023,428 m^2 (500 acres). The area was then divided proportionately into three sub-areas based on the size of each, which was represented in the model as volume source "squares". The side length of each volume source "square" has a side length based on its approximate size as measured using the Year 14 layout imported into the model; the initial horizontal dimension of each volume source was to the slide length/4.3. The vertical dimension was set to the vertical dimension of the pile/2.15. The release height for all sources was set to half of the volume height of each pile. Analogously in Year 2 and Year 8, the same methodologies were utilized while the geo-referenced locations were allocated based on the Year 8 and Year 2 mine plan layouts. In Year 2, tailings will be placed in one tailings area, TSF-1, which is located north of the plant/processing area and will consist of two placement areas (designated in the model as TSF-1W [west] and TSF-1E [east]). In Year 8, tailings will be placed in one tailings area, TSF-1 which is located north of the plant/processing area and will consist of two placement areas (designated in the model as TSF-1N [north] and TSF-1S [south]). For all three modeled years, the TSF volume source exclusion zones interacted with model receptors. As such, the TSF volume sources were divided into multiple smaller volume sources with the equivalent dimensions and emissions were distributed between the volume sources according to the number of smaller volume sources required. These volume sources as designated with an "A" or a "B" in the model (ex: Year 8 TSF1N_A and TSF1N_B).

- Fugitive emissions from transfer points (ex: sulfide/oxide ore bin into the crusher, crusher discharge to conveyor, etc.) were represented by single volume sources. The side length was set to 2 meters (approximate average width of the transfer points); therefore, the initial horizontal dimension was set to 0.47 meters (2/4.3). The vertical length was set to 3 meters (approximate height of material drops). Consequently, the initial vertical dimension was set to 0.7 meters (3/4.3), and the release height was set to 3 meters (assumed height of the transfer points).

- Fugitive emissions due to vehicle traffic (fugitive dust) in the ancillary plant areas, separate from the plant road network traffic, were represented by volume sources. One volume source was assigned for each of the following areas:

  - Plant Area Warehouse (WHMOBV)
  - Plant Area Truck Shop (TRKMOBV)
  - Crusher Dump Pad (CDRMOBV)
  - Molybdenum and Copper Processing Area (CUMOMOBV).

The majority of the plant area emissions are due to smaller vehicles; a skid steer was used to represent a typical type of vehicle traveling around the plant areas off of the plant area roads. The height of a representative skid steer obtained from the manufacturer's data (Cat 246C Skid Steer) is 2.13 meters [7.0 feet]). Thus, for each plant road source, the volume height was set to 3.62 meters (1.7 times the height of the vehicles generating the emissions), the initial vertical dimension was set to 1.68 meters (volume height divided by 2.15), and the release height was set to 1.81 meters (half of the volume height). The skid steer width is 1.67 meters. Thus, the initial lateral dimension for each plant area volume source was set to 0.39 meters (1.67 meters divided by 2.15).

The above material transfer emissions were modeled using the particle size distribution shown in Table E.2 of **Appendix G**. All of the fugitive emission sources, base elevations, source dimensions, and source locations were developed utilizing the mine planning drawings for Year 2, Year 8, and Year 14 of the mine life (**Appendix A**).

6.7.2.4 Gaseous Emissions Due to Blasting

The gaseous emissions due to blasting in the pit were modeled as volume sources. The volume sources were placed within the pit using the methodology presented by ADEQ[3] where the blasting volume sources are concentrated into a single area within the pit. Blasting in each pit is represented by six (6) individual volume sources. The side length of each volume source was set to the square root of total blast area divided by 6 (for example for Rosemont Pit in Year 8, the blast area is 362,404 ft^2; the side length was set to SQRT(362,404ft^2/6) = 74.9 m); and the initial horizontal dimension was set to the side length divided by 4.3 (for example for Rosemont Pit in Year 8 = 74.9/4.3 = 17.4)).

The Open Blast Open Detonation Model (OBODM) was used to calculate the blast dimensions for each pit for each model year based on the ANFO usage per blast. The release height from OBODM represents the top of the blast plume. As such, the volume source release height for each volume source was set to the OBODM plume height divided by 2 and the initial vertical dimension of each volume source was set to the OBODM release height divided by 2.15. The base elevation for the volume sources in the pit was set to the elevation of the terrain defining the bottom of the pit based on the fact that these emissions must rise above the pit's walls before being dispersed downwind.

The Copper World Project anticipates limiting routine daily blasting to between noon and 4 p.m., with the exception of the Broadtop Butte Pit. As a result, the variable emission rate option HROFDY in AERMOD was used to model the blasting emissions in each of these clock hours. For model Years 2 and 14 for all pits and for model Year 8 for the Rosemont Pit, for evaluating the 1-hr averaged impacts from NO_2, SO_2, and CO, blasting emissions were set to occur every hour between noon to 4 p.m. For model Year 8 for the Broadtop Butte Pit evaluation of the 1-hr averaged impacts from NO_2, SO_2, and CO, blasting emissions were set to occur every hour between noon to 2 p.m. On limited occasions, as required by safety considerations (lightning and other weather conditions), blasting may occur outside of these periods. These occurrences would be considered outside of normal operations and have not been explicitly modeled.

When testing the hourly impact of blasting emissions between noon and 4 p.m., the results indicate that the maximum impact occurs in the 3-4 p.m. clock hour. Therefore, for model Years 2 and 14 for all pits and for model Year 8 for the Rosemont Pit, for all impact averaging periods greater than the 1-hr averaged impacts, blasting was set to occur at 4 p.m. every day. For model Year 8 for the Broadtop Butte Pit, blasting was sent to occur at 12 p.m. every day as 12 p.m. represented the maximum impact period for the period from 12p.m. to 2p.m. The HROFDY variable emissions rate option in AERMOD was used for this. The total blasting rates vary based on the maximum mine planning rates for each mining pit for Year 2, Year 8, and Year 14, as detailed in **Appendix F**. The PM_{10} emissions from blasting were modeled as a volume source and used the particle size distribution shown in Table E.3 of **Appendix G**.

6.7.3 Area Sources

Delivery and product shipment vehicle emissions along Santa Rita Road segments within the Copper World Project boundary were modeled as an area source; this was done to avoid the exclusion zones of defined volume sources.[4] The roadway was initially laid out in the model using the volume source methodology for road volume sources described in Section 6.7.2.1. The area sources were then drawn around the volume sources as close to the edges of the volume sources as possible to maintain the representative lateral dimensions and source spacing (the Santa Rita Road volume sources have been left in the model to verify

[3] July 20th, 2023 meeting between ADEQ, Hudbay, and Trinity.

[4] Volume source exclusion zone is ((2.15 x sigma-y) + 1 meter).

placement of the area sources; however, the volume sources are assigned a zero emissions rate). Road area sources were limited to a 10:1 length to width ratio so in some cases multiple area sources were defined to cover a road segment. Emissions for the area source segment were the sum of the volume source segment emissions within the area source. Per ADEQ recommendation receptors within 1 meter of an area source were relocated to a distance of 1 meter from the area source.[5]

6.7.4 Open Pit Sources

Fugitive particulate emissions occur at a single source in Year 14, characterized as an open pit. Within the Year 14 modeling assessment, the mine pit represents the Rosemont Pit at the location of the Rosemont Ore Deposit. The pit as designed is constrained entirely to private land. For Year 8 and Year 2, multiple pit locations will be mined. For Year 8 this includes the Rosemont Pit as well as the Broadtop Butte Pit. For Year 2 this includes the Peach Pit, Elgin Pit, Heavyweight Pit, and Copper World Pit. For each modeled year, the pit sources were included in the model at each representative location.

The open pit source parameters – easterly length, northerly length, and volume – were based on the length and width dimensions of the equivalent rectangle drawn to simulate the same horizonal area of the polygon pit shape in the model and the planned depth of the pit at the modeled operational year. The release height for emissions within the pits was set to zero.

The open pit source option in the AERMOD model requires particle size distribution data in the form of the mass-mean particle diameter, mass weighted size distribution, and particle density. Table E.1 of **Appendix G** shows the particle size distribution developed for Haul Road Emissions. This distribution was used for the open pit source since a majority of the emissions in the pit are Haul Road Emissions.

A particle density of 2.44 gm/cm^3, the other required input variable, was used in the modeling as a representative value of the average density of the various rock materials (overburden, waste rock, ore) that will be mined.

6.7.5 Plume Depletion

One other option in the AERMOD model requires particle size data. This option is known as Dry Deposition (DDEP), which specifies that dry deposition flux values will be calculated. This option, when selected in the modeling, automatically includes dry removal (depletion) mechanisms (known as dry plume depletion [DRYDPLT] in the old ISC modeling program and earlier versions of AERMOD) in the calculated concentrations. This option represents a regulatorily approved option for assessment of offsite impacts. The particulate models (24hr PM_{10}, 24hr $PM_{2.5}$ and annual $PM_{2.5}$) were initially run without the DDEP option. If the modeled impact combined with background concentration exceeded the NAAQS at select receptors, the model was re-run with 1) the DDEP option enabled and 2) a reduced receptor grid which contained only those receptors that exceeded the NAAQS.

6.8 Building Downwash

Building downwash effects were evaluated by incorporating the appropriate building/structure dimensions into the AERMOD input files using BREEZE's commercial version of EPA's Building Profile Input Program for PRIME (BPIPPRM) software. The BPIPPRM program is EPA approved and includes the latest EPA building

[5] Email to Trinity Consultants from Feng Mao of ADEQ on 9/7/2022 for the AMI South 32 Project.

downwash algorithms. The downwash files generated by the BPIPPRM program are provided electronically with this report (**Appendix F**).

7. EMISSIONS INVENTORY

Emissions from the Copper World Project will result from process equipment and mining operations. Process equipment was modeled at maximum capacity (for instantaneous material movement built into the mine plan calculations). Emissions from mining will depend upon the mining rate and haul truck travel necessary to transport the ore and waste from the pit to the primary crusher, temporary ore stockpile, Heap Leach Pad, and the Waste Rock Facility (WRF) storage areas. A summary of average and maximum mining rates and haul truck travel (vehicle miles) is presented in **Appendix H**. The mining information in **Appendix H** indicates that the highest projected emissions generating source (heavy haul truck travel) will occur in Year 14. As a result, Year 14 was selected to assess maximum ambient impacts. Further, because Year 8 represents the maximum period of out of pit haul truck travel concurrent with the maximum mining rate, this period has been included for assessment. For the assessment of the early mine life emissions, the highest projected annual mining impacts and highest haul truck travel in close proximity to the ambient boundary occurs during Year 2. As a result, Year 2 was selected for the assessment of maximum ambient impacts during the early mine life.

Since haul truck travel will be the primary source of emissions (PM_{10} and tail pipe), Year 14, Year 8, and Year 2 were modeled. Ambient impacts from operations during all other years are projected to have lower impacts than during Year 14, Year 8, or Year 2. In addition, ore and waste rock tonnage and haul mileage offset each other; therefore, haul truck mileage used in the modeling represents a conservative maximum. An increase in ore and/or waste rock tonnage (from the average value) will coincide with a haul distance decrease during any particular phase of operations. As a result, emissions would not likely increase even if short term haul truck tonnages or mileage increased. The total number of haul trucks in the mine fleet, the average haul truck speed, and the utilization of fugitive dust control practices are the limiting factors for haul truck emissions.

7.1 Annual Criteria Pollutant Emissions Modeling

Annual impacts of particulate and gaseous emissions were based upon emissions calculated using the maximum annual process rates for Year 14, Year 8, and Year 2, respectively. Emissions calculations are included in **Appendix F**.

7.2 Short-term Criteria Pollutant Emissions Modeling

Short-term impacts (1-hour, 3-hour, 8-hour, and 24-hour) were based upon the emissions calculated using the maximum short term process rates for Year 14, Year 8, and Year 2, respectively. Emissions calculations are included in **Appendix F**.

8. EVALUATION OF DISPERSION MODELING RESULTS

8.1 Primary Standards

The purpose of the dispersion modeling outlined in this report is to demonstrate that emissions from the Copper World Project will not cause exceedances of applicable National Ambient Air Quality Standards (NAAQS). This final impact analysis includes all information necessary for this demonstration including: (a) background concentrations; (b) a source location map; (c) a complete list of source parameters; (d) complete modeling input and output files; and (e) graphic presentations of the modeling results for each pollutant showing the magnitude and location of the maximum ambient impacts.

8.2 Criteria Pollutant Impact Results

This section of the report discusses the model output results. The criteria pollutant model results for Year 14, Year 8 and Year 2 are shown in **Table 8-1** through **Table 8-5**, respectively. The results of the modeling show that the Copper World Project is in compliance with all applicable NAAQS. Model source parameters are included in **Appendix F**. Model input and output files are further included electronically (**Appendix F**).

Table 8-1. Criteria Pollutant Model Results – Copper World Project – Year 14 – All Sources – CWP Met-2 Station Meteorological Data

Pollutant	Averaging Period	Modeled Concentration (µg/m³)	UTM Easting (m)	UTM Northing (m)	Background Concentration (µg/m³)	Maximum Ambient Concentration (µg/m³)[g]	NAAQS (µg/m³)
PM_{10}	24-hr [a]	110.7	522535.80	3522866.90	Monthly	110.7	150
$PM_{2.5}$	24-hr [b]	8.11	519082.44	3524689.53	9.1	17.2	35
	Annual [c]	4.21	519013.08	3524648.50	3.9	8.11	9
NO_x	1-hr [d]	107.8	519484.50	3525011.50	26.3	134.1	188.6
	Annual	1.02	519670.00	3524676.80	2.6	3.62	100
SO_2	1-hr [e]	68.3	519461.20	3525004.50	2.6	70.9	196
	3-hr [f]	27.9	519461.20	3525004.50	3.4	31.3	1,300
CO	1-hr [f]	3,999	522703.50	3521110.80	920	4,919	40,000
	8-hr [f]	731	522678.90	3521115.00	575	1,306	10,000

a. Maximum of 2nd highest modeled concentrations for a 1-year period.
b. Maximum of 1-year 8th highest modeled concentration.
c. Maximum of 1-year maximum modeled concentration.
d. Maximum of 1-year 8th highest modeled concentration.
e. Maximum of 1-year 4th highest modeled concentration.
f. Maximum of 2nd highest modeled concentration.
g. PM_{10} and $PM_{2.5}$ model runs were completed without dry depletion.

Table 8-2. Criteria Pollutant Model Results – Copper World Project – Year 14 – Sources East of Santa Rita Mountain Ridgeline – Onsite Meteorological Data and Particulate Background

Pollutant	Averaging Period	Modeled Concentration (µg/m³)	UTM Easting (m)	UTM Northing (m)	Background Concentration (µg/m³)	Maximum Ambient Concentration (µg/m³)[g]	NAAQS (µg/m³)
PM_{10}	24-hr [a]	101.4	522966.70	3523557.10	47.7	149.1	150
$PM_{2.5}$	24-hr [b]	8.54	522966.70	3523557.10	9.1	17.6	35
	Annual [c]	3.29	522966.70	3523557.10	3.9	7.19	9
NO_x	1-hr [d]	39.66	522558.80	3521195.30	26.3	65.96	188.6
	Annual	0.011	523100.70	3521325.00	2.6	2.61	100
SO_2	1-hr [e]	0.16	521162.80	3523729.00	2.6	2.76	196
	3-hr [f]	0.08	521162.80	3523629.00	3.4	3.48	1,300
CO	1-hr [f]	2,636	522537.00	3521192.70	920	3,556	40,000
	8-hr [f]	778	523100.70	3521325.00	575	1,353	10,000

a. Maximum of 3rd highest modeled concentrations for a 2-year period.
b. Maximum of 2-year means of 8th highest modeled concentrations for each year modeled.
c. Maximum of 2-year means of maximum modeled concentrations for each year modeled.
d. Maximum of 2-year means of 8th highest modeled concentrations for each year modeled.
e. Maximum of 2-year means of 4th highest modeled concentrations for each year modeled.
f. Maximum of 2nd highest modeled concentrations for each year modeled.
g. PM_{10} and $PM_{2.5}$ model runs were completed without dry depletion.

Table 8-3. Criteria Pollutant Model Results – Copper World Project – Year 8 – All Sources – CWP Met-2 Station Meteorological Data

Pollutant	Averaging Period	Modeled Concentration (µg/m³)	UTM Easting (m)	UTM Northing (m)	Background Concentration (µg/m³)	Maximum Ambient Concentration (µg/m³)[g]	NAAQS (µg/m³)
PM_{10}	24-hr [a]	148.1	521573.20	3524622.10	Monthly	148.1	150
$PM_{2.5}$	24-hr [b]	10.0	518844.17	3524559.59	9.1	19.1	35
	Annual [c]	4.97	519013.08	3524648.50	3.9	8.87	9
NO_x	1-hr [d]	107.8	519484.50	3525011.50	26.3	134.1	188.6
	Annual	1.02	519670.00	3524676.80	2.6	3.62	100
SO_2	1-hr [e]	68.3	519461.20	3525004.50	2.6	70.9	196
	3-hr [f]	27.9	519461.20	3525004.50	3.4	31.3	1,300
CO	1-hr [f]	7,842	522703.50	3521110.80	920	8,762	40,000
	8-hr [f]	1,796	522703.50	3521110.80	575	2,371	10,000

a. Maximum of 2nd highest modeled concentrations for a 1-year period.
b. Maximum of 1-year 8th highest modeled concentration.
c. Maximum of 1-year maximum modeled concentration.
d. Maximum of 1-year 8th highest modeled concentration.
e. Maximum of 1-year 4th highest modeled concentration.
f. Maximum of 2nd highest modeled concentration.
g. PM_{10} and $PM_{2.5}$ model runs were completed without dry depletion.

Table 8-4. Criteria Pollutant Model Results – Copper World Project – Year 8 – Sources East of Santa Rita Mountain Ridgeline – Onsite Meteorological Data and Particulate Background

Pollutant	Averaging Period	Modeled Concentration (µg/m³)	UTM Easting (m)	UTM Northing (m)	Background Concentration (µg/m³)	Maximum Ambient Concentration (µg/m³)[g]	NAAQS (µg/m³)
PM_{10}	24-hr [a]	92.5	522966.70	3523557.10	47.7	140.2	150
$PM_{2.5}$	24-hr [b]	11.1	522966.70	3523557.10	9.1	20.2	35
	Annual [c]	4.10	522966.70	3523557.10	3.9	8.00	9
NO_x	1-hr [d]	88.49	522558.80	3521195.30	26.3	114.79	188.6
	Annual	0.015	523100.70	3521325.00	2.6	2.62	100
SO_2	1-hr [e]	0.25	523100.70	3521325.00	2.6	2.85	196
	3-hr [f]	0.19	523100.70	3521325.00	3.4	3.59	1,300
CO	1-hr [f]	5,249	522558.80	3521195.30	920	6,169	40,000
	8-hr [f]	1,773	523100.70	3521325.00	575	2,348	10,000

a. Maximum of 3rd highest modeled concentrations for a 2-year period.
b. Maximum of 2-year means of 8th highest modeled concentrations for each year modeled.
c. Maximum of 2-year means of maximum modeled concentrations for each year modeled.
d. Maximum of 2-year means of 8th highest modeled concentrations for each year modeled.
e. Maximum of 2-year means of 4th highest modeled concentrations for each year modeled.
f. Maximum of 2nd highest modeled concentrations for each year modeled.
g. PM_{10} and $PM_{2.5}$ model runs were completed without dry depletion, with the exception of the Year 8 onsite meteorological data PM_{10} model run.

Table 8-5. Criteria Pollutant Model Results – Copper World Project – Year 2 – All Sources – CWP Met-2 Station Meteorological Data

Pollutant	Averaging Period	Modeled Concentration (µg/m³)	UTM Easting (m)	UTM Northing (m)	Background Concentration (µg/m³)	Maximum Ambient Concentration (µg/m³)[g]	NAAQS (µg/m³)
PM_{10}	24-hr [a]	107.4	519771.30	3525111.30	Monthly	107.4	150
$PM_{2.5}$	24-hr [b]	7.80	518844.17	3524559.59	9.1	17.0	35
	Annual [c]	4.05	519013.08	3524648.50	3.9	7.95	9
NO_x	1-hr [d]	110.2	519539.90	3525130.70	26.3	136.5	188.6
	Annual	1.03	519670.00	3524676.80	2.6	3.63	100
SO_2	1-hr [e]	68.3	519461.20	3525004.50	2.6	70.9	196
	3-hr [f]	27.9	519461.20	3525004.50	3.4	31.3	1,300
CO	1-hr [f]	12,278	519319.30	3525212.50	920	13,198	40,000
	8-hr [f]	2,587	519495.20	3525377.20	575	3,162	10,000

a. Maximum of 2nd highest modeled concentrations for a 1-year period.
b. Maximum of 1-year 8th highest modeled concentration.
c. Maximum of 1-year maximum modeled concentration.
d. Maximum of 1-year 8th highest modeled concentration.
e. Maximum of 1-year 4th highest modeled concentration.
f. Maximum of 2nd highest modeled concentration.
g. PM10 and PM2.5 model runs were completed without dry depletion.

9. OZONE AND SECONDARY PARTICULATE ANALYSIS

ADEQ requested a review of secondary pollutant formation. When precursor emissions for ozone (VOC and NO_X) and/or $PM_{2.5}$ (SO_2 and NO_X) trigger PSD review, ozone and secondary $PM_{2.5}$ ambient impacts must be reviewed. Although the Copper World Project facility will not trigger a PSD review, ADEQ requested a review of secondary pollutant formation.

Elevated ground-level ozone concentrations are the result of photochemical reactions among various chemical species. These reactions are more likely to occur under certain ambient conditions (e.g., high ground-level temperatures, light winds, and sunny conditions). The chemical species that contribute to ozone formation, referred to as ozone precursors, include NO_X and VOC emissions from both anthropogenic (e.g., mobile, and stationary sources) and natural sources (e.g., vegetation).

In the recently released EPA July 2022 guidance,[6] (included in **Appendix I**) proposed project increases above the PSD Significant Emission Rates (SERs) trigger a secondary $PM_{2.5}$ and/or ozone air impact analysis. The EPA July 2022 guidance is relevant for the PSD program and focuses on assessing the ambient impacts of precursors of ozone/$PM_{2.5}$ for the purposes of that program. Modeled Emission Rates for Precursors (MERPs) can be viewed as a Tier 1 demonstration tool under the PSD permitting program that provides a straightforward and representative way to relate maximum source impacts with a critical air quality threshold (e.g., a significant impact level or SIL).[7]

The MERPs framework may be used to describe how an emission rate increase of precursor chemicals (such as NO_2 or SO_2 for $PM_{2.5}$) may change the concentration of a secondary atmospheric pollutant (O_3 or $PM_{2.5}$). This can be used to determine if the change would be less than the Significant Impact Level (SIL) or whether a projected impact may cause or contribute to a violation of the NAAQS. In short, MERPs are intended to be used with SILs as analytical tools for PSD air quality analyses and if necessary, as a cumulative impacts analysis when background air quality values are included.

The first step is to define the applicable MERP site to be used in the assessment. There are three hypothetical model sources in Arizona presented in the EPA MERPS ViewQlik website, as summarized in **Table 9-1**.

[6] Guidance for Ozone and Fine Particulate Matter Permit Modeling, dated July 29, 2022 https://www.epa.gov/system/files/documents/2022-08/2022%20Guidance%20O3%20and%20Fine%20PM%20Modeling.pdf

[7] Ibid.

Table 9-1. EPA Arizona MERP Facilities and Copper World Project

Reference[8]	Hypothetical Source ID (FIPS)	County	Source	Latitude	Longitude	Distance to Rosemont (km)	Max Nearby Terrain (m)	Max Nearby Urban (%)
EPA MERP Guidance	4005	Coconino	36	35.428	-111.270	399	2,483	7.4
	4007	Gila	14	33.469	-110.789	179	1,592	4.3
	4012	La Paz	17	33.400	-113.408	299	757	0.9
Copper World	-	Pima	-	31.856	-110.791	-	2934	7.0

The EPA April 2019 guidance[9] states that the representativeness of a hypothetical source is based on *the chemical and physical environment (e.g., meteorology, background pollutant concentrations, and regional/local emissions).* Hypothetical Source 36 (FIPS 4007) is representative of the Copper World Project site based on the following:

- Proximity – Source 36 is the farthest of the three hypothetical Arizona sources to the Copper World Project facility, approximately 399 km away.
- Terrain & Land Use – Source 36 has the highest nearby urban percentage; the Copper World Project and Source 36 are near urban areas (City of Tucson [Copper World] and City of Flagstaff [Source 36].
- Climate – Although distant from each other, the two sites (Copper World Project and Source 36) occur in similar climatic zones and occur in areas with surrounding higher terrain. The climate characteristics, such as temperature and humidity, surrounding both sites exhibit similar characteristics.
- Regional Sources of Pollutants – Source 36 and the Copper World Project share similar nearby population centers and associated emissions sources. Source 36 is in proximity to the Clarkdale Cement Plant, while the Copper World Project is within proximity to several large surface mining operations.
- Background Pollutant Concentrations – For the reasons listed above, and because both counties (Pima for the City of Tucson and Coconino for the City of Flagstaff) are in attainment for NO_X and SO_2, the ambient concentrations are relatively similar.

[8] https://www.epa.gov/scram/merps-view-qlik, accessed July 2022.

[9] EPA Memorandum, Guidance on the Development of Modeled Emission Rates for Precursors (MERPs) as a Tier I Demonstration Tool for Ozone and PM2.5 under the PSD Permitting Program, April 30, 2019

Based on the above considerations, Source 36 in Coconino County was proposed as the representative MERP source.

The EPA MERPS ViewQlik website provides data for a variety of model combinations, including a source height of 10 m vs. 90 m and emission rates of 500 tons, 1,000 tons, and 3,000 tons. For Hypothetical Source 36 (FIPS 4007), only emission rates of 500 tons and 1,000 tons are available. Additionally, the 1,000-ton source is limited to only a 90 m stack value. The emissions heights at the Copper World Project facility are limited to low level dispersed sources; therefore, a stack height of 10 m at Source 36 is the most representative and conservative. Emissions of NO_x, VOC, and SO_2 at the Copper World Project are all well under 500 tons per year (tpy). Because the 500 tpy MERP includes the assessment with a 10 m stack, this MERP was selected as most representative.

The MERP values from each source were obtained from EPA's MERPS View Qlik application.[10] The NO_x and SO_2 daily and annual MERP values with 500 tons of emissions and with a 10 m source height are contained in **Table 9-2**. NO_x and VOC MERP values are contained in **Table 9-3.**

Table 9-2. MERP Values for Secondary $PM_{2.5}$ Assessment

FIPS	Source	County	Precursor	$PM_{2.5}$ 24-Hour [a, b]	$PM_{2.5}$ Annual [a, b]
4005	36	Coconino	NO_x	37,589	299,905
			SO_2	21,050	32,077

a. Based on 500 tons emissions and 10 m stack height
b. Values obtained from EPA MERPS ViewQlik website in July 2022 (https://www.epa.gov/scram/merps-view-qlik)

Table 9-3. MERP Values for Ozone Assessment

FIPS	Source	County	Precursor	8-Hour Ozone [a, b]
4005	36	Coconino	NO_x	204
			VOC	18,982

a. Based on 500 tons emissions and 10 m stack heights
b. Values obtained from EPA MERPS ViewQlik website in July 2022 (https://www.epa.gov/scram/merps-view-qlik)

9.1 Secondary $PM_{2.5}$ Assessment

Precursor pollutants for $PM_{2.5}$ (i.e., NO_x, and SO_2) can undergo photochemical reactions with gases in the atmosphere, resulting in the formation of secondary $PM_{2.5}$ downwind of an emission source, which can add to concentrations resulting from direct (or primary) emissions of $PM_{2.5}$. Two of the largest constituents of secondary $PM_{2.5}$ in the U.S. are sulphates (SO_4^{2-}) and nitrates (NO_3^-), both of which are formed from their respective precursor pollutants (i.e., SO_2 for SO_4^{2-}, NO_x for NO_3^-).

Pursuant to the EPA July 2022 guidance,[11] a proposed project with an increase of NO_x and/or SO_2 emissions in excess of 40 tpy triggers a secondary $PM_{2.5}$ air impact analysis. Unless a facility is categorized as a listed

[10] https://www.epa.gov/scram/merps-view-qlik, accessed July 2022.

[11] Ibid.

source category under PSD, the emissions compared to the 40 tpy threshold do not include fugitive emissions and are limited to stationary source emissions. Additionally, motor vehicle and mobile source crankcase emissions are excluded from the emissions modeled, consistent with Arizona Revised Statutes (A.R.S.) §49-402(A)(7) and A.A.C. R18-2-101(146)(a)(i). However, at the request of ADEQ, the MERPS analysis was completed for all sources of onsite emissions, including fugitive non-tailpipe emissions.

For Year 14 of the Copper World Project mine life, the total stationary source emissions values would be:

- Annual NO_x: 49.38 TPY, Annual VOC: 13.46 TPY, Annual SO_2: 13.74 TPY

Year 14 has the largest annual emission rates of NO_x, VOC, and SO_2 therefore is used for secondary contribution analysis.

The combined primary and secondary impacts of $PM_{2.5}$ for the source impact analysis were assessed using the highest (AERMOD) modeled primary $PM_{2.5}$ design value concentration, the Class II SIL[12], precursor emissions, and the default MERPs. If the sum of the ratios in the equation below is less than 1, then the combined $PM_{2.5}$ impacts are below the $PM_{2.5}$ SIL. However, a cumulative analysis is necessary since the ratio is greater than 1.

$$\text{Secondary } PM_{2.5} \text{ Impact} = \left(\frac{Highest\ primary\ PM2.5\ modeled\ concentration}{SIL} + \frac{NO_x \text{ Emissions}}{NO_x \text{ MERP}} + \frac{SO_2 \text{ Emissions}}{SO_2 \text{ MERP}}\right) < 1$$

24-Hour Averaging Period

Using Source 36 MERPs: $\left(\frac{8.54}{1.2} + \frac{49.38}{37,589} + \frac{13.74}{21,050}\right) = 7.12 > 1$

Annual Averaging Period

Using Source 36 MERPs: $\left(\frac{4.21}{0.2} + \frac{49.38}{299,905} + \frac{13.74}{32,077}\right) = 21.1 > 1$

Since the ratio for each averaging period is greater than 1, a cumulative impact analysis was performed. To estimate the total concentration of $PM_{2.5}$, $PM_{2.5}$ SILs 24-hour and annual values (i.e., 1.2 $\mu g/m^3$ and 0.2 $\mu g/m^3$ from FIPS 4005) calculated above for secondary $PM_{2.5}$ impacts were added to the $PM_{2.5}$ model results (i.e., primary $PM_{2.5}$ impacts) for comparison to the applicable standards. This is performed for NAAQS modeling.

[12] EPA's April 30, 2024 clarification memo stipulates that the secondary contribution should be calculated using the hypothetical source max modeled concentration instead of the MERP and SIL values. This clarification was made in light of the change to the annual PM2.5 SIL. In order to ensure consistency with previous submissions for the project, the calculations included herein retain the use of the previous MERPs and SIL method using the previous SIL. This results in a calculation of impacts that is consistent with the method described in the April 30, 2024 clarification memo by not making use of the updated SIL value.

$$\text{Secondary } PM_{2.5} \text{ Impact on NAAQS} = \left(PM_{2.5}\ Modeled\ concentration + \ Background\ PM_{2.5}\ concentration + \left(\frac{NO_x \text{ Emissions}}{NO_x \text{ MERP}} + \frac{SO_2 \text{ Emissions}}{SO_2 \text{ MERP}}\right) * \text{SIL}\right) < NAAQS$$

24-Hour Averaging Period

Using Source 36 MERPs: $\left(17.6(includes\ background) + \frac{49.38}{37{,}589} * 1.2 + \frac{13.74}{21{,}050} * 1.2\right) = 17.6 < 35$

Annual Averaging Period

Using Source 36 MERPs: $\left(8.11(includes\ background) + \frac{49.38}{299{,}905} * 0.2 + \frac{13.74}{32{,}077} * 0.2\right) = 8.11 < 9$

The results demonstrate that there is no NAAQS exceedance for fine particulate when incorporating secondary particulate formation.

9.2 Ozone Impact Analysis

Similarly, pursuant to the EPA July 2022 guidance,[13] a proposed project with an increase of NO_x and/or VOC emissions in excess of 40 tpy triggers an ozone air impact analysis.

The O_3 impacts for the source impact assessment were calculated as the sum of the ratio of precursor emissions to the MERPs. If the sum of the ratios is less than 1, then the O_3 impacts are below the O_3 SIL and no cumulative analysis is necessary.

Similar to the secondary $PM_{2.5}$ assessment, Source 36 in Coconino County remains the most representative MERP source. The ratio of the post-project Potential-To-Emit (PTE) to the MERP value is evaluated using the equation given below.

$$\text{Secondary } Ozone \text{ Impact } = \left(\frac{NO_x \text{ Emissions}}{NO_x \text{ MERP}} + \frac{\text{VOC Emissions}}{\text{VOC MERP}}\right) < 1$$

For Source 36: $\left(\frac{49.38}{204} + \frac{13.46}{18{,}982}\right) = 0.24 < 1$

As shown in the calculation above, the Copper World Project facility will not contribute to an increase in ozone above 1 ppb SIL Level; therefore, a cumulative analysis is not required.

[13] Guidance for Ozone and Fine Particulate Matter Permit Modeling, dated July 29, 2022
https://www.epa.gov/system/files/documents/2022-08/2022%20Guidance%20O3%20and%20Fine%20PM%20Modeling.pdf

APPENDIX A. FACILITY LAYOUT GRAPHICS

T.18 S. R.15 E. - S06 | T.18 S. R.15 E. - S05 | T.18 S. R.15 E. - S04 | T.18 S. R.15 E. - S03 | T.18 S. R.15 E. - S02 | T.18 S. R.15 E. - S01

T.18 S. R.15 E. - S07 | T.18 S. R.15 E. - S08 | T.18 S. R.15 E. - S09 | T.18 S. R.15 E. - S10 | T.18 S. R.15 E. - S11 | T.18 S. R.15 E. - S12

T.18 S. R.15 E. - S18 | T.18 S. R.15 E. - S17 | T.18 S. R.15 E. - S16 | T.18 S. R.15 E. - S15 | T.18 S. R.15 E. - S14 | T.18 S. R.15 E. - S13

T.18 S. R.15 E. - S19 | T.18 S. R.15 E. - S20 | T.18 S. R.15 E. - S21 | T.18 S. R.15 E. - S22 | T.18 S. R.15 E. - S23 | T.18 S. R.15 E. - S24

T.18 S. R.15 E. - S30 | T.18 S. R.15 E. - S29 | T.18 S. R.15 E. - S28 | T.18 S. R.15 E. - S27 | T.18 S. R.15 E. - S26 | T.18 S. R.15 E. - S25

TAILINGS FACILITY 1

LIMESTONE MINE

UTILITY CORRIDOR ALONG SANTA RITA ROAD

PEACH PIT

COPPER WORLD PIT

HEAVY WEIGHT PIT

HAUL ROAD

ELGIN PIT

SANTA RITA ROAD

BURIED TAILINGS LINE

HAUL ROAD

FLOTATION AREA

WASTE ROCK FACILITY/ HEAP LEACH PAD

FWDS PUMP STATION No. 2

TAILINGS FACILITY 2

LEGEND

- TOWNSHIP LINE
- GENERAL FACILITY FOOTPRINT
- PRIVATE LAND BOUNDARY
- BURIED TAILINGS LINE
- ROAD
- ROAD NETWORK 90% CONTROL EFFICIENCY
- ROAD NETWORK 95% CONTROL EFFICIENCY

NOTES:

1. FACILITY FOOTPRINT BOUNDARY AND ROADS WILL BE MODIFIED ACCORDING TO THE MINE PLAN.

N

SCALE

1000' 0 1000' 2000'

CONTOUR INTERVAL = 10'

PROJECT:
COPPER WORLD PROJECT

COUNTY: PIMA	STATE: ARIZONA
	DATE: OCTOBER 2023

FIGURE NO. 1
YEAR 2 OF OPERATIONS
ROAD NETWORK CONTROL EFFICIENCIES

HUDBAY

T.18 S. R.15 E. - S06 | T.18 S. R.15 E. - S05 | T.18 S. R.15 E. - S04 | T.18 S. R.15 E. - S03 | T.18 S. R.15 E. - S02 | T.18 S. R.15 E. - S01 | T.18 S. R.16E. - S06 | T.18 S. R.16E. - S05

T.18 S. R.15 E. - S07 | T.18 S. R.15 E. - S08 | T.18 S. R.15 E. - S09 | T.18 S. R.15 E. - S10 | T.18 S. R.15 E. - S11 | T.18 S. R.15 E. - S12 | T.18 S. R.16E. - S07 | T.18 S. R.16E. - S08

T.18 S. R.15 E. - S18 | T.18 S. R.15 E. - S17 | T.18 S. R.15 E. - S16 | T.18 S. R.15 E. - S15 | T.18 S. R.15 E. - S14 | T.18 S. R.15 E. - S13 | T.18 S. R.16E. - S18 | T.18 S. R.16E. - S17

T.18 S. R.15 E. - S19 | T.18 S. R.15 E. - S20 | T.18 S. R.15 E. - S21 | T.18 S. R.15 E. - S22 | T.18 S. R.15 E. - S23 | T.18 S. R.15 E. - S24 | T.18 S. R.16E. - S19 | T.18 S. R.16E. - S20

T.18 S. R.15 E. - S30 | T.18 S. R.15 E. - S29 | T.18 S. R.15 E. - S28 | T.18 S. R.15 E. - S27 | T.18 S. R.15 E. - S26 | T.18 S. R.15 E. - S25 | T.18 S. R.16E. - S30 | T.18 S. R.16E. - S29

T.18 S. R.15 E. - S31 | T.18 S. R.15 E. - S32 | T.18 S. R.15 E. - S33 | T.18 S. R.15 E. - S34 | T.18 S. R.15 E. - S35 | T.18 S. R.15 E. - S36 | T.18 S. R.16E. - S31 | T.18 S. R.16E. - S32

T.19 S. R.15 E. - S06 | T.19 S. R.15 E. - S05 | T.19 S. R.15 E. - S04 | T.19 S. R.15 E. - S03 | T.19 S. R.15 E. - S02 | T.19 S. R.15 E. - S01 | T.19 S. R.16E. - S06 | T.19 S. R.16E. - S07

TAILINGS FACILITY 1

UTILITY CORRIDOR ALONG SANTA RITA ROAD

SANTA RITA ROAD

BURIED TAILINGS LINE

FWDS PUMP STATION No. 2

FLOTATION AREA

TAILINGS FACILITY 2

HEAVY WEIGHT PIT (WASTE ROCK PLACEMENT)

PEACH PIT

ELGIN PIT

WASTE ROCK FACILITY/ HEAP LEACH PAD

HAUL ROAD

LIMESTONE MINE

WASTE ROCK FACILITY

COPPER WORLD PIT (WASTE ROCK PLACEMENT)

HAUL ROAD

BROADTOP BUTTE PIT

ROSEMONT PIT

LEGEND

- TOWNSHIP LINE
- GENERAL FACILITY FOOTPRINT
- PRIVATE LAND BOUNDARY
- BURIED TAILINGS LINE
- ROAD
- ROAD NETWORK 95% CONTROL EFFICIENCY

NOTES:

1. FACILITY FOOTPRINT BOUNDARY AND ROADS WILL BE MODIFIED ACCORDING TO THE MINE PLAN.

N

SCALE

1500' 0 1500' 3000'

CONTOUR INTERVAL = 10'

PROJECT:
COPPER WORLD PROJECT

COUNTY: PIMA | STATE: ARIZONA

DATE: OCTOBER 2023

FIGURE NO. 2
YEAR 8 OF OPERATIONS
ROAD NETWORK CONTROL EFFICIENCIES

HUDBAY

T.18 S. R.15 E. - S06 | T.18 S. R.15 E. - S05 | T.18 S. R.15 E. - S04 | T.18 S. R.15 E. - S03 | T.18 S. R.15 E. - S02 | T.18 S. R.15 E. - S01 | T.18 S. R.16E. - S06 | T.18 S. R.16E. - S05

T.18 S. R.15 E. - S07 | T.18 S. R.15 E. - S08 | T.18 S. R.15 E. - S09 | T.18 S. R.15 E. - S10 | T.18 S. R.15 E. - S11 | T.18 S. R.15 E. - S12 | T.18 S. R.16E. - S07 | T.18 S. R.16E. - S08

T.18 S. R.15 E. - S18 | T.18 S. R.15 E. - S17 | T.18 S. R.15 E. - S16 | T.18 S. R.15 E. - S15 | T.18 S. R.15 E. - S14 | T.18 S. R.15 E. - S13 | T.18 S. R.16E. - S18 | T.18 S. R.16E. - S17

T.18 S. R.15 E. - S19 | T.18 S. R.15 E. - S20 | T.18 S. R.15 E. - S21 | T.18 S. R.15 E. - S22 | T.18 S. R.15 E. - S23 | T.18 S. R.15 E. - S24 | T.18 S. R.16E. - S19 | T.18 S. R.16E. - S20

T.18 S. R.15 E. - S30 | T.18 S. R.15 E. - S29 | T.18 S. R.15 E. - S28 | T.18 S. R.15 E. - S27 | T.18 S. R.15 E. - S26 | T.18 S. R.15 E. - S25 | T.18 S. R.16E. - S30 | T.18 S. R.16E. - S29

T.18 S. R.15 E. - S31 | T.18 S. R.15 E. - S32 | T.18 S. R.15 E. - S33 | T.18 S. R.15 E. - S34 | T.18 S. R.15 E. - S35 | T.18 S. R.15 E. - S36 | T.18 S. R.16E. - S31 | T.18 S. R.16E. - S32

T.19 S. R.15 E. - S06 | T.19 S. R.15 E. - S05 | T.19 S. R.15 E. - S04 | T.19 S. R.15 E. - S03 | T.19 S. R.15 E. - S02 | T.19 S. R.15 E. - S01 | T.19 S. R.16E. - S06 | T.19 S. R.16E. - S07

UTILITY CORRIDOR ALONG SANTA RITA ROAD

SANTA RITA ROAD

BURIED TAILINGS LINE

FWDS PUMP STATION No. 2

FLOTATION AREA

TAILINGS FACILITY 1

TAILINGS FACILITY 2

WASTE ROCK FACILITY/ HEAP LEACH PAD

PEACH PIT

ELGIN PIT

HAUL ROAD

LIMESTONE MINE

HEAVY WEIGHT PIT (WASTE ROCK PLACEMENT)

WASTE ROCK FACILITY

COPPER WORLD PIT (WASTE ROCK PLACEMENT)

BROADTOP BUTTE PIT (WASTE ROCK PLACEMENT)

HAUL ROAD

ROSEMONT PIT

LEGEND

- TOWNSHIP LINE
- GENERAL FACILITY FOOTPRINT
- PRIVATE LAND BOUNDARY
- BURIED TAILINGS LINE
- ROAD
- ROAD NETWORK 90% CONTROL EFFICIENCY
- ROAD NETWORK 95% CONTROL EFFICIENCY

NOTES:

1. FACILITY FOOTPRINT BOUNDARY AND ROADS WILL BE MODIFIED ACCORDING TO THE MINE PLAN.

N

SCALE

1500' 0 1500' 3000'

CONTOUR INTERVAL = 10'

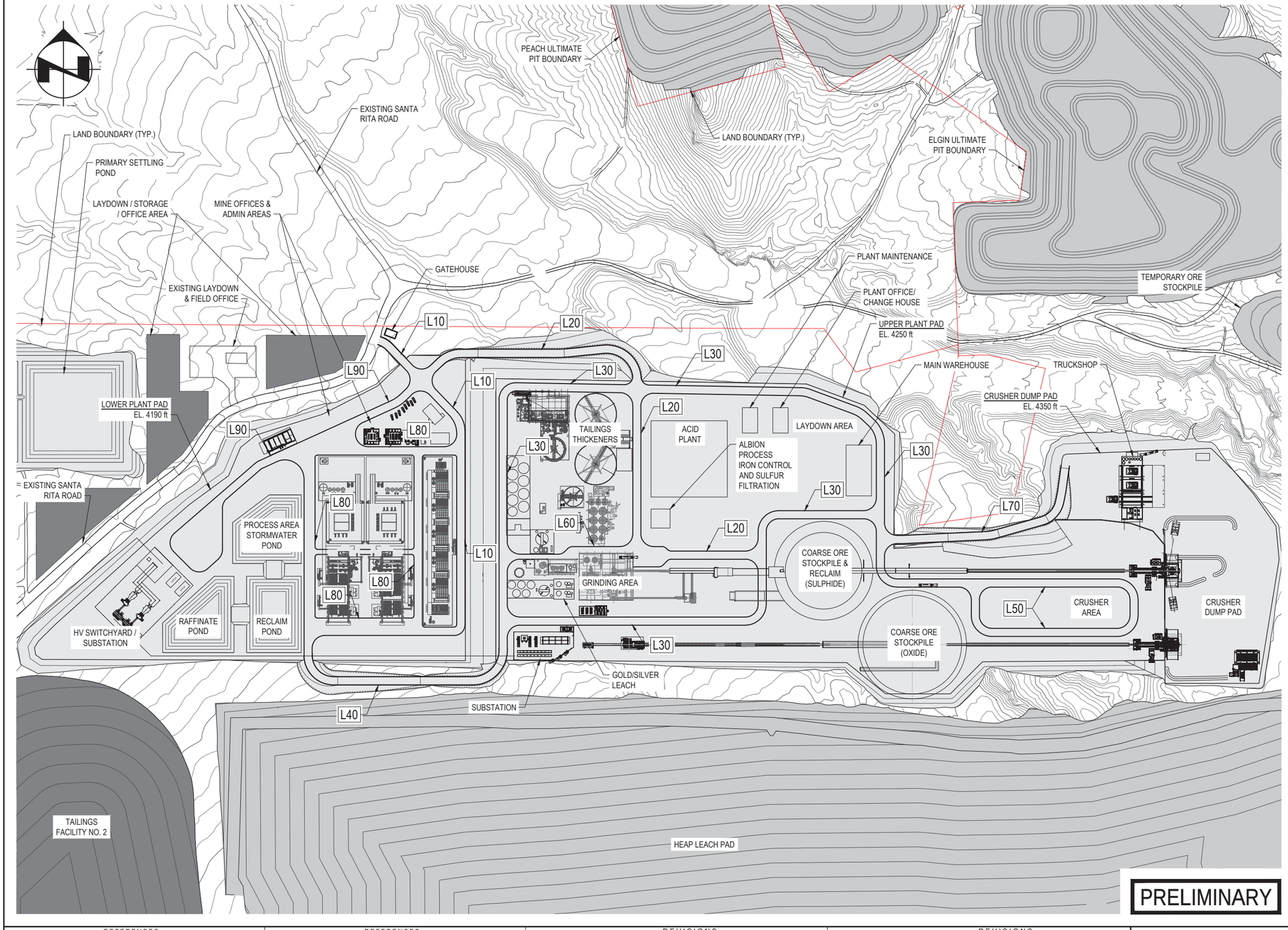
PROJECT:
COPPER WORLD PROJECT

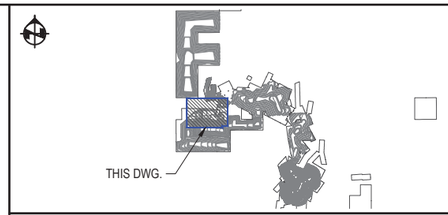
COUNTY: PIMA | STATE: ARIZONA

DATE: OCTOBER 2023

FIGURE NO. 3
YEAR 14 OF OPERATIONS
ROAD NETWORK CONTROL EFFICIENCIES

HUDBAY





KEY PLAN

GRAVEL IN-PLANT ROADS

NAME:	DESCRIPTION:	LANES:	LENGTH:
L10	ACCESS ROAD FROM SANTA RITA ROAD TO LOWER PLANT PAD AND ELECTROWINNING & SOLVENT EXTRACTION AREAS	2	1430'
L20	ACCESS ROAD TO UPPER PLANT PAD AND GRINDING AREA	2	2100'
L30	ACCESS ROAD LOOP AROUND GRINDING, TAILINGS, LAYDOWN AND CONCENTRATE AREAS	2	4560'
L40	ACCESS ROAD TO LOWER PLANT AREA AND ELECTROWINNING & SOLVENT EXTRACTION AREAS	2	1110'
L50	ACCESS ROAD LOOP TO LOWER CRUSHER AREA	2	2165'
L60	ACCESS ROAD THROUGH GRINDING AREA	1	535'
L70	ACCESS ROAD TO CRUSHER DUMP PAD AND TRUCKSHOP	2	895'
L80	ACCESS ROAD LOOP AROUND ELECTROWINNING & SOLVENT EXTRACTION AREAS	2	2430'
L90	ACCESS ROAD TO MINE OFFICE AND ADMINISTRATION AREA	2	1130'
		TOTAL:	16355'

NOTES:

1. ALL DIMENSIONS ARE IN FEET UNLESS OTHERWISE NOTED.
2. ALL ROADS ARE UNPAVED GRAVEL UNLESS OTHERWISE NOTED.

LEGEND:

EXISTING GROUND MAJOR CONTOUR (25')

EXISTING GROUND MINOR CONTOUR (5')

200' 0 200' 400' 600' 800'

SCALE: 1"=200'

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W www.ausenco.com

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Safety Rules

REFERENCES

DWG. NO.	TITLE

REFERENCES

DWG. NO.	TITLE

REVISIONS

NO.	BY	CKD	APP	CLIENT	DATE	DESCRIPTION

REVISIONS

NO.	BY	CKD	APP	CLIENT	DATE	DESCRIPTION
A	IAC	SM			11FEB22	PRELIMINARY ISSUE
B	IAC	SM			23FEB22	ISSUED FOR STUDY
C	JC	SM			02MAY22	AREAS ADDED

HUDBAY
ROSEMONT COPPER WORLD COMPANY

ROSEMONT COPPER WORLD PROJECT

ROADS
CIVIL
PLANT SITE
GENERAL ARRANGMENT - SHEET 2

CONTRACTOR DWG. NO. 106075-5200-B-101
DWG. NO. - FIGURE NO. 4
REVISION C
DATE 02MAY2022

LEGEND

- EXISTING ROAD
- BURIED TAILINGS LINE
- PROPERTY BOUNDARY

NOTE:

1. AMSL = ABOVE MEAN SEA LEVEL.

N

SCALE

200' 0 200' 400'

PROJECT:
ROSEMONT COPPER WORLD PROJECT

COUNTY: PIMA | STATE: ARIZONA

DATE: APRIL 2022

FIGURE 1
PROPOSED PROJECT FACILITIES
PLANT SITE AREA

HUDBAY

APPENDIX B. PM_{10} SUMMARY AND NATURAL EVENTS DOCUMENTATION

Step 2 - CDT Compute monthly maximum 24-hour concentration each year

Monthly maximum

Month	2019	2020	2021	Post Removal Maximum	Event Removal Description	Date of Impact
1	13	19	63	19	Frontal Passage - Wind Blown Dust Event - Gusts to 40MPH	1/19/2021
2	11	40	24	40		
3	32	24	32	32		
4	40	21	60	40	Frontal Passage - Wind Blown Dust Event - Gusts to 40MPH	4/1/2021
5	31	29	21	31		
6	24	29	40	40		
7	24	28	52	28	Storm Gust - Wind Blown Dust Event - Intermittent Gusts to 43MPH	7/12/2021
8	28	39	16	39		
9	14	53	32	53		
10	58	64	30	30	Storm Gusts - Wind Blown Dust Event - Gusts to 31MPH intermittent all day (10/26/2020) and Storm Gusts - Wind Blown Dust Event - Gusts to 38MPH intermittent all day (10/25/2019)	10/26/2020 and 10/25/2019
11	56	61	39	39	Frontal Passage - Wind Blown Dust Event - Gusts to 43MPH (11/7 and into 11/8/2020) - Storm Gusts - Wind Blown Dust Event - Gusts to 44MPH intermittent all day (11/12/2019)	11/8/2020 and 11/12/2019
12	17	30	27	30		

Step 1 - Determine highest ~~five~~ 24-hour concentrations from 3-year data set and remove from consideration

High	2019	2020	2021
1	58	64	63
2	56	61	60
3	40	53	52
4	39	43	40
5	36	42	39
6	32	40	36

Step 2 - Compute monthly maximum 24-hour concentration each year

		Monthly maximum				**Date of Impact**
Month	2019	2020	2021	Post Removal Maximum	Event Removal Description	
1	13.0	19.0	63.0	19.0	Frontal Passage - Wind Blown Dust Event - Gusts to 40MPH	1/19/2021
2	11.0	40.0	24.0	40.0		
3	32.0	24.0	32.0	32.0		
4	40.0	21.0	60.0	40.0	Frontal Passage - Wind Blown Dust Event - Gusts to 40MPH	4/1/2021
5	31.0	29.0	21.0	31.0		
6	24.0	29.0	40.0	40.0		
7	24.0	28.0	52.0	28.0	Storm Gust - Wind Blown Dust Event - Intermittent Gusts to 43MPH	7/12/2021
8	28.0	39.0	16.0	39.0		
9	14.0	53.0	32.0	53.0		
10	58.0	64.0	30.0	30.0	Storm Gusts - Wind Blown Dust Event - Gusts to 31MPH intermittent all day (10/26/2020) and Storm Gusts - Wind Blown Dust Event - Gusts to 38MPH intermittent all day (10/25/2019)	10/26/2020 and 10/25/2019
11	56.0	61.0	39.0	39.0	Frontal Passage - Wind Blown Dust Event - Gusts to 43MPH (11/7 and into 11/8/2020) - Storm Gusts - Wind Blown Dust Event - Gusts to 44MPH intermittent all day (11/12/2019)	11/8/2020 and 11/12/2019
12	17.0	30.0	27.0	30.0		

Step 3 - Determine maximum value for each season, maximum of included years

Seasonal Maximum	
Dec - Feb	17.0
Mar - May	40.0
Jun - Aug	28.0
Sep - Nov	58.0

Trinity Consultants
702 W Idaho St, Ste 1100, Boise, ID 83702 / P 208.472.8837 / F 678.441.9978 / **trinityconsultants.com**

September, 2022

Mr. Feng Mao
Arizona Dept. of Environmental Quality
1110 West Washington Street
Phoenix, AZ 85007

RE: Natural Events Removal for Corona De Tucson PM10 Ambient Air Quality Monitoring.

Dear Mr. Mao:

The purpose of this letter is to provide an analysis of the PM_{10} ambient concentration data at the Corona De Tucson monitor to be used as background concentrations in the demonstration of compliance with the 24-hr PM_{10} National Ambient Air Quality Standard. Specifically, seven days (January 19, 2021, April 1, 2021, July 12, 2021, October 26, 2020, November 8, 2020, October 25, 2019, and November 12, 2019) were evaluated for the Rosemont Copper Company (Rosemont) permit application for the Rosemont Class II Permit Renewal/Modification Application that incorporates the Rosemont Copper Project and the Rosemont Copper World Project (Rosemont Projects), to see if they should be excluded pursuant to the natural events policy.

Background PM_{10} Concentrations for Demonstrating 24-hr PM_{10} NAAQS Compliance

Arizona Department of Environmental Quality (ADEQ) has tentatively agreed with the approach of using the Tucson site's monthly PM_{10} concentrations to represent the background values for the Rosemont Projects analyses. However, Rosemont has requested that the monitored PM_{10} concentration from seven days during the 3-year baseline period be excluded. ADEQ requested that these days be scrutinized to see if they meet the natural events policy in order to be excluded.

The monitored values of PM_{10} on January 19, 2021, April 1, 2021, July 12, 2021, October 26, 2020, November 8, 2020, October 25, 2019, and November 12, 2019 (the requested dates), at the Corona De Tucson monitor are significantly higher than typical readings for this site. The monitored values do not exceed the NAAQS for 24-hour PM_{10}, but the discrepancy is great enough that including these values in air quality analyses at Rosemont Copper World Project will unnecessarily bias the results by including periods impacted by natural windblown dust events. Trinity Consultants Inc. (Trinity) proposes to exclude these seven days from the background monitor value calculation using the guidelines included in the Technical Criteria Documents for Determination of Natural and Exceptional Events published on May 31, 2000, February 10, 2005, and December 12, 2005.

The requested dates episodes met the criteria described in the December 12, 2005, guidance. The analytical framework and how it applies to the requested dates episodes are described below.

Step 1 – Properly Qualify and Validate the Air Quality Measurements to be Flagged

Trinity reviewed PM_{10} data from the most representative monitor for the requested dates from EPA's AQS database. Trinity considers the EPA AQS database to be a quality-assured source of the data for this proposal. A description of the monitor with its location, objectives, and operation dates is provided in Table 1 through Table 7. All of the monitors are within 92 km surrounding the Rosemont Projects. They represent

data collection on a variety of scales, which should provide a comprehensive picture of PM_{10} levels in the Tucson area. All of the monitors were established before 2019 and are still currently monitoring PM_{10}. Therefore, none of the data is in question due to initial setup of the monitors or faulty monitors that needed to be removed from service. One monitor (040191026) records values every sixth day. The values shown in Table 1 through Table 7 from this monitor are the days closest to the requested dates.

PM_{10} levels at the Corona De Tucson monitor were examined from January 2019 to December 2021. The monitor is located 18 km from Rosemont Copper Project and 16.5 km from the Rosemont Copper World Project. The 24-hr measurements for the three-year time period are shown in Figure 1. The monitor values shows that the three-year average of 24-hr PM_{10} levels at the site was 14 $\mu g/m^3$ and the 95th percentile was 28 $\mu g/m^3$.

January 19, 2021

The monitored value on January 19, 2021, is 63 $\mu g/m^3$. 49 $\mu g/m^3$ higher that the three-year average and 35 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

April 1, 2021

The monitored value on April 1, 2021, is 60 $\mu g/m^3$. 46 $\mu g/m^3$ higher that the three-year average and 32 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

July 12, 2021

The monitored value on July 12, 2021, is 52 $\mu g/m^3$. 38 $\mu g/m^3$ higher that the three-year average and 24 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

October 26, 2020

The monitored value on October 26, 2020, is 64 $\mu g/m^3$. 50 $\mu g/m^3$ higher that the three-year average and 36 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

November 8, 2020

The monitored value on November 8, 2020, is 61 $\mu g/m^3$. 47 $\mu g/m^3$ higher that the three-year average and 33 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

October 25, 2019

The monitored value on October 25, 2019, is 58 $\mu g/m^3$. 44 $\mu g/m^3$ higher that the three-year average and 30 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

November 12, 2019

The monitored value on November 12, 2019, is 56 $\mu g/m^3$. 42 $\mu g/m^3$ higher that the three-year average and 28 $\mu g/m^3$ higher than the 95th percentile value. Trinity considers this discrepancy to be significant and elected to continue the analysis to determine potential causes.

Step 2 – Review Suspected Contributing Sources

Trinity performed an initial examination of sources locations to demonstrate that the PM_{10} levels at the Corona De Tucson monitor were significantly higher on the requested dates than normal for the site. Trinity reviewed the meteorological wind data from the Tucson International Airport for the requested dates. Table 8 below shows the average wind speed and wind gusts, along with the maximum wind gusts on each requested date. The cause of the winds were a combination of synoptic frontal passages and mesoscale storm gusts. Based on this assessment, these dates would qualify as natural exceptional events for high winds.

Step 3 – Examine All Air Quality Monitoring Information

Natural events due to windblown dust were identified on EPA's web site at the Corona De Tucson monitor on all the requested dates. In addition, daily average PM_{10} concentrations for the requested dates were collected for all the monitors in Table 1 through Table 7. All these sites reported concentrations above the 95^{th} percentile for PM_{10} over the three-year period. Local wind speeds were not extremely high, but for each of the requested days high speed, intermittent gusts were recorded. The high wind gusts elevated PM_{10} levels throughout the region surrounding Rosemont.

Step 4 – Examine the Meteorological Conditions Before and During the Event

Trinity reviewed the meteorological data from the University of Utah MesoWest & Synoptic Data. Wind speeds and gusts were recorded for every three minutes for all requested dates other than November 8, 2020, which has data recorded every hour. Data was also reviewed for the day before each requested date. The wind data is included in Attachment 1. High winds in the Tucson region recorded on the requested dates support the results of increased PM_{10} due to natural windblown dust.

Step 5 – Perform a Qualitative Attribution to Emission Sources

PM_{10} levels were elevated at all monitors in the region surrounding the Corona De Tucson monitor. The high wind levels recorded by the Tucson International Airport monitor support that the high PM_{10} levels were caused by natural windblown dust events.

Step 6 – Estimation of Contribution from Sources

Dust transported by high winds in the Tucson region likely contributed to the high PM_{10} levels measured in the region around the site. The contribution from these sources was determined using the three years of PM_{10} measurement data from the Corona De Tucson monitor. The three-year average concentration was 14 $\mu g/m^3$ and the 95^{th} percentile concentration was 28 $\mu g/m^3$. The concentration on January 19, 2021, April 1, 2021, July 12, 2021, October 26, 2020, November 8, 2020, October 25, 2019, and November 12, 2019, were 63 $\mu g/m^3$, 60 $\mu g/m^3$, 52 $\mu g/m^3$, 64 $\mu g/m^3$, 61 $\mu g/m^3$, 58 $\mu g/m^3$, and 56 $\mu g/m^3$, respectively. Trinity proposes that the difference between the 95^{th} percentile and the value on the requested dates was the contribution from natural or exceptional sources.

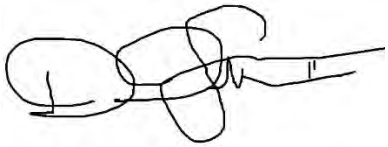
Step 7 – Determination that a Natural or Exceptional Event Contributed to an Exceedance

The monitors near the Corona De Tucson monitor did not exceed the NAAQS on the requested dates. However, the concentration was significantly higher than typical concentrations in the area. Including the requested dates in the background would significantly alter the air quality analysis for the Rosemont Copper

World Project. Trinity proposes that the PM_{10} monitored values on the requested dates be excluded based on the presented evidence that they were exceptional events resulting in windblown dust in the Tucson region.

Please let us know if ADEQ requires further information in this determination. We look forward to the results of your review of this information. If you have any questions or comments concerning the information provided, please contact me.

Sincerely,
TRINITY CONSULTANTS



David Strohm
Managing Consultant

Attachments: 1. MesoWest Wind Data

cc: Hudbay Minerals, Inc.

Table 1. Jan 19, 2021 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 1/19/2021 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**63**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	69
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	209
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	105
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	75
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	42
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	36*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	42
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	80

Table 2. April 1, 2021 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 4/1/2021 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**60**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	59
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	177
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	63
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	60
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	42
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	24*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	33
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	58

Table 3. July 12, 2021 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 7/12/2021 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**52**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	62
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	90
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	60
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	62
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	62
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	31*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	35
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	55

Table 4. October 26, 2020 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 10/26/2020 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**64**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	73
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	86
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	70
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	87
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	74
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	30*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	61
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	78

Table 5. November 8, 2020 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 11/8/2020 (µg/m³)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**61**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	55
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	62
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	64
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	63
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	57
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	20*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	47
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	47

Table 6. October 25, 2019 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 10/25/2019 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**58**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	29
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	48
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	45
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	55
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	18
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	25*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	29
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	29

Table 7. November 12, 2019 EPA Data

Site	Latitude	Longitude	Monitor Type	Scale	Dominant Source Type	Monitoring Objective	Site Established	Monitored Value on 11/12/2019 ($\mu g/m^3$)
040190008	**32.004707**	**-110.792593**	**SLAMS**	**Regional**	**-**	**Background**	**3/1/1987**	**56**
040190011	32.322661	-111.038389	SLAMS	Neighborhood	-	Highest Conc.	7/1/2017	39
040190020	32.414344	-111.154544	SLAMS	Middle	-	-	4/1/2010	64
040191001	32.201978	-110.967905	SLAMS	Neighborhood	-	Pop. Exposure	10/1/2017	51
040191113	32.251843	-110.965293	SLAMS	Neighborhood	-	-	7/1/2007	38
040191018	32.425261	-111.063520	SLAMS	Urban	-	Background	1/1/1994	29
040191026	32.125919	-110.982556	SLAMS	Neighborhood	-	Pop. Exposure	3/30/1994	27*
040191030	31.879520	-110.996440	SLAMS	Neighborhood	-	Pop. Exposure	2/13/2001	21
040213007	32.508306	-111.308056	SLAMS	Regional	Area	Regional Transport	6/7/2012	43

Figure 1. Corona De Tucson (2019-2021)

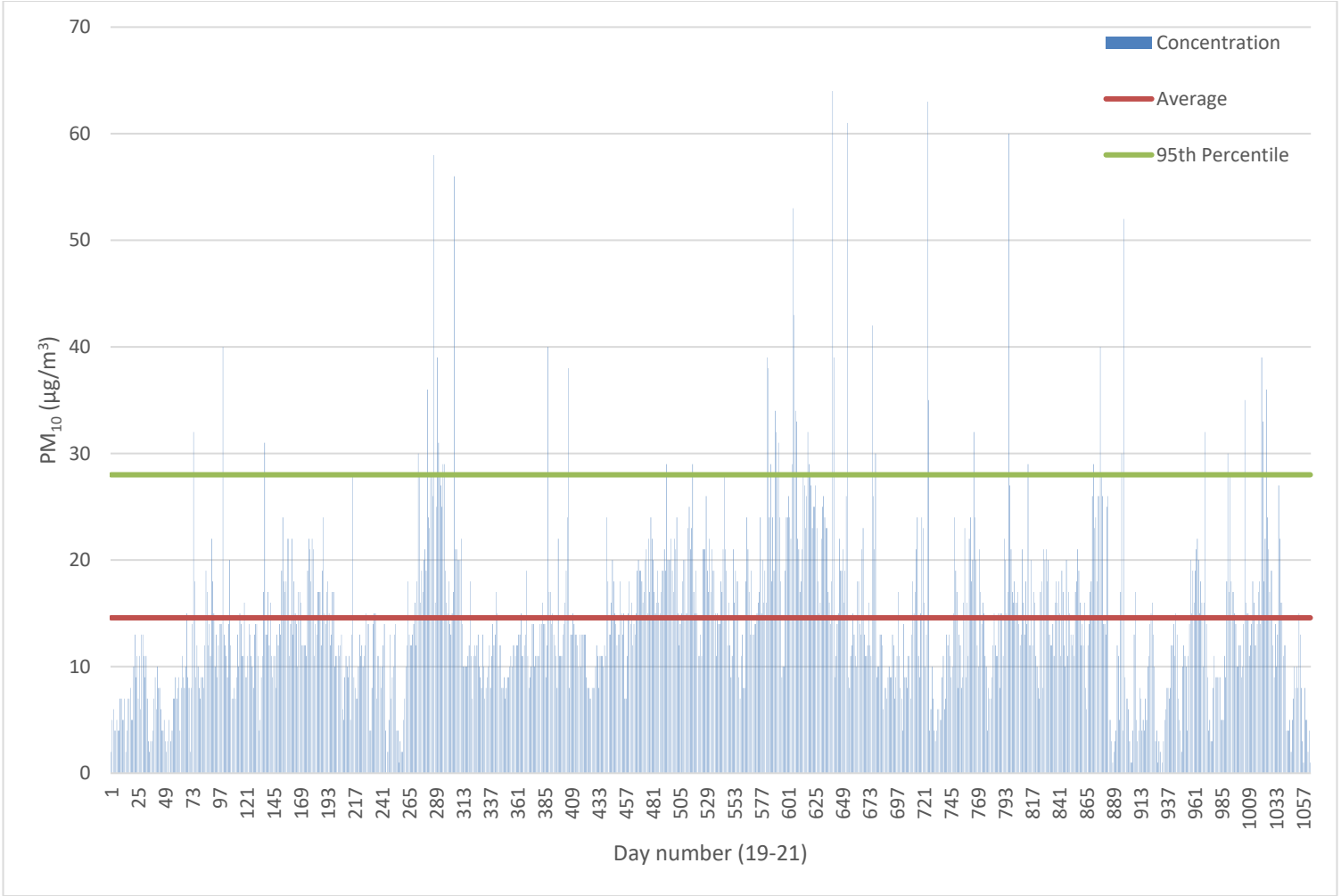


Table 8. Daily Wind Speed and Gusts

Date	Cause	Average Wind Speed	Average Wind Gust	Maximum Wind Gust
1/19/2021	Frontal Passage	10.69	31.22	43.73
4/1/2021	Frontal Passage	17.29	28.49	39.13
7/12/2021	Storm Gusts	9.76	23.84	42.58
10/26/2020	Storm Gusts	10.00	22.64	31.07
11/8/2020	Frontal Passage	9.69	24.27	32.22
10/25/2019	Storm Gusts	14.25	27.58	37.90
11/12/2019	Storm Gusts	14.55	27.734	43.73

STATION: KTUS
STATION Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	10/24/2019 22:00 MST	0	0	
KTUS	10/24/2019 22:05 MST	4.61	40	
KTUS	10/24/2019 22:10 MST	5.75	100	
KTUS	10/24/2019 22:15 MST	5.75	100	
KTUS	10/24/2019 22:20 MST	5.75	100	
KTUS	10/24/2019 22:25 MST	6.91	130	
KTUS	10/24/2019 22:30 MST	5.75	110	
KTUS	10/24/2019 22:35 MST	8.05	90	
KTUS	10/24/2019 22:40 MST	5.75	110	
KTUS	10/24/2019 22:45 MST	0	0	
KTUS	10/24/2019 22:50 MST	3.44	340	
KTUS	10/24/2019 22:53 MST	3.44	330	
KTUS	10/24/2019 22:55 MST	3.44	320	
KTUS	10/24/2019 23:00 MST	0	0	
KTUS	10/24/2019 23:05 MST	0	0	
KTUS	10/24/2019 23:10 MST	0	0	
KTUS	10/24/2019 23:15 MST	0	0	
KTUS	10/24/2019 23:20 MST	3.44	80	
KTUS	10/24/2019 23:25 MST	0	0	
KTUS	10/24/2019 23:30 MST			
KTUS	10/24/2019 23:35 MST	5.75	140	
KTUS	10/24/2019 23:40 MST	6.91	140	
KTUS	10/24/2019 23:45 MST	9.22	160	
KTUS	10/24/2019 23:50 MST	8.05	170	
KTUS	10/24/2019 23:53 MST	6.91	160	
KTUS	10/24/2019 23:55 MST	5.75	170	
KTUS	10/25/2019 00:00 MST	5.75	170	
KTUS	10/25/2019 00:05 MST	3.44	160	
KTUS	10/25/2019 00:10 MST	4.61	180	
KTUS	10/25/2019 00:15 MST	3.44	160	
KTUS	10/25/2019 00:20 MST	8.05	170	
KTUS	10/25/2019 00:25 MST	6.91	150	
KTUS	10/25/2019 00:30 MST	8.05	140	
KTUS	10/25/2019 00:35 MST	6.91	140	
KTUS	10/25/2019 00:40 MST	5.75	120	
KTUS	10/25/2019 00:45 MST	5.75	120	
KTUS	10/25/2019 00:50 MST	5.75	100	
KTUS	10/25/2019 00:53 MST	9.22	110	
KTUS	10/25/2019 00:55 MST	8.05	120	
KTUS	10/25/2019 01:00 MST	5.75	170	
KTUS	10/25/2019 01:05 MST	5.75	170	
KTUS	10/25/2019 01:10 MST	8.05	170	
KTUS	10/25/2019 01:15 MST	8.05	170	
KTUS	10/25/2019 01:20 MST	5.75	170	

KTUS	10/25/2019 01:25 MST	4.61	150	
KTUS	10/25/2019 01:30 MST	0	0	
KTUS	10/25/2019 01:35 MST			
KTUS	10/25/2019 01:40 MST	5.75	170	
KTUS	10/25/2019 01:45 MST	4.61	130	
KTUS	10/25/2019 01:50 MST	5.75	180	
KTUS	10/25/2019 01:53 MST	5.75	170	
KTUS	10/25/2019 01:55 MST	6.91	150	
KTUS	10/25/2019 02:00 MST	6.91	160	
KTUS	10/25/2019 02:05 MST	6.91	150	
KTUS	10/25/2019 02:10 MST	3.44	120	
KTUS	10/25/2019 02:15 MST	4.61	120	
KTUS	10/25/2019 02:20 MST	3.44	90	
KTUS	10/25/2019 02:25 MST	3.44	100	
KTUS	10/25/2019 02:30 MST	4.61	160	
KTUS	10/25/2019 02:35 MST	8.05	140	
KTUS	10/25/2019 02:40 MST	5.75	130	
KTUS	10/25/2019 02:45 MST	3.44	90	
KTUS	10/25/2019 02:50 MST	4.61	110	
KTUS	10/25/2019 02:53 MST	4.61	140	
KTUS	10/25/2019 02:55 MST	3.44	150	
KTUS	10/25/2019 03:00 MST	6.91	140	
KTUS	10/25/2019 03:05 MST	8.05	120	
KTUS	10/25/2019 03:10 MST	6.91	90	
KTUS	10/25/2019 03:15 MST	11.5	90	
KTUS	10/25/2019 03:20 MST	10.36	90	
KTUS	10/25/2019 03:25 MST	14.97	90	20.71
KTUS	10/25/2019 03:30 MST	13.8	90	
KTUS	10/25/2019 03:35 MST	12.66	100	
KTUS	10/25/2019 03:40 MST	10.36	110	
KTUS	10/25/2019 03:45 MST	11.5	110	
KTUS	10/25/2019 03:50 MST	14.97	110	
KTUS	10/25/2019 03:53 MST	13.8	110	
KTUS	10/25/2019 03:55 MST	11.5	100	17.27
KTUS	10/25/2019 04:00 MST	11.5	90	
KTUS	10/25/2019 04:05 MST	12.66	100	
KTUS	10/25/2019 04:10 MST	12.66	90	
KTUS	10/25/2019 04:15 MST	11.5	90	
KTUS	10/25/2019 04:20 MST	13.8	90	
KTUS	10/25/2019 04:25 MST	12.66	90	
KTUS	10/25/2019 04:30 MST	14.97	110	
KTUS	10/25/2019 04:35 MST	14.97	110	21.85
KTUS	10/25/2019 04:40 MST	12.66	110	
KTUS	10/25/2019 04:45 MST	16.11	110	24.16
KTUS	10/25/2019 04:50 MST	16.11	110	
KTUS	10/25/2019 04:53 MST	14.97	110	25.32
KTUS	10/25/2019 04:55 MST	14.97	110	20.71
KTUS	10/25/2019 05:00 MST	17.27	120	26.46
KTUS	10/25/2019 05:05 MST	18.41	120	24.16
KTUS	10/25/2019 05:10 MST	19.57	120	31.07
KTUS	10/25/2019 05:15 MST	20.71	110	27.63
KTUS	10/25/2019 05:20 MST	13.8	120	

KTUS	10/25/2019 05:25 MST	16.11	120	21.85
KTUS	10/25/2019 05:30 MST	20.71	120	29.93
KTUS	10/25/2019 05:35 MST	18.41	110	27.63
KTUS	10/25/2019 05:40 MST	19.57	120	
KTUS	10/25/2019 05:45 MST	18.41	110	29.93
KTUS	10/25/2019 05:50 MST	18.41	120	28.77
KTUS	10/25/2019 05:53 MST	19.57	120	32.21
KTUS	10/25/2019 05:55 MST	20.71	110	32.21
KTUS	10/25/2019 06:00 MST	17.27	110	27.63
KTUS	10/25/2019 06:05 MST	16.11	110	23.02
KTUS	10/25/2019 06:10 MST	16.11	110	25.32
KTUS	10/25/2019 06:15 MST	16.11	110	
KTUS	10/25/2019 06:20 MST	17.27	120	24.16
KTUS	10/25/2019 06:25 MST	20.71	120	
KTUS	10/25/2019 06:30 MST	18.41	120	26.46
KTUS	10/25/2019 06:35 MST	17.27	120	23.02
KTUS	10/25/2019 06:40 MST	17.27	120	25.32
KTUS	10/25/2019 06:45 MST	16.11	100	
KTUS	10/25/2019 06:50 MST	6.91	70	
KTUS	10/25/2019 06:53 MST	10.36	90	26.46
KTUS	10/25/2019 06:55 MST	8.05	90	
KTUS	10/25/2019 07:00 MST	12.66	120	18.41
KTUS	10/25/2019 07:05 MST	13.8	110	
KTUS	10/25/2019 07:10 MST	14.97	120	23.02
KTUS	10/25/2019 07:15 MST	20.71	120	27.63
KTUS	10/25/2019 07:20 MST	17.27	120	23.02
KTUS	10/25/2019 07:25 MST	17.27	120	26.46
KTUS	10/25/2019 07:30 MST	17.27	120	28.77
KTUS	10/25/2019 07:35 MST	17.27	120	23.02
KTUS	10/25/2019 07:40 MST	14.97	110	24.16
KTUS	10/25/2019 07:45 MST	12.66	90	
KTUS	10/25/2019 07:50 MST	12.66	100	18.41
KTUS	10/25/2019 07:53 MST	13.8	120	26.46
KTUS	10/25/2019 07:55 MST	23.02	120	32.21
KTUS	10/25/2019 08:00 MST	24.16	130	29.93
KTUS	10/25/2019 08:05 MST	20.71	130	26.46
KTUS	10/25/2019 08:10 MST	21.85	130	28.77
KTUS	10/25/2019 08:15 MST	23.02	120	31.07
KTUS	10/25/2019 08:20 MST	25.32	130	33.38
KTUS	10/25/2019 08:25 MST	27.63	130	
KTUS	10/25/2019 08:30 MST	28.77	130	35.68
KTUS	10/25/2019 08:35 MST	25.32	130	32.21
KTUS	10/25/2019 08:40 MST	21.85	120	29.93
KTUS	10/25/2019 08:45 MST	23.02	130	29.93
KTUS	10/25/2019 08:50 MST	19.57	120	26.46
KTUS	10/25/2019 08:53 MST	21.85	130	33.38
KTUS	10/25/2019 08:55 MST	23.02	120	31.07
KTUS	10/25/2019 09:00 MST	21.85	120	28.77
KTUS	10/25/2019 09:05 MST	18.41	120	28.77
KTUS	10/25/2019 09:10 MST	19.57	120	28.77
KTUS	10/25/2019 09:15 MST	17.27	120	23.02
KTUS	10/25/2019 09:20 MST	21.85	120	28.77

KTUS	10/25/2019 09:25 MST	26.46	130	
KTUS	10/25/2019 09:30 MST	23.02	130	28.77
KTUS	10/25/2019 09:35 MST	24.16	120	29.93
KTUS	10/25/2019 09:40 MST	27.63	130	37.98
KTUS	10/25/2019 09:45 MST	25.32	130	34.52
KTUS	10/25/2019 09:50 MST	23.02	120	
KTUS	10/25/2019 09:53 MST	24.16	130	37.98
KTUS	10/25/2019 09:55 MST	23.02	120	33.38
KTUS	10/25/2019 10:00 MST	19.57	120	27.63
KTUS	10/25/2019 10:05 MST	24.16	120	31.07
KTUS	10/25/2019 10:10 MST	27.63	120	33.38
KTUS	10/25/2019 10:15 MST	25.32	120	
KTUS	10/25/2019 10:20 MST	24.16	130	31.07
KTUS	10/25/2019 10:25 MST	23.02	130	
KTUS	10/25/2019 10:30 MST	26.46	120	32.21
KTUS	10/25/2019 10:35 MST	24.16	120	35.68
KTUS	10/25/2019 10:40 MST	25.32	130	32.21
KTUS	10/25/2019 10:45 MST	26.46	130	
KTUS	10/25/2019 10:50 MST	28.77	130	
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KTUS	10/25/2019 11:00 MST	23.02	120	35.68
KTUS	10/25/2019 11:05 MST	27.63	120	37.98
KTUS	10/25/2019 11:10 MST	21.85	120	29.93
KTUS	10/25/2019 11:15 MST	21.85	120	35.68
KTUS	10/25/2019 11:20 MST	24.16	130	
KTUS	10/25/2019 11:25 MST	21.85	120	29.93
KTUS	10/25/2019 11:30 MST	23.02	120	
KTUS	10/25/2019 11:35 MST	27.63	130	34.52
KTUS	10/25/2019 11:40 MST	19.57	120	28.77
KTUS	10/25/2019 11:45 MST	24.16	130	29.93
KTUS	10/25/2019 11:50 MST	20.71	120	
KTUS	10/25/2019 11:53 MST	21.85	110	34.52
KTUS	10/25/2019 11:55 MST	23.02	110	31.07
KTUS	10/25/2019 12:00 MST	24.16	130	29.93
KTUS	10/25/2019 12:05 MST	20.71	110	26.46
KTUS	10/25/2019 12:10 MST	25.32	120	35.68
KTUS	10/25/2019 12:15 MST	21.85	120	27.63
KTUS	10/25/2019 12:20 MST	24.16	130	33.38
KTUS	10/25/2019 12:25 MST	23.02	120	
KTUS	10/25/2019 12:30 MST	18.41	120	24.16
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KTUS	10/25/2019 12:45 MST	25.32	120	
KTUS	10/25/2019 12:50 MST	24.16	130	32.21
KTUS	10/25/2019 12:53 MST	19.57	120	33.38
KTUS	10/25/2019 12:55 MST	14.97	110	26.46
KTUS	10/25/2019 13:00 MST	20.71	120	29.93
KTUS	10/25/2019 13:05 MST	20.71	130	
KTUS	10/25/2019 13:10 MST	20.71	110	
KTUS	10/25/2019 13:15 MST	19.57	120	27.63
KTUS	10/25/2019 13:20 MST	20.71	110	29.93

KTUS	10/25/2019 13:25 MST	17.27	120	23.02
KTUS	10/25/2019 13:30 MST	17.27	110	24.16
KTUS	10/25/2019 13:35 MST	18.41	130	
KTUS	10/25/2019 13:40 MST	16.11	120	21.85
KTUS	10/25/2019 13:45 MST	17.27	100	23.02
KTUS	10/25/2019 13:50 MST	14.97	110	21.85
KTUS	10/25/2019 13:53 MST	17.27	120	27.63
KTUS	10/25/2019 13:55 MST	16.11	130	24.16
KTUS	10/25/2019 14:00 MST	10.36	80	
KTUS	10/25/2019 14:05 MST	14.97	120	24.16
KTUS	10/25/2019 14:10 MST	12.66	80	
KTUS	10/25/2019 14:15 MST	4.61	90	
KTUS	10/25/2019 14:20 MST			
KTUS	10/25/2019 14:25 MST	11.5	80	
KTUS	10/25/2019 14:30 MST	8.05	90	
KTUS	10/25/2019 14:35 MST	9.22	110	
KTUS	10/25/2019 14:40 MST	18.41	130	
KTUS	10/25/2019 14:45 MST	16.11	120	
KTUS	10/25/2019 14:50 MST	13.8	140	
KTUS	10/25/2019 14:53 MST	11.5	90	24.16
KTUS	10/25/2019 14:55 MST	11.5	110	
KTUS	10/25/2019 15:00 MST	10.36	60	
KTUS	10/25/2019 15:05 MST	11.5	100	
KTUS	10/25/2019 15:10 MST	5.75	80	
KTUS	10/25/2019 15:15 MST	10.36	100	
KTUS	10/25/2019 15:20 MST	9.22	60	
KTUS	10/25/2019 15:25 MST	10.36	70	
KTUS	10/25/2019 15:30 MST	12.66	60	18.41
KTUS	10/25/2019 15:35 MST	10.36	50	16.11
KTUS	10/25/2019 15:40 MST	9.22	70	
KTUS	10/25/2019 15:45 MST	13.8	60	
KTUS	10/25/2019 15:50 MST	12.66	50	
KTUS	10/25/2019 15:53 MST	10.36	60	
KTUS	10/25/2019 15:55 MST	13.8	60	31.07
KTUS	10/25/2019 16:00 MST	14.97	130	
KTUS	10/25/2019 16:05 MST	10.36	80	
KTUS	10/25/2019 16:10 MST	11.5	60	
KTUS	10/25/2019 16:15 MST	12.66	60	
KTUS	10/25/2019 16:20 MST	11.5	60	
KTUS	10/25/2019 16:25 MST	11.5	60	
KTUS	10/25/2019 16:30 MST	12.66	60	
KTUS	10/25/2019 16:35 MST	13.8	70	
KTUS	10/25/2019 16:40 MST	11.5	60	17.27
KTUS	10/25/2019 16:45 MST	10.36	60	
KTUS	10/25/2019 16:50 MST	10.36	90	16.11
KTUS	10/25/2019 16:53 MST	10.36	80	
KTUS	10/25/2019 16:55 MST	9.22	60	
KTUS	10/25/2019 17:00 MST	11.5	60	
KTUS	10/25/2019 17:05 MST	9.22	70	
KTUS	10/25/2019 17:10 MST	8.05	80	
KTUS	10/25/2019 17:15 MST	6.91	90	
KTUS	10/25/2019 17:20 MST	5.75	110	

KTUS	10/25/2019 17:25 MST	5.75	110	
KTUS	10/25/2019 17:30 MST	4.61	110	
KTUS	10/25/2019 17:35 MST	6.91	100	
KTUS	10/25/2019 17:40 MST	8.05	70	
KTUS	10/25/2019 17:45 MST	6.91	70	
KTUS	10/25/2019 17:50 MST	6.91	80	
KTUS	10/25/2019 17:53 MST	5.75	80	
KTUS	10/25/2019 17:55 MST	4.61	100	
KTUS	10/25/2019 18:00 MST	5.75	90	
KTUS	10/25/2019 18:05 MST	0	0	
KTUS	10/25/2019 18:10 MST	5.75	110	
KTUS	10/25/2019 18:15 MST	9.22	120	
KTUS	10/25/2019 18:20 MST	10.36	110	
KTUS	10/25/2019 18:25 MST	9.22	110	
KTUS	10/25/2019 18:30 MST	10.36	110	
KTUS	10/25/2019 18:35 MST	8.05	100	
KTUS	10/25/2019 18:40 MST	9.22	110	
KTUS	10/25/2019 18:45 MST	10.36	110	16.11
KTUS	10/25/2019 18:50 MST	11.5	120	
KTUS	10/25/2019 18:53 MST	10.36	120	
KTUS	10/25/2019 18:55 MST	10.36	120	
KTUS	10/25/2019 19:00 MST	11.5	120	
KTUS	10/25/2019 19:05 MST	11.5	120	
KTUS	10/25/2019 19:10 MST	12.66	120	
KTUS	10/25/2019 19:15 MST	14.97	130	20.71
KTUS	10/25/2019 19:20 MST	13.8	130	
KTUS	10/25/2019 19:25 MST	17.27	120	25.32
KTUS	10/25/2019 19:30 MST	14.97	120	20.71
KTUS	10/25/2019 19:35 MST	17.27	120	25.32
KTUS	10/25/2019 19:40 MST	16.11	110	
KTUS	10/25/2019 19:45 MST	18.41	120	25.32
KTUS	10/25/2019 19:50 MST	17.27	120	23.02
KTUS	10/25/2019 19:53 MST	16.11	120	27.63
KTUS	10/25/2019 19:55 MST	16.11	120	25.32
KTUS	10/25/2019 20:00 MST	18.41	120	
KTUS	10/25/2019 20:05 MST	18.41	120	24.16
KTUS	10/25/2019 20:10 MST	19.57	120	25.32
KTUS	10/25/2019 20:15 MST	19.57	130	25.32
KTUS	10/25/2019 20:20 MST	21.85	130	29.93
KTUS	10/25/2019 20:25 MST	21.85	130	28.77
KTUS	10/25/2019 20:30 MST	18.41	120	24.16
KTUS	10/25/2019 20:35 MST	19.57	130	26.46
KTUS	10/25/2019 20:40 MST	21.85	130	28.77
KTUS	10/25/2019 20:45 MST	20.71	130	29.93
KTUS	10/25/2019 20:50 MST	19.57	140	
KTUS	10/25/2019 20:53 MST	19.57	140	29.93
KTUS	10/25/2019 21:00 MST	19.57	130	
KTUS	10/25/2019 21:05 MST	23.02	130	31.07
KTUS	10/25/2019 21:10 MST	21.85	130	27.63
KTUS	10/25/2019 21:15 MST	20.71	130	
KTUS	10/25/2019 21:20 MST	21.85	130	29.93
KTUS	10/25/2019 21:25 MST	19.57	130	25.32

KTUS	10/25/2019 21:30 MST	19.57	130	25.32
KTUS	10/25/2019 21:35 MST	21.85	130	27.63
KTUS	10/25/2019 21:40 MST	23.02	130	
KTUS	10/25/2019 21:45 MST	23.02	130	
KTUS	10/25/2019 21:50 MST	19.57	130	25.32
KTUS	10/25/2019 21:53 MST	21.85	130	
KTUS	10/25/2019 21:55 MST	20.71	140	
KTUS	10/25/2019 22:00 MST	19.57	140	

STATION: KTUS
STATION NAME: Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	11/11/2019 23:00 MST	4.61	130	
KTUS	11/11/2019 23:05 MST	6.91	130	
KTUS	11/11/2019 23:10 MST	5.75	130	
KTUS	11/11/2019 23:15 MST	5.75	120	
KTUS	11/11/2019 23:20 MST	3.44	120	
KTUS	11/11/2019 23:25 MST	4.61	130	
KTUS	11/11/2019 23:30 MST	3.44	140	
KTUS	11/11/2019 23:35 MST	5.75	170	
KTUS	11/11/2019 23:40 MST	5.75	130	
KTUS	11/11/2019 23:45 MST	5.75	160	
KTUS	11/11/2019 23:50 MST	4.61	150	
KTUS	11/11/2019 23:53 MST	4.61	160	
KTUS	11/11/2019 23:55 MST	5.75	150	
KTUS	11/12/2019 00:00 MST	3.44	160	
KTUS	11/12/2019 00:05 MST	5.75	150	
KTUS	11/12/2019 00:10 MST	5.75	140	
KTUS	11/12/2019 00:15 MST	4.61	140	
KTUS	11/12/2019 00:20 MST	5.75	140	
KTUS	11/12/2019 00:25 MST	4.61	130	
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KTUS	11/12/2019 00:35 MST	3.44	110	
KTUS	11/12/2019 00:40 MST	3.44	120	
KTUS	11/12/2019 00:45 MST	3.44	140	
KTUS	11/12/2019 00:50 MST	4.61	140	
KTUS	11/12/2019 00:53 MST	4.61	140	
KTUS	11/12/2019 00:55 MST	5.75	130	
KTUS	11/12/2019 01:00 MST	5.75	130	
KTUS	11/12/2019 01:05 MST	3.44	90	
KTUS	11/12/2019 01:10 MST	4.61	110	
KTUS	11/12/2019 01:15 MST	4.61	120	
KTUS	11/12/2019 01:20 MST	5.75	140	
KTUS	11/12/2019 01:25 MST	8.05	130	
KTUS	11/12/2019 01:30 MST	5.75	160	
KTUS	11/12/2019 01:35 MST	6.91	150	
KTUS	11/12/2019 01:40 MST	6.91	140	
KTUS	11/12/2019 01:45 MST	5.75	150	
KTUS	11/12/2019 01:50 MST	5.75	130	
KTUS	11/12/2019 01:53 MST	5.75	140	
KTUS	11/12/2019 01:55 MST	5.75	130	
KTUS	11/12/2019 02:00 MST	6.91	140	
KTUS	11/12/2019 02:05 MST	5.75	150	
KTUS	11/12/2019 02:10 MST	5.75	160	
KTUS	11/12/2019 02:15 MST	3.44	210	
KTUS	11/12/2019 02:20 MST	5.75	170	

KTUS	11/12/2019 02:25 MST	5.75	150	
KTUS	11/12/2019 02:30 MST	6.91	140	
KTUS	11/12/2019 02:35 MST	8.05	150	
KTUS	11/12/2019 02:40 MST	8.05	150	
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KTUS	11/12/2019 03:00 MST	4.61	200	
KTUS	11/12/2019 03:05 MST	3.44	210	
KTUS	11/12/2019 03:10 MST	4.61	220	
KTUS	11/12/2019 03:15 MST	3.44	210	
KTUS	11/12/2019 03:20 MST	3.44	230	
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KTUS	11/12/2019 03:30 MST	0	0	
KTUS	11/12/2019 03:35 MST	0	0	
KTUS	11/12/2019 03:40 MST			
KTUS	11/12/2019 03:45 MST	10.36	110	
KTUS	11/12/2019 03:50 MST	11.5	110	17.27
KTUS	11/12/2019 03:53 MST	10.36	110	
KTUS	11/12/2019 03:55 MST	10.36	110	
KTUS	11/12/2019 04:00 MST	11.5	110	
KTUS	11/12/2019 04:05 MST	12.66	110	
KTUS	11/12/2019 04:10 MST	12.66	110	
KTUS	11/12/2019 04:15 MST	12.66	120	
KTUS	11/12/2019 04:20 MST	14.97	120	
KTUS	11/12/2019 04:25 MST	13.8	120	19.57
KTUS	11/12/2019 04:30 MST	13.8	120	19.57
KTUS	11/12/2019 04:35 MST	13.8	120	
KTUS	11/12/2019 04:40 MST	12.66	120	
KTUS	11/12/2019 04:45 MST	12.66	120	
KTUS	11/12/2019 04:50 MST	14.97	110	
KTUS	11/12/2019 04:53 MST	16.11	110	
KTUS	11/12/2019 04:55 MST	12.66	110	
KTUS	11/12/2019 05:00 MST	16.11	120	23.02
KTUS	11/12/2019 05:05 MST	13.8	120	
KTUS	11/12/2019 05:10 MST	16.11	120	
KTUS	11/12/2019 05:15 MST	14.97	110	
KTUS	11/12/2019 05:20 MST	13.8	120	
KTUS	11/12/2019 05:25 MST	12.66	120	
KTUS	11/12/2019 05:30 MST	12.66	120	19.57
KTUS	11/12/2019 05:35 MST	13.8	130	
KTUS	11/12/2019 05:40 MST	12.66	120	
KTUS	11/12/2019 05:45 MST	13.8	120	
KTUS	11/12/2019 05:50 MST	12.66	120	
KTUS	11/12/2019 05:53 MST	13.8	120	20.71
KTUS	11/12/2019 05:55 MST	12.66	130	
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KTUS	11/12/2019 06:10 MST	10.36	120	17.27
KTUS	11/12/2019 06:15 MST	8.05	110	
KTUS	11/12/2019 06:20 MST	9.22	100	

KTUS	11/12/2019 06:25 MST	10.36	100	
KTUS	11/12/2019 06:30 MST	9.22	100	
KTUS	11/12/2019 06:35 MST	10.36	110	
KTUS	11/12/2019 06:40 MST	10.36	130	
KTUS	11/12/2019 06:45 MST	12.66	130	18.41
KTUS	11/12/2019 06:50 MST	13.8	130	
KTUS	11/12/2019 06:53 MST	12.66	130	
KTUS	11/12/2019 06:55 MST	14.97	130	
KTUS	11/12/2019 07:00 MST	16.11	130	
KTUS	11/12/2019 07:05 MST	13.8	120	
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KTUS	11/12/2019 07:15 MST	17.27	130	
KTUS	11/12/2019 07:20 MST	14.97	140	20.71
KTUS	11/12/2019 07:25 MST	18.41	130	
KTUS	11/12/2019 07:30 MST	17.27	130	
KTUS	11/12/2019 07:35 MST	18.41	120	24.16
KTUS	11/12/2019 07:40 MST	16.11	130	23.02
KTUS	11/12/2019 07:45 MST	20.71	130	
KTUS	11/12/2019 07:50 MST	21.85	130	
KTUS	11/12/2019 07:53 MST	20.71	120	
KTUS	11/12/2019 07:55 MST	19.57	130	
KTUS	11/12/2019 08:00 MST	20.71	130	26.46
KTUS	11/12/2019 08:05 MST	19.57	120	27.63
KTUS	11/12/2019 08:10 MST	21.85	120	27.63
KTUS	11/12/2019 08:15 MST	21.85	120	31.07
KTUS	11/12/2019 08:20 MST	17.27	110	26.46
KTUS	11/12/2019 08:25 MST	20.71	110	26.46
KTUS	11/12/2019 08:30 MST	19.57	120	29.93
KTUS	11/12/2019 08:35 MST	18.41	120	24.16
KTUS	11/12/2019 08:40 MST	23.02	120	
KTUS	11/12/2019 08:45 MST	23.02	120	28.77
KTUS	11/12/2019 08:50 MST	23.02	120	34.52
KTUS	11/12/2019 08:53 MST	23.02	130	35.68
KTUS	11/12/2019 08:55 MST	27.63	130	
KTUS	11/12/2019 09:00 MST	25.32	130	34.52
KTUS	11/12/2019 09:05 MST	24.16	130	35.68
KTUS	11/12/2019 09:10 MST	21.85	130	
KTUS	11/12/2019 09:15 MST	26.46	130	33.38
KTUS	11/12/2019 09:20 MST	26.46	130	34.52
KTUS	11/12/2019 09:25 MST	28.77	130	
KTUS	11/12/2019 09:30 MST	27.63	130	35.68
KTUS	11/12/2019 09:35 MST	24.16	130	31.07
KTUS	11/12/2019 09:40 MST	26.46	130	33.38
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KTUS	11/12/2019 09:53 MST	23.02	120	35.68
KTUS	11/12/2019 09:55 MST	21.85	120	31.07
KTUS	11/12/2019 10:00 MST	24.16	120	
KTUS	11/12/2019 10:05 MST	21.85	110	28.77
KTUS	11/12/2019 10:10 MST	21.85	120	33.38
KTUS	11/12/2019 10:15 MST	19.57	120	27.63
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KTUS	11/12/2019 10:40 MST	23.02	120	31.07
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KTUS	11/12/2019 11:00 MST	25.32	120	35.68
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KTUS	11/12/2019 11:10 MST	25.32	120	37.98
KTUS	11/12/2019 11:15 MST	25.32	120	33.38
KTUS	11/12/2019 11:20 MST	24.16	120	33.38
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KTUS	11/12/2019 11:40 MST	24.16	120	31.07
KTUS	11/12/2019 11:45 MST	27.63	130	
KTUS	11/12/2019 11:50 MST	29.93	130	
KTUS	11/12/2019 11:53 MST	28.77	130	37.98
KTUS	11/12/2019 11:55 MST	27.63	120	35.68
KTUS	11/12/2019 12:00 MST	24.16	120	33.38
KTUS	11/12/2019 12:05 MST	27.63	130	
KTUS	11/12/2019 12:10 MST	26.46	120	34.52
KTUS	11/12/2019 12:15 MST	21.85	110	29.93
KTUS	11/12/2019 12:20 MST	24.16	110	31.07
KTUS	11/12/2019 12:25 MST	26.46	120	34.52
KTUS	11/12/2019 12:30 MST	25.32	120	32.21
KTUS	11/12/2019 12:35 MST	24.16	120	32.21
KTUS	11/12/2019 12:40 MST	23.02	110	32.21
KTUS	11/12/2019 12:45 MST	26.46	110	35.68
KTUS	11/12/2019 12:50 MST	24.16	120	29.93
KTUS	11/12/2019 12:53 MST	26.46	120	36.82
KTUS	11/12/2019 12:55 MST	26.46	120	35.68
KTUS	11/12/2019 13:00 MST	24.16	120	29.93
KTUS	11/12/2019 13:05 MST	24.16	110	32.21
KTUS	11/12/2019 13:10 MST	23.02	110	33.38
KTUS	11/12/2019 13:15 MST	18.41	110	
KTUS	11/12/2019 13:20 MST	20.71	120	27.63
KTUS	11/12/2019 13:25 MST	20.71	110	28.77
KTUS	11/12/2019 13:30 MST	23.02	120	28.77
KTUS	11/12/2019 13:35 MST	17.27	120	26.46
KTUS	11/12/2019 13:40 MST	21.85	130	27.63
KTUS	11/12/2019 13:45 MST	17.27	110	24.16
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KTUS	11/12/2019 14:05 MST	18.41	120	24.16
KTUS	11/12/2019 14:10 MST	19.57	130	
KTUS	11/12/2019 14:15 MST	18.41	120	26.46
KTUS	11/12/2019 14:20 MST	18.41	110	24.16

KTUS	11/12/2019 14:25 MST	17.27	120	
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KTUS	11/12/2019 14:35 MST	18.41	120	26.46
KTUS	11/12/2019 14:40 MST	19.57	120	
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KTUS	11/12/2019 15:10 MST	17.27	120	
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KTUS	11/12/2019 15:25 MST	17.27	120	23.02
KTUS	11/12/2019 15:30 MST	18.41	120	
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KTUS	11/12/2019 16:00 MST	18.41	110	24.16
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KTUS	11/12/2019 16:15 MST	17.27	110	
KTUS	11/12/2019 16:20 MST	14.97	110	
KTUS	11/12/2019 16:25 MST	11.5	100	
KTUS	11/12/2019 16:30 MST	16.11	110	
KTUS	11/12/2019 16:35 MST	12.66	120	18.41
KTUS	11/12/2019 16:40 MST	14.97	110	23.02
KTUS	11/12/2019 16:45 MST	14.97	120	
KTUS	11/12/2019 16:50 MST	17.27	120	
KTUS	11/12/2019 16:53 MST	13.8	120	23.02
KTUS	11/12/2019 16:55 MST	13.8	120	21.85
KTUS	11/12/2019 17:00 MST	16.11	120	
KTUS	11/12/2019 17:05 MST	17.27	120	23.02
KTUS	11/12/2019 17:10 MST	16.11	110	
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KTUS	11/12/2019 20:10 MST	11.5	90	
KTUS	11/12/2019 20:15 MST	11.5	90	
KTUS	11/12/2019 20:20 MST	11.5	90	17.27
KTUS	11/12/2019 20:25 MST	11.5	90	
KTUS	11/12/2019 20:30 MST	10.36	90	
KTUS	11/12/2019 20:35 MST	9.22	90	
KTUS	11/12/2019 20:40 MST	9.22	90	
KTUS	11/12/2019 20:45 MST	11.5	90	17.27
KTUS	11/12/2019 20:50 MST	11.5	90	
KTUS	11/12/2019 20:53 MST	11.5	90	
KTUS	11/12/2019 20:55 MST	11.5	90	
KTUS	11/12/2019 21:00 MST	9.22	90	
KTUS	11/12/2019 21:05 MST	10.36	90	
KTUS	11/12/2019 21:10 MST	11.5	90	
KTUS	11/12/2019 21:15 MST	10.36	90	
KTUS	11/12/2019 21:25 MST	10.36	100	
KTUS	11/12/2019 21:30 MST	10.36	100	
KTUS	11/12/2019 21:35 MST	12.66	100	
KTUS	11/12/2019 21:40 MST	10.36	100	
KTUS	11/12/2019 21:45 MST	12.66	100	
KTUS	11/12/2019 21:50 MST	12.66	100	
KTUS	11/12/2019 21:53 MST	11.5	100	
KTUS	11/12/2019 21:55 MST	11.5	100	17.27
KTUS	11/12/2019 22:00 MST	13.8	100	
KTUS	11/12/2019 22:05 MST	12.66	110	
KTUS	11/12/2019 22:10 MST	13.8	110	19.57
KTUS	11/12/2019 22:15 MST	12.66	110	
KTUS	11/12/2019 22:20 MST	13.8	110	19.57
KTUS	11/12/2019 22:25 MST	13.8	110	19.57

KTUS	11/12/2019 22:30 MST	13.8	110	21.85
KTUS	11/12/2019 22:35 MST	13.8	110	19.57
KTUS	11/12/2019 22:40 MST	12.66	110	
KTUS	11/12/2019 22:45 MST	13.8	110	19.57
KTUS	11/12/2019 22:50 MST	17.27	120	23.02
KTUS	11/12/2019 22:53 MST	12.66	120	
KTUS	11/12/2019 22:55 MST	16.11	110	24.16
KTUS	11/12/2019 23:00 MST	16.11	110	

STATION: KTUS
STATION NAME: Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	10/25/2020 22:00 MST	5.75	280	
KTUS	10/25/2020 22:05 MST	5.75	280	
KTUS	10/25/2020 22:10 MST	6.91	270	
KTUS	10/25/2020 22:15 MST	5.75	260	
KTUS	10/25/2020 22:20 MST	3.45	240	
KTUS	10/25/2020 22:25 MST	3.45	210	
KTUS	10/25/2020 22:30 MST	3.45	210	
KTUS	10/25/2020 22:35 MST	0	0	
KTUS	10/25/2020 22:40 MST	0	0	
KTUS	10/25/2020 22:45 MST	0	0	
KTUS	10/25/2020 22:50 MST	0	0	
KTUS	10/25/2020 22:53 MST	3.45	350	
KTUS	10/25/2020 22:55 MST	0	0	
KTUS	10/25/2020 23:00 MST	3.45	340	
KTUS	10/25/2020 23:05 MST	3.45	300	
KTUS	10/25/2020 23:10 MST	4.6	270	
KTUS	10/25/2020 23:15 MST	4.6	300	
KTUS	10/25/2020 23:20 MST			
KTUS	10/25/2020 23:25 MST	5.75	270	
KTUS	10/25/2020 23:30 MST	8.06	290	
KTUS	10/25/2020 23:35 MST	10.36	270	
KTUS	10/25/2020 23:40 MST	9.21	270	
KTUS	10/25/2020 23:45 MST	9.21	290	
KTUS	10/25/2020 23:50 MST	8.06	290	
KTUS	10/25/2020 23:53 MST	8.06	290	
KTUS	10/25/2020 23:55 MST	6.91	300	
KTUS	10/26/2020 00:00 MST	10.36	300	
KTUS	10/26/2020 00:05 MST	10.36	290	
KTUS	10/26/2020 00:10 MST	8.06	280	
KTUS	10/26/2020 00:15 MST	9.21	290	
KTUS	10/26/2020 00:20 MST	10.36	280	
KTUS	10/26/2020 00:25 MST	11.51	280	17.26
KTUS	10/26/2020 00:30 MST	11.51	270	
KTUS	10/26/2020 00:35 MST	12.66	260	20.71
KTUS	10/26/2020 00:40 MST	13.81	240	
KTUS	10/26/2020 00:45 MST	14.96	240	
KTUS	10/26/2020 00:50 MST	11.51	240	
KTUS	10/26/2020 00:53 MST	12.66	230	
KTUS	10/26/2020 00:55 MST	11.51	240	
KTUS	10/26/2020 01:00 MST	11.51	230	
KTUS	10/26/2020 01:05 MST	9.21	230	
KTUS	10/26/2020 01:10 MST	9.21	220	
KTUS	10/26/2020 01:15 MST	10.36	220	
KTUS	10/26/2020 01:20 MST	12.66	220	

KTUS	10/26/2020 01:25 MST	10.36	210
KTUS	10/26/2020 01:30 MST	9.21	200
KTUS	10/26/2020 01:35 MST	9.21	200
KTUS	10/26/2020 01:40 MST	8.06	200
KTUS	10/26/2020 01:45 MST	6.91	200
KTUS	10/26/2020 01:50 MST	4.6	200
KTUS	10/26/2020 01:53 MST	5.75	200
KTUS	10/26/2020 01:55 MST	6.91	200
KTUS	10/26/2020 02:00 MST	4.6	220
KTUS	10/26/2020 02:05 MST	0	0
KTUS	10/26/2020 02:10 MST	0	0
KTUS	10/26/2020 02:15 MST	3.45	270
KTUS	10/26/2020 02:20 MST	3.45	250
KTUS	10/26/2020 02:25 MST	3.45	290
KTUS	10/26/2020 02:30 MST	0	0
KTUS	10/26/2020 02:35 MST	0	0
KTUS	10/26/2020 02:40 MST	0	0
KTUS	10/26/2020 02:45 MST	5.75	160
KTUS	10/26/2020 02:50 MST	5.75	210
KTUS	10/26/2020 02:53 MST	3.45	
KTUS	10/26/2020 02:55 MST	0	0
KTUS	10/26/2020 03:00 MST	4.6	170
KTUS	10/26/2020 03:05 MST	5.75	170
KTUS	10/26/2020 03:10 MST	5.75	170
KTUS	10/26/2020 03:15 MST	6.91	150
KTUS	10/26/2020 03:20 MST	3.45	160
KTUS	10/26/2020 03:25 MST	0	0
KTUS	10/26/2020 03:30 MST	0	0
KTUS	10/26/2020 03:35 MST	0	0
KTUS	10/26/2020 03:40 MST	3.45	340
KTUS	10/26/2020 03:45 MST	4.6	330
KTUS	10/26/2020 03:50 MST	4.6	20
KTUS	10/26/2020 03:53 MST	0	0
KTUS	10/26/2020 03:55 MST	0	0
KTUS	10/26/2020 04:00 MST	0	0
KTUS	10/26/2020 04:05 MST	0	0
KTUS	10/26/2020 04:10 MST	0	0
KTUS	10/26/2020 04:15 MST	3.45	240
KTUS	10/26/2020 04:20 MST	3.45	250
KTUS	10/26/2020 04:25 MST	0	0
KTUS	10/26/2020 04:30 MST	3.45	250
KTUS	10/26/2020 04:35 MST	6.91	240
KTUS	10/26/2020 04:40 MST	6.91	250
KTUS	10/26/2020 04:45 MST	6.91	240
KTUS	10/26/2020 04:50 MST	5.75	230
KTUS	10/26/2020 04:53 MST	9.21	230
KTUS	10/26/2020 04:55 MST	9.21	220
KTUS	10/26/2020 05:00 MST	8.06	210
KTUS	10/26/2020 05:05 MST	8.06	180
KTUS	10/26/2020 05:10 MST	9.21	170
KTUS	10/26/2020 05:15 MST	9.21	170
KTUS	10/26/2020 05:20 MST	9.21	180

KTUS	10/26/2020 05:25 MST	8.06	190
KTUS	10/26/2020 05:30 MST	8.06	200
KTUS	10/26/2020 05:35 MST	10.36	210
KTUS	10/26/2020 05:40 MST	10.36	220
KTUS	10/26/2020 05:45 MST	10.36	220
KTUS	10/26/2020 05:50 MST	11.51	220
KTUS	10/26/2020 05:53 MST	11.51	220
KTUS	10/26/2020 05:55 MST	11.51	220
KTUS	10/26/2020 06:00 MST	12.66	220
KTUS	10/26/2020 06:05 MST	11.51	220
KTUS	10/26/2020 06:10 MST	10.36	220
KTUS	10/26/2020 06:15 MST	9.21	230
KTUS	10/26/2020 06:20 MST	5.75	220
KTUS	10/26/2020 06:25 MST	6.91	240
KTUS	10/26/2020 06:30 MST	5.75	250
KTUS	10/26/2020 06:35 MST	4.6	300
KTUS	10/26/2020 06:40 MST	4.6	290
KTUS	10/26/2020 06:45 MST	0	0
KTUS	10/26/2020 06:50 MST	0	0
KTUS	10/26/2020 06:53 MST	0	0
KTUS	10/26/2020 06:55 MST	0	0
KTUS	10/26/2020 07:00 MST	3.45	260
KTUS	10/26/2020 07:05 MST	5.75	300
KTUS	10/26/2020 07:10 MST	8.06	290
KTUS	10/26/2020 07:15 MST	8.06	290
KTUS	10/26/2020 07:20 MST	8.06	290
KTUS	10/26/2020 07:25 MST	6.91	270
KTUS	10/26/2020 07:30 MST	6.91	260
KTUS	10/26/2020 07:35 MST	6.91	260
KTUS	10/26/2020 07:40 MST	5.75	260
KTUS	10/26/2020 07:45 MST	3.45	250
KTUS	10/26/2020 07:50 MST	3.45	210
KTUS	10/26/2020 07:53 MST	0	0
KTUS	10/26/2020 07:55 MST	3.45	250
KTUS	10/26/2020 08:00 MST	4.6	300
KTUS	10/26/2020 08:05 MST	4.6	290
KTUS	10/26/2020 08:10 MST	6.91	280
KTUS	10/26/2020 08:15 MST	4.6	290
KTUS	10/26/2020 08:20 MST	9.21	280
KTUS	10/26/2020 08:25 MST	9.21	290
KTUS	10/26/2020 08:30 MST	10.36	300
KTUS	10/26/2020 08:35 MST	10.36	290
KTUS	10/26/2020 08:40 MST	11.51	270
KTUS	10/26/2020 08:45 MST	12.66	300
KTUS	10/26/2020 08:50 MST	10.36	300
KTUS	10/26/2020 08:53 MST	12.66	300
KTUS	10/26/2020 08:55 MST	11.51	310
KTUS	10/26/2020 09:00 MST	11.51	300
KTUS	10/26/2020 09:05 MST	12.66	310
KTUS	10/26/2020 09:10 MST	13.81	300
KTUS	10/26/2020 09:15 MST	12.66	300
KTUS	10/26/2020 09:20 MST	12.66	290

KTUS	10/26/2020 09:25 MST	10.36	290	
KTUS	10/26/2020 09:30 MST	11.51	290	17.26
KTUS	10/26/2020 09:35 MST	8.06	290	
KTUS	10/26/2020 09:40 MST	10.36	300	
KTUS	10/26/2020 09:45 MST	13.81	290	
KTUS	10/26/2020 09:50 MST	10.36	300	
KTUS	10/26/2020 09:53 MST	9.21	290	19.56
KTUS	10/26/2020 09:55 MST	10.36	300	16.11
KTUS	10/26/2020 10:00 MST	12.66	310	
KTUS	10/26/2020 10:05 MST	6.91	300	
KTUS	10/26/2020 10:10 MST	11.51	290	
KTUS	10/26/2020 10:15 MST	11.51	310	
KTUS	10/26/2020 10:20 MST	12.66	310	
KTUS	10/26/2020 10:25 MST	11.51	300	
KTUS	10/26/2020 10:30 MST	12.66	280	
KTUS	10/26/2020 10:35 MST	11.51	300	17.26
KTUS	10/26/2020 10:40 MST	14.96	280	20.71
KTUS	10/26/2020 10:45 MST	16.11	270	21.86
KTUS	10/26/2020 10:50 MST	11.51	300	19.56
KTUS	10/26/2020 10:53 MST	14.96	310	21.86
KTUS	10/26/2020 10:55 MST	12.66	300	
KTUS	10/26/2020 11:00 MST	13.81	300	
KTUS	10/26/2020 11:05 MST	10.36	300	
KTUS	10/26/2020 11:10 MST	12.66	290	
KTUS	10/26/2020 11:15 MST	13.81	290	
KTUS	10/26/2020 11:20 MST	14.96	320	
KTUS	10/26/2020 11:25 MST	14.96	290	
KTUS	10/26/2020 11:30 MST	13.81	320	20.71
KTUS	10/26/2020 11:35 MST	12.66	300	18.41
KTUS	10/26/2020 11:40 MST	11.51	300	
KTUS	10/26/2020 11:45 MST	11.51	310	19.56
KTUS	10/26/2020 11:50 MST	11.51	310	
KTUS	10/26/2020 11:53 MST	14.96	320	23.02
KTUS	10/26/2020 11:55 MST	14.96	300	
KTUS	10/26/2020 12:00 MST	12.66	310	
KTUS	10/26/2020 12:05 MST	12.66	290	19.56
KTUS	10/26/2020 12:10 MST	14.96	310	24.17
KTUS	10/26/2020 12:15 MST	16.11	300	
KTUS	10/26/2020 12:20 MST	12.66	300	18.41
KTUS	10/26/2020 12:25 MST	13.81	270	
KTUS	10/26/2020 12:30 MST	14.96	270	
KTUS	10/26/2020 12:35 MST	13.81	280	21.86
KTUS	10/26/2020 12:40 MST	14.96	290	
KTUS	10/26/2020 12:45 MST	14.96	290	21.86
KTUS	10/26/2020 12:50 MST	13.81	300	20.71
KTUS	10/26/2020 12:53 MST	12.66	290	28.77
KTUS	10/26/2020 12:55 MST	16.11	280	
KTUS	10/26/2020 13:00 MST	11.51	300	
KTUS	10/26/2020 13:05 MST	16.11	310	21.86
KTUS	10/26/2020 13:10 MST	12.66	310	
KTUS	10/26/2020 13:15 MST	16.11	290	
KTUS	10/26/2020 13:20 MST	13.81	300	

KTUS	10/26/2020 13:25 MST	11.51	310	18.41
KTUS	10/26/2020 13:30 MST	14.96	310	21.86
KTUS	10/26/2020 13:35 MST	12.66	320	
KTUS	10/26/2020 13:40 MST	11.51	280	18.41
KTUS	10/26/2020 13:45 MST	14.96	290	
KTUS	10/26/2020 13:50 MST	10.36	300	17.26
KTUS	10/26/2020 13:53 MST	12.66	300	21.86
KTUS	10/26/2020 13:55 MST	13.81	300	
KTUS	10/26/2020 14:00 MST	13.81	300	
KTUS	10/26/2020 14:05 MST	13.81	310	
KTUS	10/26/2020 14:10 MST	13.81	290	19.56
KTUS	10/26/2020 14:15 MST	13.81	300	
KTUS	10/26/2020 14:20 MST	16.11	310	
KTUS	10/26/2020 14:25 MST	17.26	320	25.32
KTUS	10/26/2020 14:30 MST	13.81	300	19.56
KTUS	10/26/2020 14:35 MST	16.11	300	
KTUS	10/26/2020 14:40 MST	20.71	310	
KTUS	10/26/2020 14:45 MST	12.66	320	
KTUS	10/26/2020 14:50 MST	17.26	320	24.17
KTUS	10/26/2020 14:53 MST	14.96	330	26.47
KTUS	10/26/2020 14:55 MST	12.66	320	20.71
KTUS	10/26/2020 15:00 MST	20.71	330	
KTUS	10/26/2020 15:05 MST	14.96	320	
KTUS	10/26/2020 15:10 MST	19.56	330	25.32
KTUS	10/26/2020 15:15 MST	17.26	310	25.32
KTUS	10/26/2020 15:20 MST	19.56	330	27.62
KTUS	10/26/2020 15:25 MST	17.26	310	
KTUS	10/26/2020 15:30 MST	17.26	320	24.17
KTUS	10/26/2020 15:35 MST	18.41	320	24.17
KTUS	10/26/2020 15:40 MST	16.11	320	
KTUS	10/26/2020 15:45 MST	12.66	310	
KTUS	10/26/2020 15:50 MST	18.41	300	
KTUS	10/26/2020 15:53 MST	16.11	300	28.77
KTUS	10/26/2020 15:55 MST	17.26	300	25.32
KTUS	10/26/2020 16:00 MST	19.56	290	27.62
KTUS	10/26/2020 16:05 MST	16.11	300	24.17
KTUS	10/26/2020 16:10 MST	17.26	290	24.17
KTUS	10/26/2020 16:15 MST	16.11	300	
KTUS	10/26/2020 16:20 MST	13.81	300	
KTUS	10/26/2020 16:25 MST	19.56	310	26.47
KTUS	10/26/2020 16:30 MST	16.11	300	
KTUS	10/26/2020 16:35 MST	18.41	300	26.47
KTUS	10/26/2020 16:40 MST	18.41	300	27.62
KTUS	10/26/2020 16:45 MST	18.41	300	25.32
KTUS	10/26/2020 16:50 MST	19.56	300	26.47
KTUS	10/26/2020 16:53 MST	19.56	290	31.07
KTUS	10/26/2020 16:55 MST	19.56	290	25.32
KTUS	10/26/2020 17:00 MST	18.41	290	28.77
KTUS	10/26/2020 17:05 MST	16.11	290	
KTUS	10/26/2020 17:10 MST	18.41	290	26.47
KTUS	10/26/2020 17:15 MST	14.96	300	21.86
KTUS	10/26/2020 17:20 MST	18.41	280	25.32

KTUS	10/26/2020 17:25 MST	18.41	290	
KTUS	10/26/2020 17:30 MST	13.81	290	20.71
KTUS	10/26/2020 17:35 MST	14.96	280	20.71
KTUS	10/26/2020 17:40 MST	18.41	280	25.32
KTUS	10/26/2020 17:45 MST	13.81	280	
KTUS	10/26/2020 17:50 MST	16.11	290	
KTUS	10/26/2020 17:53 MST	16.11	290	24.17
KTUS	10/26/2020 17:55 MST	16.11	290	
KTUS	10/26/2020 18:00 MST	18.41	290	
KTUS	10/26/2020 18:04 MST	14.96	290	27.62
KTUS	10/26/2020 18:05 MST	16.11	290	21.86
KTUS	10/26/2020 18:10 MST	13.81	290	
KTUS	10/26/2020 18:15 MST	9.21	290	
KTUS	10/26/2020 18:20 MST	10.36	310	18.41
KTUS	10/26/2020 18:25 MST	11.51	300	
KTUS	10/26/2020 18:30 MST	12.66	310	18.41
KTUS	10/26/2020 18:35 MST	12.66	310	
KTUS	10/26/2020 18:40 MST	11.51	320	
KTUS	10/26/2020 18:45 MST	11.51	310	
KTUS	10/26/2020 18:50 MST	6.91	310	
KTUS	10/26/2020 18:53 MST	9.21	310	
KTUS	10/26/2020 18:55 MST	10.36	310	
KTUS	10/26/2020 19:00 MST	8.06	300	
KTUS	10/26/2020 19:05 MST	11.51	300	
KTUS	10/26/2020 19:10 MST	10.36	290	
KTUS	10/26/2020 19:15 MST	10.36	300	
KTUS	10/26/2020 19:20 MST	10.36	300	
KTUS	10/26/2020 19:25 MST	8.06	300	
KTUS	10/26/2020 19:30 MST	13.81	290	
KTUS	10/26/2020 19:35 MST	10.36	290	
KTUS	10/26/2020 19:40 MST	12.66	290	
KTUS	10/26/2020 19:45 MST	10.36	280	
KTUS	10/26/2020 19:50 MST	10.36	290	
KTUS	10/26/2020 19:53 MST	12.66	290	
KTUS	10/26/2020 19:55 MST	11.51	280	
KTUS	10/26/2020 20:00 MST	12.66	280	19.56
KTUS	10/26/2020 20:05 MST	13.81	290	
KTUS	10/26/2020 20:10 MST	12.66	290	19.56
KTUS	10/26/2020 20:15 MST	10.36	290	
KTUS	10/26/2020 20:20 MST	10.36	290	
KTUS	10/26/2020 20:25 MST	8.06	290	
KTUS	10/26/2020 20:30 MST	10.36	290	
KTUS	10/26/2020 20:35 MST	10.36	280	
KTUS	10/26/2020 20:40 MST	9.21	290	
KTUS	10/26/2020 20:45 MST	8.06	280	
KTUS	10/26/2020 20:50 MST	8.06	280	
KTUS	10/26/2020 20:53 MST	9.21	290	
KTUS	10/26/2020 20:55 MST	9.21	290	
KTUS	10/26/2020 21:00 MST	9.21	290	
KTUS	10/26/2020 21:05 MST	9.21	280	
KTUS	10/26/2020 21:10 MST	6.91	270	
KTUS	10/26/2020 21:15 MST	5.75	260	

KTUS	10/26/2020 21:20 MST	6.91	250
KTUS	10/26/2020 21:25 MST	5.75	250
KTUS	10/26/2020 21:30 MST	6.91	260
KTUS	10/26/2020 21:35 MST	6.91	260
KTUS	10/26/2020 21:40 MST	6.91	270
KTUS	10/26/2020 21:45 MST	4.6	260
KTUS	10/26/2020 21:50 MST	4.6	240
KTUS	10/26/2020 21:53 MST	5.75	250
KTUS	10/26/2020 21:55 MST	5.75	240
KTUS	10/26/2020 22:00 MST	5.75	240

STATION: KTUS
STATION NAME: Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	11/07/2020 23:53 MST	8.06	280	
KTUS	11/08/2020 00:53 MST	12.66	330	
KTUS	11/08/2020 01:53 MST	10.36	340	
KTUS	11/08/2020 02:53 MST	8.06	320	
KTUS	11/08/2020 03:53 MST	0	0	
KTUS	11/08/2020 04:53 MST	3.45	270	
KTUS	11/08/2020 05:53 MST	3.45	190	
KTUS	11/08/2020 06:53 MST	4.6	230	
KTUS	11/08/2020 07:53 MST	3.45	140	
KTUS	11/08/2020 08:53 MST	3.45	190	
KTUS	11/08/2020 09:53 MST	5.75	120	
KTUS	11/08/2020 10:53 MST	12.66	200	23.02
KTUS	11/08/2020 11:53 MST	16.11	230	24.17
KTUS	11/08/2020 12:53 MST	14.96	210	28.77
KTUS	11/08/2020 13:53 MST	12.66	220	20.71
KTUS	11/08/2020 14:53 MST	19.56	250	32.22
KTUS	11/08/2020 15:53 MST	14.96	250	28.77
KTUS	11/08/2020 16:53 MST	14.96	260	27.62
KTUS	11/08/2020 17:53 MST	11.51	260	19.56
KTUS	11/08/2020 18:53 MST	9.21	260	19.56
KTUS	11/08/2020 19:53 MST	11.51	260	
KTUS	11/08/2020 20:53 MST	13.81	210	23.02
KTUS	11/08/2020 21:53 MST	8.06	230	19.56
KTUS	11/08/2020 22:53 MST	9.21	190	

STATION: KTUS
STATION NAME: Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	01/18/2021 23:00 MST	5.75	150	
KTUS	01/18/2021 23:05 MST	3.45	150	
KTUS	01/18/2021 23:10 MST	3.45	140	
KTUS	01/18/2021 23:15 MST	4.6	130	
KTUS	01/18/2021 23:20 MST	5.75	130	
KTUS	01/18/2021 23:25 MST	5.75	130	
KTUS	01/18/2021 23:30 MST	4.6	140	
KTUS	01/18/2021 23:35 MST	5.75	140	
KTUS	01/18/2021 23:40 MST	5.75	140	
KTUS	01/18/2021 23:45 MST	6.91	140	
KTUS	01/18/2021 23:50 MST	6.91	150	
KTUS	01/18/2021 23:53 MST	6.91	140	
KTUS	01/18/2021 23:55 MST	6.91	140	
KTUS	01/19/2021 00:00 MST	6.91	150	
KTUS	01/19/2021 00:05 MST	5.75	150	
KTUS	01/19/2021 00:10 MST	5.75	140	
KTUS	01/19/2021 00:15 MST	4.6	140	
KTUS	01/19/2021 00:20 MST	4.6	120	
KTUS	01/19/2021 00:25 MST	3.45	130	
KTUS	01/19/2021 00:30 MST	4.6	130	
KTUS	01/19/2021 00:35 MST	3.45	120	
KTUS	01/19/2021 00:40 MST	3.45	120	
KTUS	01/19/2021 00:45 MST	5.75	120	
KTUS	01/19/2021 00:50 MST	3.45	130	
KTUS	01/19/2021 00:53 MST	3.45	140	
KTUS	01/19/2021 00:55 MST	4.6	140	
KTUS	01/19/2021 01:00 MST	4.6	130	
KTUS	01/19/2021 01:05 MST	3.45	140	
KTUS	01/19/2021 01:10 MST	3.45	130	
KTUS	01/19/2021 01:15 MST	3.45	140	
KTUS	01/19/2021 01:20 MST	3.45	140	
KTUS	01/19/2021 01:25 MST	0	0	
KTUS	01/19/2021 01:30 MST	0	0	
KTUS	01/19/2021 01:35 MST	4.6	130	
KTUS	01/19/2021 01:40 MST	0	0	
KTUS	01/19/2021 01:45 MST	3.45	110	
KTUS	01/19/2021 01:50 MST	5.75	110	
KTUS	01/19/2021 01:53 MST	5.75	120	
KTUS	01/19/2021 01:55 MST	5.75	120	
KTUS	01/19/2021 02:00 MST	5.75	120	
KTUS	01/19/2021 02:05 MST	5.75	140	
KTUS	01/19/2021 02:10 MST	4.6	150	
KTUS	01/19/2021 02:15 MST	3.45	180	
KTUS	01/19/2021 02:20 MST	4.6	160	

KTUS	01/19/2021 02:25 MST	5.75	160
KTUS	01/19/2021 02:30 MST	6.91	310
KTUS	01/19/2021 02:35 MST	0	0
KTUS	01/19/2021 02:40 MST	0	0
KTUS	01/19/2021 02:45 MST	0	0
KTUS	01/19/2021 02:50 MST	5.75	180
KTUS	01/19/2021 02:53 MST	4.6	150
KTUS	01/19/2021 02:55 MST	5.75	130
KTUS	01/19/2021 03:00 MST	0	0
KTUS	01/19/2021 03:05 MST	0	0
KTUS	01/19/2021 03:10 MST	0	0
KTUS	01/19/2021 03:15 MST	0	0
KTUS	01/19/2021 03:20 MST	3.45	110
KTUS	01/19/2021 03:25 MST	4.6	120
KTUS	01/19/2021 03:30 MST	5.75	150
KTUS	01/19/2021 03:35 MST	5.75	140
KTUS	01/19/2021 03:40 MST	5.75	140
KTUS	01/19/2021 03:45 MST	6.91	150
KTUS	01/19/2021 03:50 MST	6.91	150
KTUS	01/19/2021 03:53 MST	8.06	160
KTUS	01/19/2021 03:55 MST	8.06	150
KTUS	01/19/2021 04:00 MST	8.06	150
KTUS	01/19/2021 04:05 MST	9.21	150
KTUS	01/19/2021 04:10 MST	3.45	130
KTUS	01/19/2021 04:15 MST	4.6	330
KTUS	01/19/2021 04:20 MST	0	0
KTUS	01/19/2021 04:25 MST	0	0
KTUS	01/19/2021 04:30 MST	4.6	10
KTUS	01/19/2021 04:35 MST	8.06	360
KTUS	01/19/2021 04:40 MST	6.91	20
KTUS	01/19/2021 04:45 MST	3.45	360
KTUS	01/19/2021 04:50 MST	3.45	20
KTUS	01/19/2021 04:53 MST	3.45	10
KTUS	01/19/2021 04:55 MST	3.45	20
KTUS	01/19/2021 05:00 MST	3.45	40
KTUS	01/19/2021 05:05 MST	5.75	40
KTUS	01/19/2021 05:10 MST	8.06	30
KTUS	01/19/2021 05:15 MST	10.36	20
KTUS	01/19/2021 05:20 MST	5.75	20
KTUS	01/19/2021 05:25 MST	4.6	360
KTUS	01/19/2021 05:30 MST	0	0
KTUS	01/19/2021 05:35 MST	3.45	40
KTUS	01/19/2021 05:40 MST	4.6	40
KTUS	01/19/2021 05:45 MST	4.6	30
KTUS	01/19/2021 05:50 MST	4.6	30
KTUS	01/19/2021 05:53 MST	4.6	40
KTUS	01/19/2021 05:55 MST	4.6	40
KTUS	01/19/2021 06:00 MST	6.91	40
KTUS	01/19/2021 06:05 MST	3.45	30
KTUS	01/19/2021 06:10 MST	0	0
KTUS	01/19/2021 06:15 MST	0	0
KTUS	01/19/2021 06:20 MST	0	0

KTUS	01/19/2021 06:25 MST	3.45	30
KTUS	01/19/2021 06:30 MST	3.45	50
KTUS	01/19/2021 06:35 MST	4.6	40
KTUS	01/19/2021 06:40 MST	3.45	60
KTUS	01/19/2021 06:45 MST	0	0
KTUS	01/19/2021 06:50 MST	0	0
KTUS	01/19/2021 06:53 MST	0	0
KTUS	01/19/2021 06:55 MST	0	0
KTUS	01/19/2021 07:00 MST	0	0
KTUS	01/19/2021 07:05 MST	3.45	50
KTUS	01/19/2021 07:10 MST	5.75	60
KTUS	01/19/2021 07:15 MST	5.75	50
KTUS	01/19/2021 07:20 MST	4.6	60
KTUS	01/19/2021 07:25 MST	0	0
KTUS	01/19/2021 07:30 MST	3.45	270
KTUS	01/19/2021 07:35 MST	0	0
KTUS	01/19/2021 07:40 MST	0	0
KTUS	01/19/2021 07:45 MST	0	0
KTUS	01/19/2021 07:50 MST	0	0
KTUS	01/19/2021 07:53 MST	3.45	80
KTUS	01/19/2021 07:55 MST	0	0
KTUS	01/19/2021 08:00 MST	4.6	80
KTUS	01/19/2021 08:05 MST	0	0
KTUS	01/19/2021 08:10 MST	0	0
KTUS	01/19/2021 08:15 MST	3.45	70
KTUS	01/19/2021 08:20 MST	3.45	80
KTUS	01/19/2021 08:25 MST	6.91	100
KTUS	01/19/2021 08:30 MST	5.75	80
KTUS	01/19/2021 08:35 MST	8.06	90
KTUS	01/19/2021 08:40 MST	6.91	90
KTUS	01/19/2021 08:45 MST	5.75	160
KTUS	01/19/2021 08:50 MST	3.45	200
KTUS	01/19/2021 08:53 MST	5.75	260
KTUS	01/19/2021 08:55 MST	8.06	250
KTUS	01/19/2021 09:00 MST	6.91	240
KTUS	01/19/2021 09:05 MST	4.6	250
KTUS	01/19/2021 09:10 MST	3.45	230
KTUS	01/19/2021 09:15 MST	0	0
KTUS	01/19/2021 09:20 MST	3.45	150
KTUS	01/19/2021 09:25 MST	4.6	140
KTUS	01/19/2021 09:30 MST	8.06	140
KTUS	01/19/2021 09:35 MST	8.06	140
KTUS	01/19/2021 09:40 MST	5.75	160
KTUS	01/19/2021 09:45 MST	5.75	180
KTUS	01/19/2021 09:50 MST	3.45	210
KTUS	01/19/2021 09:53 MST	3.45	
KTUS	01/19/2021 09:55 MST	4.6	240
KTUS	01/19/2021 10:00 MST	0	0
KTUS	01/19/2021 10:05 MST	0	0
KTUS	01/19/2021 10:10 MST	0	0
KTUS	01/19/2021 10:15 MST	3.45	100
KTUS	01/19/2021 10:20 MST	3.45	90

KTUS	01/19/2021 10:25 MST	4.6	90	
KTUS	01/19/2021 10:30 MST	4.6	80	
KTUS	01/19/2021 10:35 MST	5.75	80	
KTUS	01/19/2021 10:40 MST	4.6	80	
KTUS	01/19/2021 10:45 MST	4.6	60	
KTUS	01/19/2021 10:50 MST	5.75	30	
KTUS	01/19/2021 10:53 MST	3.45	20	
KTUS	01/19/2021 10:55 MST	0	0	
KTUS	01/19/2021 11:00 MST	3.45	330	
KTUS	01/19/2021 11:05 MST	4.6	310	
KTUS	01/19/2021 11:10 MST	3.45	280	
KTUS	01/19/2021 11:15 MST	0	0	
KTUS	01/19/2021 11:20 MST	0	0	
KTUS	01/19/2021 11:25 MST	0	0	
KTUS	01/19/2021 11:30 MST	0	0	
KTUS	01/19/2021 11:35 MST	5.75	100	
KTUS	01/19/2021 11:40 MST	4.6	120	
KTUS	01/19/2021 11:45 MST	12.66	140	
KTUS	01/19/2021 11:50 MST	9.21	130	
KTUS	01/19/2021 11:53 MST	10.36	140	
KTUS	01/19/2021 11:55 MST	10.36	160	
KTUS	01/19/2021 12:00 MST	10.36	130	
KTUS	01/19/2021 12:05 MST	11.51	120	
KTUS	01/19/2021 12:10 MST	10.36	120	
KTUS	01/19/2021 12:15 MST	10.36	110	
KTUS	01/19/2021 12:20 MST	10.36	140	
KTUS	01/19/2021 12:25 MST	10.36	130	
KTUS	01/19/2021 12:30 MST	8.06	160	
KTUS	01/19/2021 12:35 MST	11.51	140	
KTUS	01/19/2021 12:40 MST	13.81	160	21.86
KTUS	01/19/2021 12:45 MST	14.96	190	
KTUS	01/19/2021 12:50 MST	10.36	180	
KTUS	01/19/2021 12:53 MST	6.91	170	18.41
KTUS	01/19/2021 12:55 MST	6.91	160	
KTUS	01/19/2021 13:00 MST	8.06	140	
KTUS	01/19/2021 13:05 MST	8.06	180	
KTUS	01/19/2021 13:10 MST	6.91	190	
KTUS	01/19/2021 13:15 MST	10.36	170	
KTUS	01/19/2021 13:20 MST	8.06	120	
KTUS	01/19/2021 13:25 MST	5.75	120	
KTUS	01/19/2021 13:30 MST	6.91	150	
KTUS	01/19/2021 13:35 MST	10.36	170	
KTUS	01/19/2021 13:40 MST	12.66	150	
KTUS	01/19/2021 13:45 MST	3.45	170	
KTUS	01/19/2021 13:50 MST	11.51	170	20.71
KTUS	01/19/2021 13:53 MST	8.06	170	20.71
KTUS	01/19/2021 13:55 MST	8.06	150	
KTUS	01/19/2021 14:00 MST	11.51	140	18.41
KTUS	01/19/2021 14:05 MST	9.21	180	
KTUS	01/19/2021 14:10 MST	6.91	140	
KTUS	01/19/2021 14:15 MST	10.36	140	
KTUS	01/19/2021 14:20 MST	6.91	150	

KTUS	01/19/2021 14:25 MST	10.36	140	16.11
KTUS	01/19/2021 14:30 MST	11.51	150	
KTUS	01/19/2021 14:35 MST	5.75	150	
KTUS	01/19/2021 14:40 MST	13.81	190	
KTUS	01/19/2021 14:45 MST	24.17	180	31.07
KTUS	01/19/2021 14:50 MST	25.32	180	36.82
KTUS	01/19/2021 14:53 MST	24.17	190	37.98
KTUS	01/19/2021 14:55 MST	20.71	190	
KTUS	01/19/2021 15:00 MST	17.26	200	
KTUS	01/19/2021 15:05 MST	25.32	180	31.07
KTUS	01/19/2021 15:10 MST	25.32	190	32.22
KTUS	01/19/2021 15:15 MST	24.17	190	35.67
KTUS	01/19/2021 15:20 MST	24.17	190	33.37
KTUS	01/19/2021 15:25 MST	19.56	180	
KTUS	01/19/2021 15:30 MST	18.41	190	27.62
KTUS	01/19/2021 15:35 MST	18.41	190	
KTUS	01/19/2021 15:40 MST	21.86	190	
KTUS	01/19/2021 15:45 MST	20.71	190	29.92
KTUS	01/19/2021 15:50 MST	18.41	190	
KTUS	01/19/2021 15:53 MST	19.56	190	32.22
KTUS	01/19/2021 15:55 MST	13.81	190	
KTUS	01/19/2021 16:00 MST	14.96	190	21.86
KTUS	01/19/2021 16:05 MST	14.96	170	
KTUS	01/19/2021 16:10 MST	17.26	180	
KTUS	01/19/2021 16:15 MST	16.11	180	21.86
KTUS	01/19/2021 16:20 MST	13.81	150	19.56
KTUS	01/19/2021 16:25 MST	14.96	150	
KTUS	01/19/2021 16:30 MST	14.96	170	
KTUS	01/19/2021 16:35 MST	9.21	160	
KTUS	01/19/2021 16:40 MST	21.86	170	29.92
KTUS	01/19/2021 16:45 MST	19.56	180	26.47
KTUS	01/19/2021 16:50 MST	16.11	200	
KTUS	01/19/2021 16:53 MST	16.11	190	27.62
KTUS	01/19/2021 16:55 MST	17.26	190	24.17
KTUS	01/19/2021 17:00 MST	16.11	190	
KTUS	01/19/2021 17:05 MST	14.96	200	
KTUS	01/19/2021 17:10 MST	17.26	190	
KTUS	01/19/2021 17:15 MST	12.66	190	
KTUS	01/19/2021 17:20 MST	12.66	180	
KTUS	01/19/2021 17:25 MST	14.96	160	
KTUS	01/19/2021 17:30 MST	18.41	150	
KTUS	01/19/2021 17:35 MST	18.41	140	
KTUS	01/19/2021 17:40 MST	17.26	130	
KTUS	01/19/2021 17:45 MST	16.11	130	
KTUS	01/19/2021 17:50 MST	12.66	120	
KTUS	01/19/2021 17:53 MST	12.66	130	
KTUS	01/19/2021 17:55 MST	11.51	130	
KTUS	01/19/2021 18:00 MST	10.36	120	
KTUS	01/19/2021 18:05 MST	13.81	120	
KTUS	01/19/2021 18:10 MST	13.81	110	21.86
KTUS	01/19/2021 18:15 MST	14.96	110	21.86
KTUS	01/19/2021 18:20 MST	14.96	100	

KTUS	01/19/2021 18:25 MST	17.26	110	
KTUS	01/19/2021 18:30 MST	16.11	110	
KTUS	01/19/2021 18:35 MST	14.96	110	
KTUS	01/19/2021 18:40 MST	13.81	110	
KTUS	01/19/2021 18:45 MST	16.11	110	
KTUS	01/19/2021 18:50 MST	18.41	110	25.32
KTUS	01/19/2021 18:53 MST	16.11	110	26.47
KTUS	01/19/2021 18:55 MST	17.26	110	25.32
KTUS	01/19/2021 19:00 MST	20.71	110	27.62
KTUS	01/19/2021 19:05 MST	20.71	110	28.77
KTUS	01/19/2021 19:10 MST	24.17	110	32.22
KTUS	01/19/2021 19:15 MST	21.86	120	28.77
KTUS	01/19/2021 19:20 MST	26.47	120	37.98
KTUS	01/19/2021 19:25 MST	23.02	120	32.22
KTUS	01/19/2021 19:30 MST	23.02	120	32.22
KTUS	01/19/2021 19:35 MST	24.17	120	35.67
KTUS	01/19/2021 19:40 MST	19.56	120	25.32
KTUS	01/19/2021 19:45 MST	23.02	120	28.77
KTUS	01/19/2021 19:50 MST	23.02	120	
KTUS	01/19/2021 19:53 MST	20.71	120	34.52
KTUS	01/19/2021 19:55 MST	24.17	120	36.82
KTUS	01/19/2021 20:00 MST	23.02	120	28.77
KTUS	01/19/2021 20:05 MST	23.02	120	32.22
KTUS	01/19/2021 20:10 MST	27.62	120	35.67
KTUS	01/19/2021 20:15 MST	24.17	120	40.28
KTUS	01/19/2021 20:20 MST	27.62	120	
KTUS	01/19/2021 20:25 MST	27.62	120	33.37
KTUS	01/19/2021 20:30 MST	27.62	120	40.28
KTUS	01/19/2021 20:35 MST	21.86	110	
KTUS	01/19/2021 20:40 MST	27.62	120	33.37
KTUS	01/19/2021 20:45 MST	24.17	120	31.07
KTUS	01/19/2021 20:50 MST	25.32	120	34.52
KTUS	01/19/2021 20:53 MST	26.47	120	37.98
KTUS	01/19/2021 20:55 MST	24.17	120	31.07
KTUS	01/19/2021 21:00 MST	25.32	120	33.37
KTUS	01/19/2021 21:05 MST	25.32	120	33.37
KTUS	01/19/2021 21:10 MST	24.17	120	33.37
KTUS	01/19/2021 21:15 MST	25.32	120	34.52
KTUS	01/19/2021 21:20 MST	25.32	120	
KTUS	01/19/2021 21:25 MST	27.62	120	43.73
KTUS	01/19/2021 21:30 MST	27.62	120	36.82
KTUS	01/19/2021 21:35 MST	25.32	120	
KTUS	01/19/2021 21:40 MST	21.86	110	33.37
KTUS	01/19/2021 21:45 MST	24.17	120	33.37
KTUS	01/19/2021 21:50 MST	20.71	110	31.07
KTUS	01/19/2021 21:53 MST	21.86	120	34.52
KTUS	01/19/2021 21:55 MST	21.86	120	31.07
KTUS	01/19/2021 22:00 MST	25.32	120	34.52
KTUS	01/19/2021 22:05 MST	25.32	120	39.13
KTUS	01/19/2021 22:10 MST	28.77	120	42.58
KTUS	01/19/2021 22:15 MST	21.86	120	35.67
KTUS	01/19/2021 22:20 MST	24.17	120	31.07

KTUS	01/19/2021 22:25 MST	24.17	120	33.37
KTUS	01/19/2021 22:30 MST	27.62	110	36.82
KTUS	01/19/2021 22:35 MST	24.17	120	31.07
KTUS	01/19/2021 22:40 MST	25.32	120	36.82
KTUS	01/19/2021 22:45 MST	28.77	120	34.52
KTUS	01/19/2021 22:50 MST	24.17	120	31.07
KTUS	01/19/2021 22:53 MST	24.17	120	40.28
KTUS	01/19/2021 22:55 MST	27.62	120	36.82
KTUS	01/19/2021 23:00 MST	26.47	120	34.52

STATION: KTUS
STATIOl Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	03/31/202	6.91	200	
KTUS	03/31/202	5.75	190	
KTUS	03/31/202	6.91	180	
KTUS	03/31/202	5.75	200	
KTUS	03/31/202	5.75	190	
KTUS	03/31/202	8.06	180	
KTUS	03/31/202	6.91	180	
KTUS	03/31/202	6.91	170	
KTUS	03/31/202	5.75	170	
KTUS	03/31/202	3.45	130	
KTUS	03/31/202	3.45	200	
KTUS	03/31/202	3.45	210	
KTUS	03/31/202	4.6	180	
KTUS	03/31/202	5.75	160	
KTUS	03/31/202	5.75	180	
KTUS	03/31/202	6.91	200	
KTUS	03/31/202	4.6	200	
KTUS	03/31/202	4.6	200	
KTUS	03/31/202	5.75	210	
KTUS	03/31/202	3.45	80	
KTUS	03/31/202	0	0	
KTUS	03/31/202	0	0	
KTUS	03/31/202	0	0	
KTUS	03/31/202	3.45	130	
KTUS	03/31/202	4.6	110	
KTUS	03/31/202	4.6	110	
KTUS	04/01/202	4.6	120	
KTUS	04/01/202	5.75	130	
KTUS	04/01/202	8.06	130	
KTUS	04/01/202	6.91	140	
KTUS	04/01/202	6.91	130	
KTUS	04/01/202	9.21	150	
KTUS	04/01/202	9.21	140	
KTUS	04/01/202	8.06	140	
KTUS	04/01/202	8.06	150	
KTUS	04/01/202	9.21	150	
KTUS	04/01/202	10.36	140	
KTUS	04/01/202	11.51	140	
KTUS	04/01/202	12.66	140	
KTUS	04/01/202	11.51	120	
KTUS	04/01/202	6.91	80	
KTUS	04/01/202	6.91	100	
KTUS	04/01/202	9.21	90	
KTUS	04/01/202	9.21	100	

KTUS	04/01/202	6.91	130	
KTUS	04/01/202	12.66	150	
KTUS	04/01/202	12.66	150	19.56
KTUS	04/01/202	16.11	140	21.86
KTUS	04/01/202	14.96	140	
KTUS	04/01/202	17.26	150	
KTUS	04/01/202	16.11	150	25.32
KTUS	04/01/202	14.96	150	21.86
KTUS	04/01/202	12.66	140	
KTUS	04/01/202	13.81	130	
KTUS	04/01/202	11.51	120	
KTUS	04/01/202	10.36	120	
KTUS	04/01/202	9.21	120	
KTUS	04/01/202	12.66	120	18.41
KTUS	04/01/202	11.51	120	
KTUS	04/01/202	17.26	150	
KTUS	04/01/202	20.71	150	
KTUS	04/01/202	18.41	140	
KTUS	04/01/202	18.41	140	
KTUS	04/01/202	17.26	140	
KTUS	04/01/202	18.41	140	
KTUS	04/01/202	19.56	140	
KTUS	04/01/202	21.86	130	27.62
KTUS	04/01/202	21.86	130	27.62
KTUS	04/01/202	21.86	130	28.77
KTUS	04/01/202	23.02	130	
KTUS	04/01/202	24.17	130	
KTUS	04/01/202	20.71	130	
KTUS	04/01/202	20.71	120	27.62
KTUS	04/01/202	18.41	120	
KTUS	04/01/202	20.71	130	26.47
KTUS	04/01/202	25.32	130	31.07
KTUS	04/01/202	25.32	130	33.37
KTUS	04/01/202	26.47	120	35.67
KTUS	04/01/202	23.02	120	
KTUS	04/01/202	23.02	120	28.77
KTUS	04/01/202	21.86	120	31.07
KTUS	04/01/202	23.02	130	28.77
KTUS	04/01/202	25.32	130	33.37
KTUS	04/01/202	25.32	130	31.07
KTUS	04/01/202	23.02	130	
KTUS	04/01/202	13.81	110	
KTUS	04/01/202	11.51	100	
KTUS	04/01/202	13.81	110	
KTUS	04/01/202	13.81	120	
KTUS	04/01/202	13.81	120	21.86
KTUS	04/01/202	13.81	110	20.71
KTUS	04/01/202	11.51	100	
KTUS	04/01/202	12.66	110	
KTUS	04/01/202	13.81	100	19.56
KTUS	04/01/202	13.81	90	
KTUS	04/01/202	11.51	110	

KTUS	04/01/202	13.81	110	
KTUS	04/01/202	12.66	110	
KTUS	04/01/202	11.51	100	
KTUS	04/01/202	16.11	100	
KTUS	04/01/202	13.81	100	
KTUS	04/01/202	16.11	110	
KTUS	04/01/202	16.11	110	
KTUS	04/01/202	14.96	120	
KTUS	04/01/202	16.11	120	
KTUS	04/01/202	14.96	120	21.86
KTUS	04/01/202	14.96	120	
KTUS	04/01/202	14.96	120	
KTUS	04/01/202	13.81	130	
KTUS	04/01/202	13.81	130	
KTUS	04/01/202	12.66	120	
KTUS	04/01/202	12.66	120	
KTUS	04/01/202	13.81	120	
KTUS	04/01/202	12.66	110	19.56
KTUS	04/01/202	13.81	120	
KTUS	04/01/202	17.26	130	24.17
KTUS	04/01/202	14.96	130	
KTUS	04/01/202	17.26	140	
KTUS	04/01/202	19.56	140	
KTUS	04/01/202	18.41	140	24.17
KTUS	04/01/202	21.86	130	27.62
KTUS	04/01/202	20.71	130	26.47
KTUS	04/01/202	21.86	130	29.92
KTUS	04/01/202	20.71	120	27.62
KTUS	04/01/202	24.17	120	
KTUS	04/01/202	26.47	120	33.37
KTUS	04/01/202	20.71	130	29.92
KTUS	04/01/202	25.32	130	33.37
KTUS	04/01/202	26.47	130	33.37
KTUS	04/01/202	25.32	130	33.37
KTUS	04/01/202	25.32	130	33.37
KTUS	04/01/202	21.86	130	29.92
KTUS	04/01/202	25.32	130	
KTUS	04/01/202	21.86	120	34.52
KTUS	04/01/202	21.86	120	
KTUS	04/01/202	21.86	120	
KTUS	04/01/202	24.17	110	31.07
KTUS	04/01/202	24.17	120	29.92
KTUS	04/01/202	19.56	120	26.47
KTUS	04/01/202	24.17	120	31.07
KTUS	04/01/202	26.47	130	36.82
KTUS	04/01/202	25.32	120	
KTUS	04/01/202	27.62	120	33.37
KTUS	04/01/202	26.47	120	32.22
KTUS	04/01/202	26.47	120	33.37
KTUS	04/01/202	26.47	120	32.22
KTUS	04/01/202	24.17	120	36.82
KTUS	04/01/202	29.92	120	36.82

KTUS	04/01/202	27.62	120	37.98
KTUS	04/01/202	27.62	120	36.82
KTUS	04/01/202	28.77	120	37.98
KTUS	04/01/202	24.17	120	33.37
KTUS	04/01/202	27.62	120	34.52
KTUS	04/01/202	27.62	120	39.13
KTUS	04/01/202	29.92	120	39.13
KTUS	04/01/202	28.77	130	34.52
KTUS	04/01/202	27.62	120	33.37
KTUS	04/01/202	29.92	130	
KTUS	04/01/202	23.02	120	35.67
KTUS	04/01/202	27.62	120	36.82
KTUS	04/01/202	23.02	110	32.22
KTUS	04/01/202	23.02	120	31.07
KTUS	04/01/202	21.86	110	29.92
KTUS	04/01/202	23.02	110	33.37
KTUS	04/01/202	24.17	110	32.22
KTUS	04/01/202	24.17	120	35.67
KTUS	04/01/202	25.32	120	37.98
KTUS	04/01/202	26.47	110	33.37
KTUS	04/01/202	20.71	110	31.07
KTUS	04/01/202	23.02	100	36.82
KTUS	04/01/202	20.71	110	26.47
KTUS	04/01/202	26.47	120	33.37
KTUS	04/01/202	20.71	110	28.77
KTUS	04/01/202	23.02	110	29.92
KTUS	04/01/202	27.62	120	
KTUS	04/01/202	20.71	110	29.92
KTUS	04/01/202	25.32	110	
KTUS	04/01/202	21.86	100	29.92
KTUS	04/01/202	20.71	110	26.47
KTUS	04/01/202	24.17	110	34.52
KTUS	04/01/202	21.86	120	32.22
KTUS	04/01/202	20.71	110	33.37
KTUS	04/01/202	21.86	110	32.22
KTUS	04/01/202	20.71	100	29.92
KTUS	04/01/202	21.86	110	32.22
KTUS	04/01/202	20.71	110	31.07
KTUS	04/01/202	21.86	110	27.62
KTUS	04/01/202	18.41	100	24.17
KTUS	04/01/202	23.02	110	31.07
KTUS	04/01/202	24.17	120	29.92
KTUS	04/01/202	20.71	100	28.77
KTUS	04/01/202	19.56	100	28.77
KTUS	04/01/202	20.71	120	29.92
KTUS	04/01/202	23.02	120	29.92
KTUS	04/01/202	21.86	120	28.77
KTUS	04/01/202	18.41	100	24.17
KTUS	04/01/202	19.56	120	
KTUS	04/01/202	19.56	100	
KTUS	04/01/202	20.71	120	
KTUS	04/01/202	18.41	100	24.17

KTUS	04/01/202	19.56	110	29.92
KTUS	04/01/202	18.41	110	
KTUS	04/01/202	19.56	110	26.47
KTUS	04/01/202	20.71	100	29.92
KTUS	04/01/202	19.56	100	27.62
KTUS	04/01/202	18.41	100	31.07
KTUS	04/01/202	18.41	100	27.62
KTUS	04/01/202	17.26	120	
KTUS	04/01/202	12.66	110	18.41
KTUS	04/01/202	17.26	110	
KTUS	04/01/202	17.26	110	
KTUS	04/01/202	13.81	110	
KTUS	04/01/202	16.11	110	27.62
KTUS	04/01/202	19.56	90	26.47
KTUS	04/01/202	18.41	90	25.32
KTUS	04/01/202	14.96	100	
KTUS	04/01/202	14.96	100	
KTUS	04/01/202	17.26	110	24.17
KTUS	04/01/202	18.41	110	27.62
KTUS	04/01/202	18.41	100	
KTUS	04/01/202	17.26	90	26.47
KTUS	04/01/202	17.26	100	25.32
KTUS	04/01/202	14.96	100	21.86
KTUS	04/01/202	18.41	100	27.62
KTUS	04/01/202	20.71	100	
KTUS	04/01/202	19.56	90	27.62
KTUS	04/01/202	20.71	100	
KTUS	04/01/202	21.86	90	28.77
KTUS	04/01/202	20.71	90	29.92
KTUS	04/01/202	19.56	100	28.77
KTUS	04/01/202	18.41	90	26.47
KTUS	04/01/202	16.11	100	29.92
KTUS	04/01/202	20.71	90	29.92
KTUS	04/01/202	20.71	100	
KTUS	04/01/202	23.02	90	28.77
KTUS	04/01/202	20.71	90	26.47
KTUS	04/01/202	18.41	90	28.77
KTUS	04/01/202	20.71	80	29.92
KTUS	04/01/202	17.26	90	
KTUS	04/01/202	19.56	90	27.62
KTUS	04/01/202	21.86	90	27.62
KTUS	04/01/202	23.02	90	
KTUS	04/01/202	20.71	90	26.47
KTUS	04/01/202	18.41	80	26.47
KTUS	04/01/202	18.41	80	27.62
KTUS	04/01/202	18.41	100	25.32
KTUS	04/01/202	18.41	90	25.32
KTUS	04/01/202	17.26	100	
KTUS	04/01/202	16.11	110	21.86
KTUS	04/01/202	13.81	100	
KTUS	04/01/202	17.26	100	
KTUS	04/01/202	17.26	110	

KTUS	04/01/202	18.41	110	
KTUS	04/01/202	16.11	90	21.86
KTUS	04/01/202	13.81	100	20.71
KTUS	04/01/202	14.96	110	
KTUS	04/01/202	16.11	100	
KTUS	04/01/202	17.26	100	25.32
KTUS	04/01/202	16.11	100	
KTUS	04/01/202	16.11	100	
KTUS	04/01/202	13.81	90	19.56
KTUS	04/01/202	19.56	90	25.32
KTUS	04/01/202	16.11	90	25.32
KTUS	04/01/202	14.96	100	20.71
KTUS	04/01/202	14.96	100	
KTUS	04/01/202	11.51	90	
KTUS	04/01/202	13.81	80	20.71
KTUS	04/01/202	12.66	90	
KTUS	04/01/202	11.51	80	17.26
KTUS	04/01/202	11.51	70	
KTUS	04/01/202	11.51	70	
KTUS	04/01/202	11.51	70	
KTUS	04/01/202	10.36	70	16.11
KTUS	04/01/202	14.96	80	
KTUS	04/01/202	10.36	70	
KTUS	04/01/202	11.51	80	
KTUS	04/01/202	12.66	90	18.41
KTUS	04/01/202	14.96	90	
KTUS	04/01/202	10.36	90	17.26
KTUS	04/01/202	10.36	80	16.11
KTUS	04/01/202	10.36	80	
KTUS	04/01/202	11.51	100	
KTUS	04/01/202	12.66	100	
KTUS	04/01/202	11.51	100	
KTUS	04/01/202	13.81	90	
KTUS	04/01/202	12.66	100	18.41
KTUS	04/01/202	13.81	100	
KTUS	04/01/202	12.66	100	
KTUS	04/01/202	12.66	100	
KTUS	04/01/202	11.51	100	18.41
KTUS	04/01/202	12.66	100	
KTUS	04/01/202	10.36	90	
KTUS	04/01/202	10.36	90	
KTUS	04/01/202	9.21	90	
KTUS	04/01/202	9.21	80	
KTUS	04/01/202	9.21	80	
KTUS	04/01/202	9.21	90	
KTUS	04/01/202	9.21	90	
KTUS	04/01/202	8.06	100	
KTUS	04/01/202	9.21	110	
KTUS	04/01/202	9.21	90	
KTUS	04/01/202	5.75	90	
KTUS	04/01/202	5.75	80	
KTUS	04/01/202	5.75	100	

KTUS	04/01/202	8.06	100
KTUS	04/01/202	9.21	90
KTUS	04/01/202	4.6	80
KTUS	04/01/202	3.45	90
KTUS	04/01/202	4.6	110
KTUS	04/01/202	5.75	100
KTUS	04/01/202	5.75	100
KTUS	04/01/202	6.91	90

STATION: KTUS
STATION NAME: Tucson International Airport
LATITUDE: 32.13153
LONGITUDE: -110.95635
ELEVATION [ft]: 2546
STATE: AZ

Station_ID	Date_Time	wind_speed_set_1	wind_direction_set_1	wind_gust_set_1
		Miles/hour	Degrees	Miles/hour
KTUS	07/11/2021 22:00 MST	8.06	250	
KTUS	07/11/2021 22:05 MST	8.06	260	
KTUS	07/11/2021 22:10 MST	9.21	270	
KTUS	07/11/2021 22:15 MST	8.06	270	
KTUS	07/11/2021 22:20 MST	10.36	270	
KTUS	07/11/2021 22:25 MST	8.06	270	
KTUS	07/11/2021 22:30 MST	11.51	270	
KTUS	07/11/2021 22:35 MST	11.51	270	
KTUS	07/11/2021 22:40 MST	10.36	280	16.11
KTUS	07/11/2021 22:45 MST	12.66	270	18.41
KTUS	07/11/2021 22:50 MST	12.66	280	
KTUS	07/11/2021 22:53 MST	9.21	270	19.56
KTUS	07/11/2021 22:55 MST	9.21	270	
KTUS	07/11/2021 23:00 MST	9.21	270	
KTUS	07/11/2021 23:05 MST	6.91	260	
KTUS	07/11/2021 23:10 MST	6.91	270	
KTUS	07/11/2021 23:15 MST	8.06	270	
KTUS	07/11/2021 23:20 MST	6.91	270	
KTUS	07/11/2021 23:25 MST	6.91	260	
KTUS	07/11/2021 23:29 MST	6.91	240	
KTUS	07/11/2021 23:30 MST	6.91	240	
KTUS	07/11/2021 23:35 MST	6.91	260	
KTUS	07/11/2021 23:40 MST	9.21	280	
KTUS	07/11/2021 23:45 MST	10.36	280	
KTUS	07/11/2021 23:50 MST	9.21	280	
KTUS	07/11/2021 23:53 MST	6.91	270	
KTUS	07/11/2021 23:55 MST	4.6	270	
KTUS	07/12/2021 00:00 MST	3.45	230	
KTUS	07/12/2021 00:05 MST	0	0	
KTUS	07/12/2021 00:10 MST	4.6	70	
KTUS	07/12/2021 00:15 MST	4.6	110	
KTUS	07/12/2021 00:20 MST	6.91	120	
KTUS	07/12/2021 00:25 MST	10.36	120	
KTUS	07/12/2021 00:30 MST	9.21	110	
KTUS	07/12/2021 00:35 MST	5.75	120	
KTUS	07/12/2021 00:40 MST	5.75	140	
KTUS	07/12/2021 00:45 MST	9.21	150	
KTUS	07/12/2021 00:50 MST	8.06	130	
KTUS	07/12/2021 00:53 MST	8.06	150	
KTUS	07/12/2021 00:55 MST	8.06	170	
KTUS	07/12/2021 01:00 MST	9.21	190	
KTUS	07/12/2021 01:05 MST	11.51	180	17.26
KTUS	07/12/2021 01:10 MST	11.51	180	
KTUS	07/12/2021 01:15 MST	18.41	180	

KTUS	07/12/2021 01:20 MST	16.11	170	
KTUS	07/12/2021 01:25 MST	21.86	180	
KTUS	07/12/2021 01:30 MST	14.96	170	
KTUS	07/12/2021 01:35 MST	14.96	180	
KTUS	07/12/2021 01:39 MST	13.81	180	
KTUS	07/12/2021 01:40 MST	13.81	180	
KTUS	07/12/2021 01:45 MST	13.81	180	
KTUS	07/12/2021 01:50 MST	13.81	180	
KTUS	07/12/2021 01:53 MST	12.66	180	
KTUS	07/12/2021 01:55 MST	12.66	180	
KTUS	07/12/2021 02:00 MST	13.81	160	
KTUS	07/12/2021 02:05 MST	10.36	130	
KTUS	07/12/2021 02:10 MST	9.21	140	
KTUS	07/12/2021 02:15 MST	10.36	140	
KTUS	07/12/2021 02:20 MST	10.36	150	
KTUS	07/12/2021 02:25 MST	21.86	200	29.92
KTUS	07/12/2021 02:30 MST	16.11	200	
KTUS	07/12/2021 02:35 MST	16.11	210	25.32
KTUS	07/12/2021 02:37 MST	17.26	210	27.62
KTUS	07/12/2021 02:40 MST	18.41	210	25.32
KTUS	07/12/2021 02:45 MST	20.71	210	27.62
KTUS	07/12/2021 02:50 MST	14.96	210	21.86
KTUS	07/12/2021 02:53 MST	18.41	210	31.07
KTUS	07/12/2021 02:55 MST	14.96	200	
KTUS	07/12/2021 03:00 MST	19.56	200	
KTUS	07/12/2021 03:05 MST	17.26	200	25.32
KTUS	07/12/2021 03:10 MST	17.26	190	
KTUS	07/12/2021 03:15 MST	18.41	200	
KTUS	07/12/2021 03:20 MST	14.96	200	
KTUS	07/12/2021 03:25 MST	16.11	190	24.17
KTUS	07/12/2021 03:30 MST	13.81	170	
KTUS	07/12/2021 03:35 MST	17.26	170	
KTUS	07/12/2021 03:40 MST	10.36	170	
KTUS	07/12/2021 03:45 MST	13.81	160	20.71
KTUS	07/12/2021 03:50 MST	11.51	170	
KTUS	07/12/2021 03:53 MST	12.66	170	21.86
KTUS	07/12/2021 03:55 MST	11.51	160	
KTUS	07/12/2021 04:00 MST	10.36	150	
KTUS	07/12/2021 04:05 MST	10.36	160	
KTUS	07/12/2021 04:10 MST	12.66	170	
KTUS	07/12/2021 04:15 MST	11.51	160	17.26
KTUS	07/12/2021 04:20 MST	9.21	150	
KTUS	07/12/2021 04:25 MST	8.06	150	
KTUS	07/12/2021 04:30 MST	10.36	170	
KTUS	07/12/2021 04:35 MST	8.06	160	
KTUS	07/12/2021 04:40 MST	9.21	170	
KTUS	07/12/2021 04:45 MST	9.21	170	
KTUS	07/12/2021 04:50 MST	9.21	160	
KTUS	07/12/2021 04:53 MST	6.91	160	
KTUS	07/12/2021 04:55 MST	8.06	160	
KTUS	07/12/2021 05:00 MST	10.36	170	
KTUS	07/12/2021 05:05 MST	10.36	150	

KTUS	07/12/2021 05:10 MST	9.21	160
KTUS	07/12/2021 05:15 MST	8.06	180
KTUS	07/12/2021 05:20 MST	8.06	180
KTUS	07/12/2021 05:25 MST	11.51	180
KTUS	07/12/2021 05:30 MST	9.21	170
KTUS	07/12/2021 05:35 MST	8.06	160
KTUS	07/12/2021 05:40 MST	6.91	160
KTUS	07/12/2021 05:45 MST	6.91	170
KTUS	07/12/2021 05:50 MST	4.6	180
KTUS	07/12/2021 05:53 MST	6.91	190
KTUS	07/12/2021 05:55 MST	5.75	170
KTUS	07/12/2021 06:00 MST	8.06	160
KTUS	07/12/2021 06:05 MST	8.06	170
KTUS	07/12/2021 06:10 MST	6.91	160
KTUS	07/12/2021 06:15 MST	6.91	160
KTUS	07/12/2021 06:20 MST	6.91	150
KTUS	07/12/2021 06:25 MST	6.91	150
KTUS	07/12/2021 06:30 MST	6.91	150
KTUS	07/12/2021 06:35 MST	6.91	160
KTUS	07/12/2021 06:40 MST	8.06	180
KTUS	07/12/2021 06:45 MST	10.36	170
KTUS	07/12/2021 06:50 MST	10.36	170
KTUS	07/12/2021 06:53 MST	12.66	170
KTUS	07/12/2021 06:55 MST	11.51	160
KTUS	07/12/2021 07:00 MST	12.66	170
KTUS	07/12/2021 07:05 MST	12.66	170
KTUS	07/12/2021 07:10 MST	12.66	160
KTUS	07/12/2021 07:15 MST	10.36	180
KTUS	07/12/2021 07:20 MST	12.66	180
KTUS	07/12/2021 07:25 MST	12.66	170
KTUS	07/12/2021 07:30 MST	11.51	170
KTUS	07/12/2021 07:35 MST	12.66	160
KTUS	07/12/2021 07:40 MST	11.51	180
KTUS	07/12/2021 07:45 MST	10.36	170
KTUS	07/12/2021 07:50 MST	11.51	170
KTUS	07/12/2021 07:53 MST	10.36	170
KTUS	07/12/2021 07:55 MST	10.36	170
KTUS	07/12/2021 08:00 MST	8.06	170
KTUS	07/12/2021 08:05 MST	9.21	150
KTUS	07/12/2021 08:10 MST	9.21	170
KTUS	07/12/2021 08:15 MST	8.06	170
KTUS	07/12/2021 08:20 MST	8.06	180
KTUS	07/12/2021 08:25 MST	6.91	150
KTUS	07/12/2021 08:30 MST	6.91	170
KTUS	07/12/2021 08:35 MST	6.91	170
KTUS	07/12/2021 08:40 MST	5.75	170
KTUS	07/12/2021 08:45 MST	8.06	160
KTUS	07/12/2021 08:50 MST	4.6	110
KTUS	07/12/2021 08:53 MST	6.91	170
KTUS	07/12/2021 08:55 MST	5.75	150
KTUS	07/12/2021 09:00 MST	5.75	140
KTUS	07/12/2021 09:05 MST	5.75	140

KTUS	07/12/2021 09:10 MST	5.75	160	
KTUS	07/12/2021 09:15 MST	4.6	160	
KTUS	07/12/2021 09:20 MST	4.6	150	
KTUS	07/12/2021 09:25 MST	6.91	140	
KTUS	07/12/2021 09:30 MST	6.91	160	
KTUS	07/12/2021 09:35 MST	8.06	150	
KTUS	07/12/2021 09:40 MST	6.91	170	
KTUS	07/12/2021 09:45 MST	4.6	180	
KTUS	07/12/2021 09:50 MST	3.45	170	
KTUS	07/12/2021 09:53 MST	4.6	190	
KTUS	07/12/2021 09:55 MST	8.06	170	
KTUS	07/12/2021 10:00 MST	4.6	180	
KTUS	07/12/2021 10:05 MST	0	0	
KTUS	07/12/2021 10:10 MST	4.6	180	
KTUS	07/12/2021 10:15 MST	4.6	170	
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KTUS	07/12/2021 10:25 MST	3.45	250	
KTUS	07/12/2021 10:30 MST	4.6	160	
KTUS	07/12/2021 10:35 MST	0	0	
KTUS	07/12/2021 10:40 MST	3.45	180	
KTUS	07/12/2021 10:45 MST	3.45	260	
KTUS	07/12/2021 10:50 MST	0	0	
KTUS	07/12/2021 10:53 MST	3.45		
KTUS	07/12/2021 10:55 MST	4.6	190	
KTUS	07/12/2021 11:00 MST	0	0	
KTUS	07/12/2021 11:05 MST			
KTUS	07/12/2021 11:10 MST	0	0	
KTUS	07/12/2021 11:15 MST	3.45	40	
KTUS	07/12/2021 11:20 MST	0	0	
KTUS	07/12/2021 11:25 MST	5.75	320	
KTUS	07/12/2021 11:30 MST	8.06	310	
KTUS	07/12/2021 11:35 MST	4.6	340	
KTUS	07/12/2021 11:40 MST	6.91	300	
KTUS	07/12/2021 11:45 MST	4.6	300	
KTUS	07/12/2021 11:50 MST	8.06	30	
KTUS	07/12/2021 11:53 MST	5.75		
KTUS	07/12/2021 11:55 MST	9.21	330	
KTUS	07/12/2021 12:00 MST	9.21	360	
KTUS	07/12/2021 12:05 MST	5.75	340	
KTUS	07/12/2021 12:10 MST	5.75	10	
KTUS	07/12/2021 12:15 MST	5.75	280	
KTUS	07/12/2021 12:17 MST	5.75		
KTUS	07/12/2021 12:20 MST	8.06	300	
KTUS	07/12/2021 12:25 MST	10.36	330	
KTUS	07/12/2021 12:30 MST	4.6	320	
KTUS	07/12/2021 12:35 MST	5.75	310	
KTUS	07/12/2021 12:40 MST	6.91	330	16.11
KTUS	07/12/2021 12:45 MST	6.91	330	16.11
KTUS	07/12/2021 12:50 MST	6.91	330	16.11
KTUS	07/12/2021 12:53 MST	6.91	330	
KTUS	07/12/2021 12:55 MST	4.6	300	
KTUS	07/12/2021 13:00 MST	5.75	60	

KTUS	07/12/2021 13:05 MST	4.6	50	
KTUS	07/12/2021 13:10 MST	0	0	
KTUS	07/12/2021 13:15 MST			
KTUS	07/12/2021 13:20 MST	6.91	30	
KTUS	07/12/2021 13:25 MST	5.75	10	
KTUS	07/12/2021 13:30 MST	4.6	20	
KTUS	07/12/2021 13:35 MST	3.45	360	
KTUS	07/12/2021 13:40 MST	6.91	330	
KTUS	07/12/2021 13:45 MST			
KTUS	07/12/2021 13:50 MST	4.6	280	16.11
KTUS	07/12/2021 13:53 MST	4.6	280	
KTUS	07/12/2021 13:55 MST	4.6	290	
KTUS	07/12/2021 14:00 MST	10.36	270	
KTUS	07/12/2021 14:05 MST	0	0	
KTUS	07/12/2021 14:10 MST	8.06	20	
KTUS	07/12/2021 14:15 MST	0	0	
KTUS	07/12/2021 14:20 MST	5.75	350	
KTUS	07/12/2021 14:25 MST	4.6	360	
KTUS	07/12/2021 14:30 MST	4.6	320	
KTUS	07/12/2021 14:35 MST	5.75	260	
KTUS	07/12/2021 14:40 MST	4.6	360	
KTUS	07/12/2021 14:45 MST			
KTUS	07/12/2021 14:50 MST	8.06	290	16.11
KTUS	07/12/2021 14:53 MST	8.06	290	
KTUS	07/12/2021 14:55 MST	10.36	330	
KTUS	07/12/2021 15:00 MST	0	0	
KTUS	07/12/2021 15:05 MST	3.45	100	
KTUS	07/12/2021 15:10 MST			
KTUS	07/12/2021 15:15 MST	8.06	320	
KTUS	07/12/2021 15:20 MST	8.06	290	
KTUS	07/12/2021 15:25 MST	8.06	280	
KTUS	07/12/2021 15:30 MST	9.21	330	
KTUS	07/12/2021 15:35 MST	3.45	30	
KTUS	07/12/2021 15:40 MST	4.6	310	
KTUS	07/12/2021 15:45 MST	0	0	
KTUS	07/12/2021 15:50 MST	6.91	280	
KTUS	07/12/2021 15:53 MST	9.21	270	
KTUS	07/12/2021 15:55 MST	8.06	320	
KTUS	07/12/2021 16:00 MST	4.6	300	
KTUS	07/12/2021 16:05 MST	3.45	250	
KTUS	07/12/2021 16:10 MST	10.36	250	
KTUS	07/12/2021 16:15 MST	0	0	
KTUS	07/12/2021 16:20 MST	8.06	270	
KTUS	07/12/2021 16:25 MST	8.06	280	
KTUS	07/12/2021 16:30 MST	5.75	280	
KTUS	07/12/2021 16:35 MST	8.06	290	
KTUS	07/12/2021 16:40 MST	9.21	320	
KTUS	07/12/2021 16:45 MST			
KTUS	07/12/2021 16:50 MST	0	0	
KTUS	07/12/2021 16:53 MST			
KTUS	07/12/2021 16:55 MST			
KTUS	07/12/2021 16:57 MST	8.06	320	

KTUS	07/12/2021 17:00 MST	8.06	320	16.11
KTUS	07/12/2021 17:05 MST	8.06	320	16.11
KTUS	07/12/2021 17:10 MST	8.06	320	16.11
KTUS	07/12/2021 17:15 MST	8.06	320	16.11
KTUS	07/12/2021 17:20 MST	8.06	320	16.11
KTUS	07/12/2021 17:25 MST	8.06	320	16.11
KTUS	07/12/2021 17:30 MST	8.06	320	16.11
KTUS	07/12/2021 17:35 MST	8.06	320	16.11
KTUS	07/12/2021 17:40 MST	8.06	320	16.11
KTUS	07/12/2021 17:45 MST	8.06	320	16.11
KTUS	07/12/2021 17:50 MST	8.06	320	16.11
KTUS	07/12/2021 17:53 MST	8.06	320	
KTUS	07/12/2021 17:55 MST	10.36	300	
KTUS	07/12/2021 18:00 MST	10.36	320	
KTUS	07/12/2021 18:05 MST	8.06	310	
KTUS	07/12/2021 18:10 MST	6.91	320	
KTUS	07/12/2021 18:15 MST	8.06	310	
KTUS	07/12/2021 18:20 MST	8.06	280	
KTUS	07/12/2021 18:25 MST	8.06	290	
KTUS	07/12/2021 18:30 MST	9.21	300	
KTUS	07/12/2021 18:35 MST	8.06	300	
KTUS	07/12/2021 18:40 MST	8.06	300	
KTUS	07/12/2021 18:45 MST	8.06	300	
KTUS	07/12/2021 18:50 MST	8.06	290	
KTUS	07/12/2021 18:53 MST	9.21	290	
KTUS	07/12/2021 18:55 MST	9.21	290	
KTUS	07/12/2021 19:00 MST	9.21	280	
KTUS	07/12/2021 19:05 MST	8.06	310	
KTUS	07/12/2021 19:10 MST	6.91	310	
KTUS	07/12/2021 19:15 MST	9.21	320	
KTUS	07/12/2021 19:20 MST	11.51	330	
KTUS	07/12/2021 19:25 MST	9.21	350	
KTUS	07/12/2021 19:30 MST	9.21	330	
KTUS	07/12/2021 19:35 MST	10.36	340	
KTUS	07/12/2021 19:40 MST	10.36	320	
KTUS	07/12/2021 19:45 MST	10.36	330	
KTUS	07/12/2021 19:50 MST	12.66	330	
KTUS	07/12/2021 19:53 MST	12.66	340	
KTUS	07/12/2021 19:55 MST	11.51	340	
KTUS	07/12/2021 20:00 MST	10.36	340	
KTUS	07/12/2021 20:05 MST	12.66	330	
KTUS	07/12/2021 20:10 MST	10.36	340	
KTUS	07/12/2021 20:20 MST	10.36	340	
KTUS	07/12/2021 20:25 MST	10.36	340	
KTUS	07/12/2021 20:30 MST	10.36	330	
KTUS	07/12/2021 20:35 MST	9.21	330	
KTUS	07/12/2021 20:40 MST	8.06	330	
KTUS	07/12/2021 20:45 MST	10.36	340	
KTUS	07/12/2021 20:50 MST	9.21	330	
KTUS	07/12/2021 20:53 MST	10.36	330	
KTUS	07/12/2021 20:55 MST	9.21	330	
KTUS	07/12/2021 21:00 MST	10.36	340	

KTUS	07/12/2021 21:05 MST	10.36	340	
KTUS	07/12/2021 21:10 MST	8.06	350	
KTUS	07/12/2021 21:15 MST	6.91	350	
KTUS	07/12/2021 21:20 MST	4.6	280	
KTUS	07/12/2021 21:25 MST	11.51	220	
KTUS	07/12/2021 21:30 MST	18.41	200	
KTUS	07/12/2021 21:35 MST	27.62	190	41.43
KTUS	07/12/2021 21:40 MST	27.62	190	34.52
KTUS	07/12/2021 21:45 MST	26.47	180	33.37
KTUS	07/12/2021 21:46 MST	26.47	180	42.58
KTUS	07/12/2021 21:50 MST	28.77	200	37.98
KTUS	07/12/2021 21:53 MST	26.47	200	39.13
KTUS	07/12/2021 21:55 MST	25.32	200	34.52
KTUS	07/12/2021 22:00 MST	19.56	150	28.77
KTUS	07/12/2021 22:05 MST	11.51	170	18.41
KTUS	07/12/2021 22:10 MST			
KTUS	07/12/2021 22:13 MST	20.71	90	33.37
KTUS	07/12/2021 22:15 MST	21.86	80	31.07
KTUS	07/12/2021 22:20 MST	29.92	50	37.98
KTUS	07/12/2021 22:22 MST	25.32	50	42.58
KTUS	07/12/2021 22:25 MST	14.96	40	
KTUS	07/12/2021 22:30 MST	11.51	300	17.26
KTUS	07/12/2021 22:33 MST	13.81	290	23.02
KTUS	07/12/2021 22:35 MST	16.11	310	
KTUS	07/12/2021 22:40 MST	17.26	310	
KTUS	07/12/2021 22:43 MST	13.81	290	
KTUS	07/12/2021 22:45 MST	13.81	280	20.71
KTUS	07/12/2021 22:50 MST	17.26	260	25.32
KTUS	07/12/2021 22:53 MST	18.41	250	25.32
KTUS	07/12/2021 22:55 MST	17.26	250	
KTUS	07/12/2021 23:00 MST	14.96	260	21.86
KTUS	07/12/2021 23:02 MST	13.81	270	26.47
KTUS	07/12/2021 23:05 MST	14.96	260	20.71
KTUS	07/12/2021 23:10 MST	17.26	230	
KTUS	07/12/2021 23:13 MST	16.11	220	
KTUS	07/12/2021 23:15 MST	14.96	220	
KTUS	07/12/2021 23:20 MST	14.96	210	
KTUS	07/12/2021 23:22 MST	16.11	210	
KTUS	07/12/2021 23:25 MST	17.26	210	
KTUS	07/12/2021 23:30 MST	19.56	210	
KTUS	07/12/2021 23:35 MST	14.96	160	
KTUS	07/12/2021 23:40 MST	14.96	170	
KTUS	07/12/2021 23:45 MST	16.11	170	
KTUS	07/12/2021 23:49 MST	16.11	170	
KTUS	07/12/2021 23:50 MST	16.11	170	
KTUS	07/12/2021 23:53 MST	16.11	160	
KTUS	07/12/2021 23:55 MST	14.96	160	

APPENDIX C. ADEQ BACKGROUND VALUE COMMUNICATIONS

From: Feng Mao
To: Shannon Manoulian
Cc: David Strohm
Subject: Re: Rosemont Copper Background Concentrations
Date: Wednesday, September 7, 2022 8:26:38 AM
Attachments: image001.png
image002.jpg

Good morning, Shannon. Thank you for reaching out to me. ADEQ developed the rural background concentrations 20 years ago so the data were outdated. My understanding is that Rosemont is proposing to use the Alamo Lake data to determine the background concentration for 1-hour NO2 and the Tucson data to determine the background concentration for 1-hour SO2. To be consistent, I would recommend using the Alamo Lake data to determine the annual NO2 background concentration and the Tucson data (Children's Park Ncore) to determine the background concentrations for 3-hour SO2 and 1-hour/8-hour CO.

I did a quick review on the monitoring data and summarized the data as follows.

Pollutants	Monitor	Averaging Time	Background		Note
			(ppb)	(ug/m3)	
CO	Children'S Park Ncore	1-hour	800	920	EPA 2021 Design Value Report[1]
CO	Children'S Park Ncore	8-hour	500	575	EPA 2021 Design Value Report [1]
SO2	Children'S Park Ncore	1-hour	1	2.6	EPA 2021 Design Value Report[1]
SO2	Children'S Park Ncore	3-hour	1.3	3.4	Highest 3-hour average concentration over 2019-2021
NO2	Alamo Lake	1-hour	14	26.3	Used in the previous Rosemont modeling based on 2014-2016 data
NO2	Alamo Lake	Annual	1.36	2.6	Highest Annual concentration based on 2014-2016 data

[1] https://www.epa.gov/air-trends/air-quality-design-values

If you have any questions, please let me know.

Thank you!

Feng Mao, PhD, PE
Air Quality Facilities Emission Control
Ph: 520-628-6719

APPENDIX D. O_3 AND $PM_{2.5}$ DATA STATISTICAL ANALYSIS

O3 - Green Valley

Step 1 - Determine highest 8-hour concentrations from 3-year data set and remove from consideration									3-Year Average (2019-2021)
High	2014	2015	2016	2017	2018	2019	2020	2021	
1	0.0670	0.0610	0.0700	0.0740	0.0670	0.0640	0.0690	0.0700	0.0677
2	0.0660	0.0600	0.0690	0.0680	0.0670	0.0620	0.0690	0.0680	0.0663
3	0.0650	0.0590	0.0680	0.0680	0.0650	0.0600	0.0680	0.0650	0.0643
4	0.0650	0.0590	0.0660	0.0670	0.0650	0.0600	0.0660	0.0650	0.0637
5	0.0640	0.0580	0.0650	0.0660	0.0650	0.0600	0.0660	0.0650	0.0637
6	0.0630	0.0580	0.0650	0.0650	0.0650	0.0600	0.0650	0.0640	0.0630

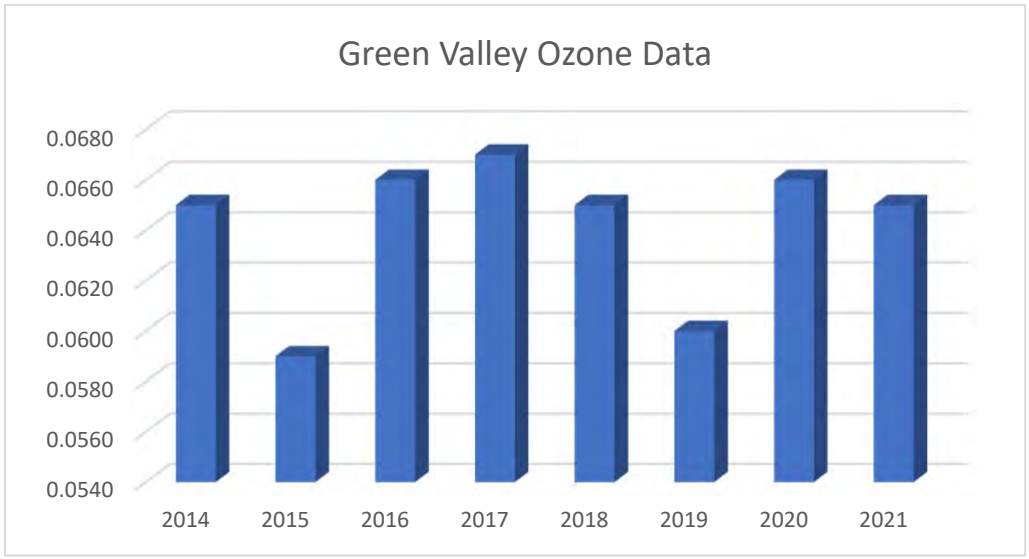

Table 2. SGE PM2.5 24-Hour 98th Percentile n^{th} Values

Year	Annual Number of Creditable Samples	98th Percentile n^{th} Maximum 24-Hour Average Value [1]
2019	109	3
2020	122	3
2021	117	3

1. Based on Table 1 of 40 CFR Part 50 Appendix N.

Table 3. SGE $PM_{2.5}$ Annual and 24-Hour 3-Year Summary Statistics

Pollutant	Form of the Standard	2019	2020	2021	3-Year Summary Statistic (Updated)	
$PM_{2.5}$ Annual	Arithmetic Mean	3.2	4.2	4.2	Average	3.9
$PM_{2.5}$ 24-Hour	98th Percentile	5.6	11.6	10.0	Average	9.1

APPENDIX E. NO_X IN-STACK RATIO DATA

Site Name	State (facility)	Facility Description	Equipment class	Equipment description	Fuel Type	Equipment capacity	Control Equipment 1	Control Equipment 2	Test date	Load (% of capacity)	Operation mode	Output units	Avg. NO2	Avg Nox	Ratio	Reporting entity
Peter Pan Seafoods King Cove Facility	Ak	Seafood Processor	Reciprocating IC Engine	Detroit Diesel 16V149TI	Diesel/Kerosene	1,000 kW	Uncontrolled	Uncontrolled	10/25/2012	35	Routine	ppmv	26.2	438	0.0598174	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Detroit Diesel 16V149TI	Diesel/Kerosene	1,000 kW	Uncontrolled	Uncontrolled	10/26/2012	48	Routine	ppmv	26.7	628	0.0425159	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Detroit Diesel 16V149TI	Diesel/Kerosene	1,000 kW	Uncontrolled	Uncontrolled	10/26/2012	65	Routine	ppmv	36.8	871	0.0422503	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Detroit Diesel 16V149TI	Diesel/Kerosene	1,000 kW	Uncontrolled	Uncontrolled	10/26/2012	55	Routine	ppmv	28.2	721	0.0391123	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512C	Diesel/Kerosene	1,050 kW	Uncontrolled		4/13/2012	30	Routine	ppmv	15	415	0.0361446	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512C	Diesel/Kerosene	1,050 kW	Uncontrolled		4/13/2012	60	Routine	ppmv	12.3	559	0.0220036	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512C	Diesel/Kerosene	1,050 kW	Uncontrolled		4/14/2012	90	Routine	ppmv	19.4	726	0.0267218	ADEC
Dillingham Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512B	Diesel/Kerosene	1,050 kW-e	Uncontrolled	Uncontrolled	10/2/2012	100	Routine	ppmv	66.9	1056	0.0633523	ADEC
Dillingham Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512B	Diesel/Kerosene	1,050 kW-e	Uncontrolled	Uncontrolled	10/3/2012	25	Routine	ppmv	28.1	571	0.0492119	ADEC
Dillingham Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512B	Diesel/Kerosene	1,050 kW-e	Uncontrolled	Uncontrolled	10/3/2012	50	Routine	ppmv	22.5	666	0.0337838	ADEC
Dillingham Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512B	Diesel/Kerosene	1,050 kW-e	Uncontrolled	Uncontrolled	10/4/2012	75	Routine	ppmv	37.7	834	0.0452038	ADEC
Peter Pan Seafoods King Cove Facility	Ak	Seafood Processor	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,100 kW	Uncontrolled	Uncontrolled	10/24/2012	47	Routine	ppmv	164.2	1665	0.0986186	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,100 kW	Uncontrolled	Uncontrolled	10/24/2012	65	Routine	ppmv	165.2	1860	0.0888172	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,100 kW	Uncontrolled	Uncontrolled	10/25/2012	78	Routine	ppmv	154.7	1882	0.0821998	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,100 kW	Uncontrolled	Uncontrolled	10/25/2012	96	Routine	ppmv	138.1	1833	0.075341	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,135 kW	Uncontrolled		4/14/2012	40	Routine	ppmv	128.4	1534	0.0837027	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,135 kW	Uncontrolled		4/14/2012	60	Routine	ppmv	148.2	1986	0.0746224	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	1,135 kW	Uncontrolled		4/15/2012	90	Routine	ppmv	123.4	1963	0.062863	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516B	Diesel/Kerosene	1,285 kW	Uncontrolled		4/11/2012	30	Routine	ppmv	54.7	901	0.0607103	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516B	Diesel/Kerosene	1,285 kW	Uncontrolled		4/11/2012	50	Routine	ppmv	78.7	1183	0.0665258	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516B	Diesel/Kerosene	1,285 kW	Uncontrolled		4/12/2012	80	Routine	ppmv	76.2	1128	0.0675532	ADEC
Peter Pan Seafoods King Cove Facility	Ak	Seafood Processor	Reciprocating IC Engine	Caterpillar 3606	Diesel/Kerosene	1,500 kW	Uncontrolled	Uncontrolled	10/23/2012	100	Routine	ppmv	147	1861	0.0789898	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3606	Diesel/Kerosene	1,500 kW	Uncontrolled	Uncontrolled	10/23/2012	80	Routine	ppmv	146.8	1869	0.0785447	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3606	Diesel/Kerosene	1,500 kW	Uncontrolled	Uncontrolled	10/23/2012	66	Routine	ppmv	141.1	1799	0.0784325	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3606	Diesel/Kerosene	1,500 kW	Uncontrolled	Uncontrolled	10/24/2012	47	Routine	ppmv	129.8	1674	0.0775388	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar C175-16	Diesel/Kerosene	1,930 kW	Uncontrolled		4/12/2012	60	Routine	ppmv	14.5	503	0.028827	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar C175-16	Diesel/Kerosene	1,930 kW	Uncontrolled		4/12/2012	50	Routine	ppmv	14.4	499	0.0288577	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar C175-16	Diesel/Kerosene	1,930 kW	Uncontrolled		4/13/2012	30	Routine	ppmv	18.2	515	0.0353398	ADEC
DU-JBER-Electric, Gas, Drinking Water and Sa	AK	LFG Power Plant	Reciprocating IC Engine	Jenbacher JGS 420 Engir	Diesel/Kerosene	1,966 bhp	Not listed - provi	Uncontrolled	11/26/2012	100	Routine	ppmv	21	95	0.2210526	ADEC
Dillingham Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3512B	Diesel/Kerosene	1.050 kW-e	Uncontrolled	Uncontrolled	10/4/2012	100	Routine	ppmv	59.3	1003	0.0591226	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3412	Diesel/Kerosene	1.54 MMBtu	Uncontrolled	Uncontrolled	10/28/2012	100	Routine	ppmv	34.8	657	0.052968	ADEC
Dutch Harbor Power Plant	AK	Power Plant	Reciprocating IC Engine	Caterpillar C-280	Diesel/Kerosene	4,400 kW-e	Centrifugal Colle	Uncontrolled	8/8/2012	100	Routine	ppmv	48	1066	0.0450281	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	440 kW	Uncontrolled		4/15/2012	30	Routine	ppmv	79.9	1186	0.0673693	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	440 kW	Uncontrolled		4/15/2012	70	Routine	ppmv	133.3	1914	0.0696447	ADEC
Tok Power Generation Station	AK	Power Plant	Reciprocating IC Engine	Caterpillar 3516	Diesel/Kerosene	440 kW	Uncontrolled		4/16/2012	100	Routine	ppmv	167	2241	0.0745203	ADEC
Dutch Harbo Power Plant	AK	Power Plant	Reciprocating IC Engine	Wartsila Model 12V32C	Diesel/Kerosene	5211 kWe	Uncontrolled	Uncontrolled	2/2/2011	50	Routine	ppmv	62.1	1125	0.0552	ADEC
Peter Pan Seafoods King Cove Facility	Ak	Seafood Processor	Reciprocating IC Engine	Caterpillar 3512	Diesel/Kerosene	810 kW	Uncontrolled	Uncontrolled	10/27/2012	99	Routine	ppmv	146.5	1842	0.0795331	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3512	Diesel/Kerosene	810 kW	Uncontrolled	Uncontrolled	10/27/2012	84	Routine	ppmv	155	1875	0.0826667	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3512	Diesel/Kerosene	810 kW	Uncontrolled	Uncontrolled	10/27/2012	69	Routine	ppmv	163.9	1857	0.0882606	ADEC
Peter Pan Seafoods King Cove Facility	AK	Seafood Processor	Reciprocating IC Engine	Caterpillar 3512	Diesel/Kerosene	810 kW	Uncontrolled	Uncontrolled	10/28/2012	49	Routine	ppmv	171.5	1789	0.0958636	ADEC

avg	0.065471
max	0.221053
min	0.022004
median	0.064939

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NO_x emissions from blasting operations in open-cut coal mining

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ABSTRACT

The Australian coal mining industry, as with other industries is coming under greater constraints with respect to their environmental impacts. Emissions of acid gases such as NO_x and SO_x to the atmosphere have been regulated for many years because of their adverse health effects. Although NO_x from blasting in open-cut coal mining may represent only a very small proportion of mining operations' total NO_x emissions, the rapid release and high concentration associated with such activities may pose a health risk. This paper presents the results of a new approach to measure these gas emissions by scanning the resulting plume from an open-cut mine blast with a miniaturised ultraviolet spectrometer. The work presented here was undertaken in the Hunter Valley, New South Wales, Australia during 2006. Overall this technique was found to be simpler, safer and more successful than other approaches that in the past have proved to be ineffective in monitoring these short lived plumes. The average emission flux of NO_x from the blasts studied was about 0.9 kt t^{-1} of explosive. Numerical modelling indicated that NO_x concentrations resulting from the blast would be indistinguishable from background levels at distances greater than about 5 km from the source.

1. Introduction

Open-cut coal mining is widespread in the upper Hunter Valley in New South Wales (NSW) with several large mines operating within close proximity to the towns of Muswellbrook and Singleton. Consequently, there is community concern about the potential environmental impacts of mining on nearby populations.

Blasting, in particular, has the potential to affect areas outside the mine boundary and accordingly, vibration and dust emission limits are set in each mine's environmental licence. However, gaseous emissions of environmental concern, such as nitrogen dioxide (NO_2) may also be released during blasting operations. Currently, there are very little quantitative data relating to the magnitude of these emissions and it is not yet possible to determine if they contribute significantly to ambient levels in the main population centres.

The explosive ammonium nitrate/fuel oil (ANFO) is used almost universally throughout the open-cut coal mining industry. Under ideal conditions, the only gaseous products from the explosion are carbon dioxide (CO_2), water (H_2O) and nitrogen (N_2).

$$3NH_4NO_3 + CH_2 \rightarrow 3N_2 + CO_2 + 7H_2O \quad (1)$$

However, even quite small changes in the stoichiometry (either in the bulk material or caused by localised conditions such as moisture in the blast hole, mineral matter or other factors) can lead to the formation of substantial amounts of the toxic gases carbon monoxide (CO) and nitric oxide (NO) as shown.

$$2NH_4NO_3 + CH_2 \rightarrow 2N_2 + CO + 5H_2O \quad (2)$$

$$5NH_4NO_3 + CH_2 \rightarrow 4N_2 + 2NO + CO_2 + 7H_2O \quad (3)$$

In addition, some of the NO formed may oxidise in the presence of oxygen (O_2) to produce NO_2.

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$$2NO + O_2 \rightarrow 2NO_2 \quad (4)$$

Often in practice, large quantities of NO_2 are released from blasts which are observed as intense orange plumes.

Although these gases are not considered in their environmental licences, each mine is required to estimate annual emissions of CO, NO_x and SO_2 for the National Pollutant Inventory (NPI), compiled each year by the Australian government. These estimates are made by multiplying the amount of explosive consumed by an emission factor which is currently 8 kg t^{-1} for NO_x, 34 kg t^{-1} for CO and 1 kg t^{-1} for SO_2 (National Pollutant Inventory, 1999). These emission factors, however, are based on limited overseas data and are subject to high uncertainty.

Most of the studies which have examined NO_x formation from blasting have used blast chambers. The results from these studies do not necessarily correlate with what is observed during actual blasts. Few studies have attempted to measure NO_x emissions under actual field conditions, presumably because of the practical difficulties involved. Plumes from blasting lack confinement, can be very large in size and are affected by prevailing weather conditions. There is also a large quantity of dust associated with the blast and these factors combine to make physical sampling of the plume very difficult. There are also the obvious safety implications which restrict access to blast sites. Consequently, quantitative measurements of plume characteristics are generally unavailable. Nevertheless, it is important for mine operators, particularly when their operations are close to residential areas, to have some method for assessing NO_x formation and more importantly, predicting the severity of the NO_x plume. At present predictions of NO_x formation are subjective and are based on the blast engineer's knowledge of the area to be blasted (e.g. rock type, area of the mine, presence of water in the holes, etc.) and the ratings obtained from blasts performed under similar conditions. Quantitative flux estimations of NO_x released from a blast require measurement of concentration through the plume in both the horizontal and vertical axes.

Some of the options available to make these measurements are given in the following sections.

1.1. Physical sampling

Sampling of blasting fumes involves taking a sample of gas from the plume for subsequent analysis, which could be either on site or in an off site laboratory. Although physical sampling could in principle provide sufficient information to characterise a plume, there are a number of serious logistical problems with this approach:

- The size of the plume means that a large number of sample points would be required to sample across the width and height of the plume.
- The force of the explosion and the resulting debris would restrict the proximity of any sampling packages to the initial gas release.
- The potential toxicity of the plume; personnel cannot move through it to take samples, hence sampling stations must be fixed prior to the blast. This means that the path of the plume must be anticipated before the blast.

1.2. Continuous analysis

Another option is to use portable analysers to measure NO_x concentrations in real time. There are, however, disadvantages with this approach since a sample of the plume must be presented to the instrument for analysis. Usually a pump draws air through a small diameter tube into the instrument, but to achieve the necessary spatial characterisation of the plume, sample tubes would need to be positioned at various points throughout the plume. Thus many of the problems identified for the physical sampling would also apply to the use of continuous analysers.

1.3. Optical methods

There are several optical methods of analysis currently available that may be applicable to field measurements of NO_x. These include open-path Fourier Transform Infra-Red Spectroscopy (FT-IR), Correlation Spectroscopy (COSPEC) and Differential Optical Absorption Spectroscopy (DOAS). FT-IR has often been used in air pollution studies (e.g. Levine and Russwurm, 1994). It has also been used in mine situations to measure fugitive methane emissions. Kirchgessner et al. (1993) used open-path FT-IR (op-FT-IR) to estimate methane emissions from open-cut coal mines in the United States. The technique relies on passing a collimated infrared beam through ambient air over a path length of up to several hundred metres. In the Kirchgessner et al. (1993) study, the concentration of methane across the plume was measured then wind speed data and a Gaussian plume dispersion model were used to estimate the methane emission rate from the mine. These authors subsequently developed a modification of their method which improved its accuracy (Piccot et al., 1994, 1996). The improved method was essentially the same as described above except that methane concentrations were measured at several elevations to better characterise the plume.

In principle, open-path FT-IR could be used to measure NO_x in blast plumes since it is sensitive to NO, NO_2, and CO along with other gases. Infrared radiation is also strongly absorbed in many parts of the spectrum by both CO_2 and water which are very likely to be present in high concentrations in blast plumes and this may tend to obscure the NO_x signal. High resolution instruments may resolve at least some of the NO_x absorption lines, however, a more serious drawback with op-FT-IR is that the infrared beam would be substantially attenuated by the dust thrown up by the blast. In the period immediately after the blast when the dust level is very high it is likely that the IR beam would be completely blocked thus making measurements impossible.

Another well established optical method is Correlation Spectroscopy (COSPEC). The system was first described by Moffat and Milan (1971) and was designed to measure point source emissions of SO_2 and NO_2 from industrial plants but found a niche application in the measurement of SO_2 fluxes from volcanoes (Galle et al., 2002). The COSPEC system utilises a "mask correlation" spectrometer and was designed to measure vertical or slant columns using

sky-scattered sunlight. By traversing beneath plumes with the mobile instrument, the concentration of the column is calculated and, once multiplied by the plume velocity, produces a source emission rate. These instruments are limited to detecting only those species where masks are available. They also suffer from interferences from other atmospheric gases and light scattering from clouds or aerosols that can produce errors in column densities (Chalmers Radio and Space Science, website).

The DOAS technique is a relatively new technique that is gaining widespread acceptance as an air pollution monitoring method. Like the open-path FT-IR method, the DOAS can simultaneously measure concentrations of a number of species over path lengths which typically range from hundreds of metres to kilometres.

A DOAS, configured as an 'active system', Fig. 1, has three main parts – a light emitter, a light receiver and a spectrometer. The emitter sends a beam of light to the receiver (in some cases the emitter and receiver are contained in the same unit and the light beam is reflected off a remotely located passive reflector). The light beam contains a range of wavelengths, from ultraviolet to visible, although instruments are now available with an infrared source, which extends the range of compounds that can be detected. Different pollutant molecules absorb light at different wavelengths along the path between the emitter and receiver. The receiver is connected to the spectrometer which measures the intensity of the different wavelengths over the entire light path and through the data system converts this signal into concentrations for each of the species being monitored.

DOAS instruments are routinely used to measure SO_2, NO_2 and O_3.

More recently, advances in miniaturising UV–vis spectrometers has lead to the development of much more compact DOAS units, configured as a passive system (Fig. 1), which have come to be known as "mini-DOAS". The mini-DOAS system has so far been used mainly in the study of SO_2 fluxes in volcanic emissions (McGonigle et al., 2003).

2. Methodology

2.1. Field measurements

A portable DOAS (mini-DOAS) manufactured by Resonance Ltd was used in this study. The instrument covers a spectral range of 280–420 nm and can measure sub-part per million levels of NO_2 and SO_2. The unit, which comprises a telescope, scanning mirrors, calibration cells and a miniature CCD array spectrometer (Ocean Optics USB2000 spectrometer), is housed in a small package which is mounted on a tripod. Calibration of the instrument was carried out using the internal calibration cell. The concentration of the cell was equivalent 50 ppm m. No SO_x measurements were undertaken.

Data collection and processing were performed by Ocean Optics OOIBase32 software loaded in a laptop computer. This results in a more compact system that is easier to deploy at mine sites and provides greater flexibility in positioning the instrument in relation to the blast plume.

Prior to each monitored blast, a dark spectrum was collected by blocking light from entering the spectrometer and a scan was performed. To produce a reference spectrum, a further scan was performed in a clear sky background which contained background absorption from NO_2. The reference spectrum was required in order to determine the increase in concentration of NO_2 above ambient levels in the blast plumes.

The plume resulting from each blast was tracked with the spectrometer until the NO_2 concentration was indistinguishable from the surrounding sky. During each field measurement, the mini-DOAS and a video camera were positioned a safe operating distance from the blast at all times.

NO_2 concentrations in the plume were calculated by subtracting the dark spectrum from the measured spectrum and the reference spectrum using the supplied software.

The results obtained from the mini-DOAS are a path-averaged NO_2 concentration profile measured in units of parts per million metre (ppm m). The mini-DOAS results must be divided by the path length through the plume to yield a concentration. To estimate the amount of NO_2 released from each blast it was necessary to multiply the concentration by the volume of the plume. Hence it was necessary to estimate the dimensions of each plume.

All of the blasts monitored were video-taped using at least one, and sometimes two, video recorders. The distances between the cameras and the blast were measured by locating their positions with a handheld GPS receiver.

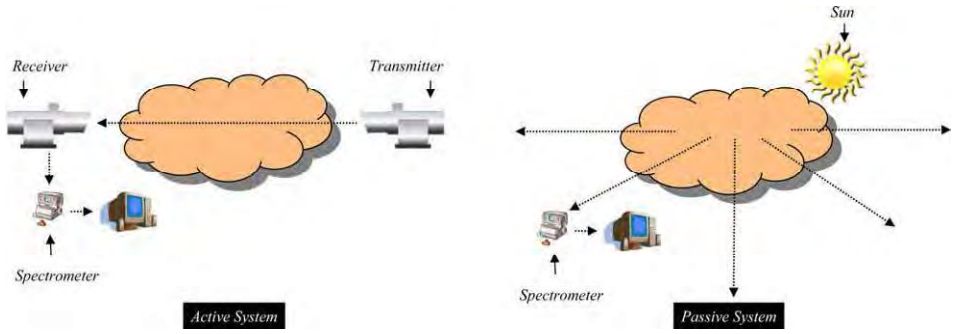

Fig. 1. Schematic diagram of DOAS systems operating in both active and passive modes.

Wind speed and directional data used to plot the directional path of the plume were obtained from a series of meteorological stations located around the mining lease. Simple trigonometry was employed to determine the distance from the video camera to the plume at the corresponding time intervals.

A rudimentary method of photogrammetry was then used to estimate the size of the plume based on still images extracted from the videos. Ratios of the plume to picture size in both the vertical and horizontal planes were made.

Once the plume to camera distance and the constraining angle for the plume is known, a crude three-dimensional estimate of the plume dimension was calculated using basic trigonometric functions. An example of the dimensions determined for a plume using this method is shown in Fig. 2.

Ground level measurements were carried out using a Greenline 8000 portable gas analyser. This instrument is capable of continuous, simultaneous analysis of O_2, CO_2, CO, SO_2, NO and NO_2. It is battery powered and can operate unattended for up to about 2 h. The instrument was calibrated against a standard gas mixture before each use. Data were logged on a laptop computer connected to the instrument.

For each experiment, the instrument was set up downwind of the blast in a location where the plume was expected to pass, but far enough away to avoid flying debris. The inlet probe was fixed at about 2 m above ground level.

It must be noted that selecting an appropriate location for the instrument was often difficult. In many cases, the wind conditions were quite variable, especially within the pit so it was not always possible to correctly anticipate the path of the blast plume. As well, the layout of the mine pit and safety considerations imposed constraints on where the instrument could be placed. Because of these problems, the plumes from many of the blasts did not pass over the analyser and data was not recorded.

2.2. Modelling

A simple modelling exercise was undertaken for this study to determine if the release of NO_2 from a blast could be of detriment to persons exposed to the plume within 5 km of the release. The results of this study are indicative and based on the assumption that the model used is appropriate. Modelling generally relies on local observational data to confirm the performance of the model. The difficulty in measuring emissions from mining blasts has meant that in this case the model is used as an indicator relying on the verifications used in the development of the chosen model. For this reason we have modelled concentrations directly downwind of theoretical blasts with AFTOX (Kunkel, 1991), a USEPA approved dispersion model (http://www.epa.gov/scram001/dispersion_alt.htm#aftox). The original DOS based QuickBasic code was transformed into Excel macros to enable many scenarios to be run.

AFTOX is a Gaussian Puff model developed for the United States Air Force to assess real time toxic chemical releases. The model uses information from US Air Weather Service (AWS) stations to calculate dispersion based on measured atmospheric conditions. As for all Gaussian models, the spread of pollutants is governed by dispersion coefficients in the horizontal (σ_y) and vertical (σ_z) directions. These coefficients depend on the atmospheric stability derived from the AWS data. In this study, the scenarios were modelled by predefining the wind speed and atmospheric stability classes. The wind speeds modelled ranged from very low (0.5 m s^{-1}) to moderate (10 m s^{-1}). Stability was modelled in six steps representing the standard Pasquill-Gifford stability classes, i.e. A–F, where A, B and C represent unstable conditions (where A is the most unstable), D is neutral and E and F are stable conditions. These stability classes are used to categorise the rate at which a plume will disperse. Unstable conditions might be found on a sunny day with light winds leading to rapid plume dispersion while the stable conditions may occur in clear skies with light winds and perhaps a temperature inversion present. Plume spread is slow in these circumstances.

AFTOX is operated by assuming an emission release from a single location. The emissions can be either continuous or instantaneous. In this study AFTOX was used to describe an area source by representing it as a large number of individual points. The area of the emission (i.e. the area over which the explosives were distributed) was

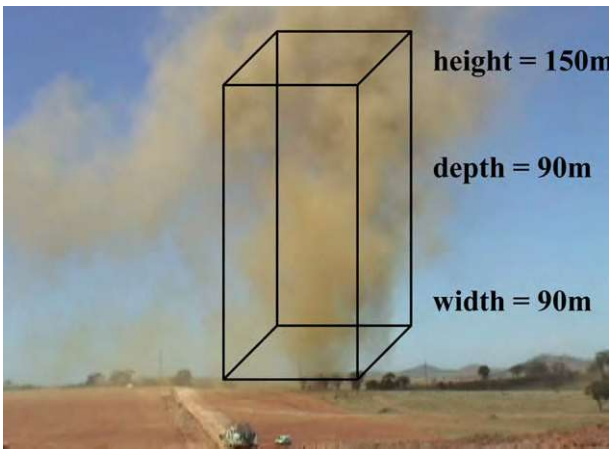

Fig. 2. Blast plume with estimated dimensions.

assumed to be 100 m × 200 m based upon sizes commonly observed during the field measurements. The area was subdivided into 10 m × 10 m units. Each square was represented by a point source with its source at the centre. In total, the area was modelled as 231 separate point sources (see Fig. 3). The total flux of emissions for the source was set at 100 kg. To estimate the maximum concentration and pollutant exposure values, the values should be multiplied by an appropriate scaling factor.

One hundred and twenty scenarios were modelled in which the 100 kg of emissions were spread randomly throughout the source area. A multi-stage process was employed for this task. In the first step, the total maximum number of points emitting was determined. This was defined by a random number between 20% and 80% of the maximum number of sources (in this case 231). The range chosen was an estimate from the portion of blasts that appeared to fume in conditions witnessed during this study. The total emission was then divided by this number. Each portion of the total emission was then placed randomly within the emission area. This process allowed certain points to receive multiple portions of the total emissions enabling the formation of hot spots. An example of one emission grid (Scenario 1 of 120) is displayed in Fig. 4.

Concentrations were determined for each of the 120 emission scenarios at distances of 200 m, 300 m, 400 m, 500 m, 750 m, 1 km, 1.25 km, 1.5 km, 2 km, 2.5 km, 3 km, 4 km and 5 km from the origin of the source. A concentration was determined for a number of discrete times that encompassed the complete plume travelling past the receptor. Further the concentrations were determined at 21 locations 10 m apart in a plane parallel and directly downwind of the source area (see Fig. 3). An average concentration from each of the receptors was determined; in this case with N equal to 21.

$$C^{*} = \frac{1}{N}\sum_{i=1}^{N} C_i \tag{5}$$

The average for each scenario was then used to create an ensemble average and standard deviation for the entire run (i.e. $N = 120$).

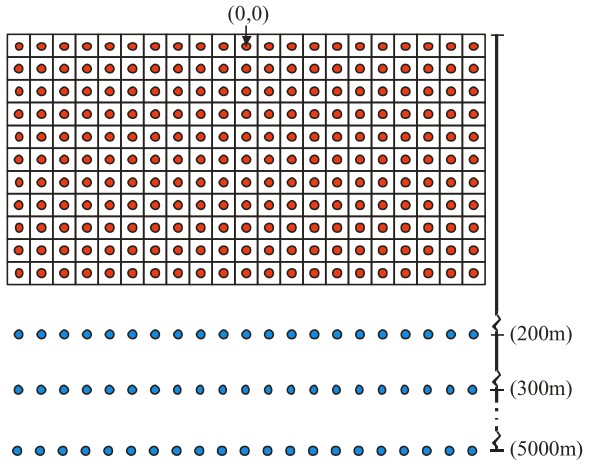

Fig. 3. Emission grid and receptor array setup.

$$\overline{C} = \frac{1}{N}\sum_{j=1}^{N} C_j^{*} \tag{6}$$

$$\sigma_{\overline{C}} = \frac{1}{N}\sum_{j=1}^{N}\left(C_j^{*} - \overline{C}\right)^2 \tag{7}$$

$$C_{\max} = \max_{k=1}^{N}[\overline{C}_k] \tag{8}$$

A dosage expressed in ppm s was determined from the times when the ensemble average plume travelled past the receptors located at each distance downwind of the source. Again N represents each discrete time step (dt) where $C' \neq 0$.

$$C_{\text{dose}} = \sum_{k=1}^{N}(\overline{C}_k)\mathrm{d}t \tag{9}$$

The relative variation for the dosage is provided by similarly treating the ensemble standard deviation.

$$\sigma_{\text{dose}} = \sum_{k=1}^{N}(\sigma_{\overline{C}k})\mathrm{d}t \tag{10}$$

3. Results and discussion

3.1. Field measurements

Plume measurements were made using the mini-DOAS spectrometer at two open-cut mine sites located in the Hunter Valley. The combination of the spectral analysis and the plume estimation technique allowed for NO_2 concentration and mass flux estimates to be made remotely, totally eliminating the requirement of physical sampling.

An example of the spectral output produced by the mini-DOAS is shown in Fig. 5. The spectral output consists of the NO_2 concentration (ppm m) as a function of time. The figure also contains a series of photographs depicting the formation of a blast plume at time intervals of 70, 110, 163, 250 and 350 s post-blast initiation. It is worth noting the change in intensity of the colour of plume and size as a function of time.

Reliable concentration measurements with the mini-DOAS may only be made when the spectrometer is aimed into a sky background above the horizon from the point of observation. In this example, a peak concentration of 580 ppm m was achieved in 163 s post-blast initiation (third image from the left). At this time the plume has risen above the horizon from the point of observation. The plume to mini-DOAS distance at this stage is approximately 500 m, with an estimated plume depth of 105 m. This results in a NO_2 concentration of 5.6 ppm at that particular stage of the plumes' dispersion.

After 350 s, the plume is barely visible and is now estimated to be approximately 650 m from the mini-DOAS unit. The plume depth has increased to 125 m with

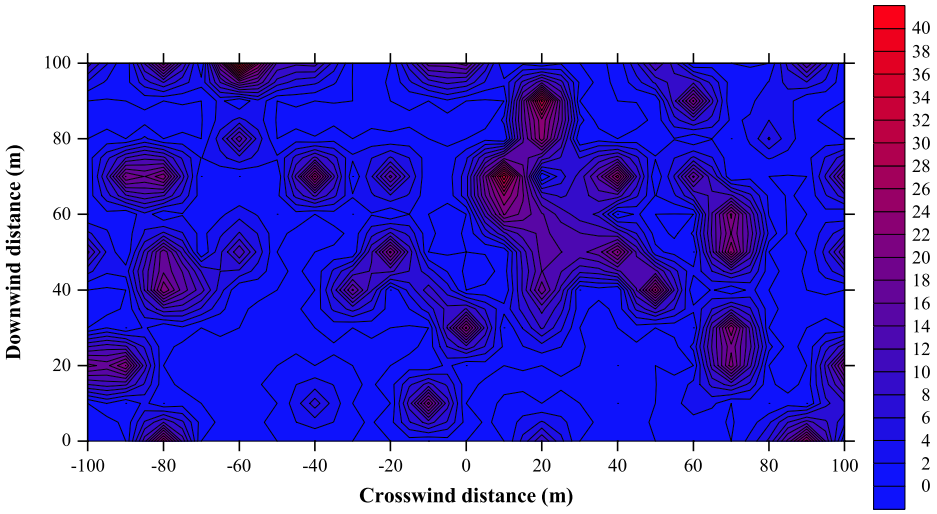

Fig. 4. Example of emission grid for 1 of the 120 scenarios modelled (the scale on the right hand side refers to NO_2 concentration in ppm).

a corresponding increase in plume volume by a factor of two. This expansion of the plume corresponds to a decrease in NO_2 concentration to 2.8 ppm.

At 360 s the plume was no longer visible to the eye and was lost for a short period of time to the mini-DOAS. This, however, was rectified with scanning of the sky with the spectrometer until the invisible plume was tracked for a further period.

Results for all plumes monitored during field work at both mine sites are given in Table 1. The table gives the peak NO_2 concentration as measured by the mini-DOAS above the horizon. Also given in the table is the plume volume at peak concentration and the calculated mass of NO_2 released from the blast. The mass of ANFO typically used in a blast was on average 210 tonnes, ranging from 60 to 565 tonnes. The explosive was distributed over an area of typically 200 m × 100 m containing approximately 200 bole holes with 200 mm diameter and to a depth of 25 m.

From the table the maximum NO_2 concentrations were found to range from 0 to about 7 ppm. This range of concentrations translated to 0–63.3 kg of NO_2 in the plume. However, no correlation can be made between blast charge and NO_2 levels.

During the measurements with the mini-DOAS ground level measurements were also carried out using a portable combustion gas analyser (Greenline 8000) to augment the airborne measurements made by the mini-DOAS. For NO_2 the ground level measures were higher than those observed using the mini-DOAS at higher altitudes. When the results of both measurement methods were applied to

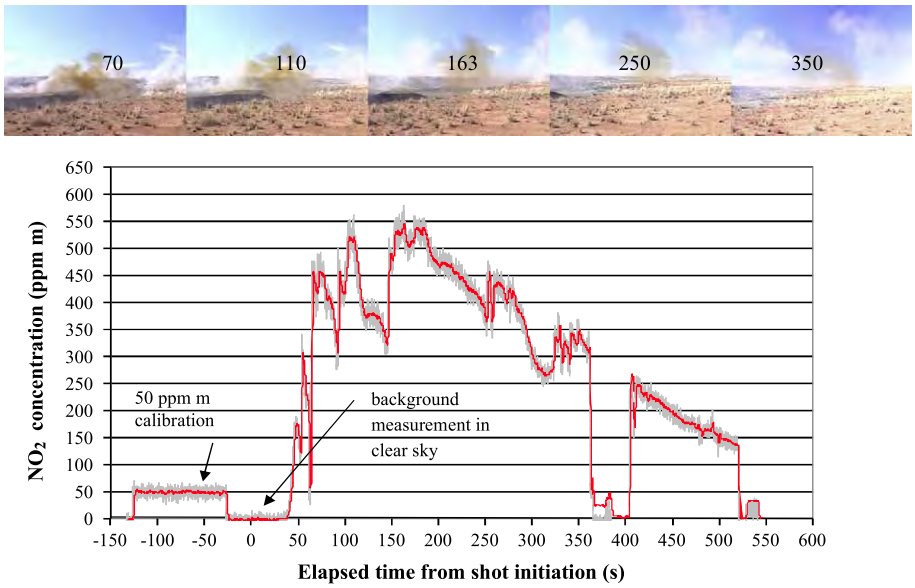

Fig. 5. Typical NO_2 spectrum demonstrating plume colour characteristics relative to concentration level.

Table 1
Through plume measurement results

Date	Total ANFO charge (t)	Peak NO_2 Conc (ppm)	Plume volume ($m^3 \times 10^{-6}$)	Mass of NO_2 (kg)	Emission flux (kg t^{-1} ANFO)		
					NO	NO_2	NO_x
12/12/2005	281	3.7	1.4	9.9	0.5	0.03	0.6
13/12/2005	150	0.4	5.3	3.7	0.4	0.03	0.4
14/12/2005	119	0.0	0.0	0.0	0.0	0.00	0.0
21/12/2005	229	1.0	4.4	7.9	0.6	0.04	0.6
22/12/2005	211	0.0	0.0	0.0	0.0	0.00	0.0
23/12/2005	222	0.0	0.0	0.0	0.0	0.00	0.0
5/01/2006	177	1.0	0.2	0.4	0.0	0.00	0.0
6/01/2006	275	1.1	15.3	30.6	1.8	0.12	1.9
12/01/2006	225	1.6	6.2	18.3	1.3	0.08	1.4
18/01/2006	169	1.3	1.7	0.2	0.4	0.02	0.4
23/01/2006	139	2.1	4.2	16.7	1.9	0.12	2.0
25/01/2006	155	0.4	4.4	2.9	0.3	0.02	0.4
30/01/2006	132	0.7	5.3	7.1	0.8	0.05	0.9
22/02/2006	224	0.0	0.00	0.0	0.0	0.00	0.0
1/03/2006	194	1.6	20.6	63.3	5.0	0.32	5.3
12/05/2006	362	6.5	1.9	23.3	1.0	0.06	1.1
15/05/2006	131	0.3	3.2	1.7	0.2	0.01	0.2
19/05/2006	168	0.0	0.00	0.0	0.0	0.00	0.0
30/05/2006	100	0.8	0.00	1.0	0.0	0.00	0.0
1/06/2006	365	0.7	3.5	4.9	0.2	0.01	0.2
6/06/2006	145	0.8	11.5	17.5	1.9	0.12	2.0
15/06/2006	60	0.0	0.00	0.0	0.0	0.00	0.0
26/06/2006	254	4.3	0.3	2.1	0.1	0.01	0.2
27/06/2006	212	5.6	0.9	10.0	0.7	0.04	0.7
28/06/2006	241	0.0	0.00	0.0	0.0	0.00	0.0
6/07/2006	565	2.8	2.7	14.0	0.4	0.03	0.4
13/07/2006	184	7.0	1.0	12.6	1.1	0.07	1.2

dispersion modelling techniques strong agreement was observed.

Point measurements which were made on Greenline 8000 indicated that a loose relationship existed between NO and NO_2 concentration. Although a strong correlation was not found, there is a general trend of increasing NO_2 with increasing NO. It was generally found that the relative proportion of NO to NO_2 from our data set was 27 to 1. This

Table 2
Maximum calculated NO_2 concentrations downwind of source

	200 m	300 m	400 m	500 m	750 m	1000 m	1250 m	1500 m	2000 m	2500 m	3000 m	4000 m	5000 m
WSPD = 0.5 m s^{-1}													
Stab A	83.0	30.0	14.4	7.9	2.5	0.9	0.4	0.2	0.1	0.0	0.0	0.0	0.0
Stab B	145.8	69.3	40.8	25.4	10.1	4.8	2.6	1.6	0.7	0.4	0.2	0.1	0.1
Stab C	219.4	122.0	80.8	55.9	26.8	14.3	8.6	5.6	2.8	1.6	1.0	0.5	0.3
Stab D	321.1	201.5	146.0	113.1	64.6	40.2	26.1	18.6	10.5	6.7	4.5	2.4	1.4
Stab E	390.2	267.4	204.3	165.5	109.6	75.9	54.6	41.3	26.4	17.9	12.7	7.1	4.5
Stab F	464.1	339.8	269.0	222.6	154.5	114.9	88.6	69.7	50.4	37.0	27.8	16.7	11.0
WSPD = 3 m s^{-1}													
Stab A	78.5	29.1	14.2	7.7	2.4	0.9	0.4	0.2	0.1	0.0	0.0	0.0	0.0
Stab B	137.6	67.7	39.7	25.1	10.0	4.8	2.6	1.6	0.7	0.4	0.2	0.1	0.1
Stab C	211.6	118.7	77.6	55.2	26.0	14.0	8.6	5.6	2.8	1.6	1.0	0.5	0.3
Stab D	312.5	197.9	143.2	110.0	62.5	39.3	26.1	18.2	10.5	6.7	4.5	2.4	1.4
Stab E	383.0	267.0	202.1	162.6	106.3	73.7	54.1	40.3	26.1	17.7	12.5	7.2	4.5
Stab F	461.5	344.6	268.4	220.8	151.1	112.3	86.1	67.6	48.9	36.4	27.5	16.6	11.0
WSPD = 7.5 m s^{-1}													
Stab A	62.5	25.5	13.0	7.3	2.3	0.9	0.4	0.2	0.1	0.0	0.0	0.0	0.0
Stab B	111.9	56.1	34.2	22.6	9.4	4.6	2.6	1.6	0.7	0.4	0.2	0.1	0.1
Stab C	173.3	100.4	66.5	47.7	23.8	13.2	8.2	5.4	2.7	1.6	1.0	0.5	0.3
Stab D	261.2	167.9	122.1	92.3	54.8	35.3	23.7	17.2	10.1	6.5	4.4	2.3	1.4
Stab E	325.9	232.2	175.8	139.6	89.5	63.8	46.7	36.0	23.9	16.8	12.1	7.0	4.4
Stab F	394.6	302.7	237.0	194.3	132.2	96.1	73.3	59.0	43.6	33.3	25.7	15.8	10.5
WSPD = 10 m s^{-1}													
Stab A	53.0	22.6	11.9	6.9	2.3	0.9	0.4	0.2	0.1	0.0	0.0	0.0	0.0
Stab B	92.3	49.7	31.0	20.9	9.0	4.5	2.5	1.5	0.7	0.4	0.2	0.1	0.1
Stab C	140.1	84.2	57.7	42.1	21.7	12.6	7.9	5.3	2.7	1.6	1.0	0.5	0.3
Stab D	205.5	138.3	102.4	79.9	48.6	31.8	22.1	16.4	9.7	6.4	4.3	2.3	1.4
Stab E	254.0	184.0	143.0	116.4	78.0	56.2	42.6	33.1	22.7	16.0	11.6	6.9	4.4
Stab F	306.8	235.8	189.6	157.9	109.9	82.8	64.5	52.2	40.0	30.9	24.0	15.2	10.2

relationship enabled the estimation of the NO fluxes in the blast plume with a reasonable level of confidence.

The results obtained in this study are the only published quantitative data available on blast plume gas composition that the authors are aware of and it is useful to compare them to the emission factors currently used for NPI estimates.

Based on the NO_2 measurements and estimates of NO, the flux for NO_x was calculated to be in the range of 0.04–5.3 kg t^{-1} ANFO. The average flux level for all the blast plumes measured was 0.9 kg t^{-1}. This figure is considerably lower than the current NPI emission factor which is 8 kg t^{-1}.

3.2. Modelling

Results of the modelling runs are summarised in Table 2 and show the peak NO_2 concentrations (ppm) at various points downwind of the blast for the six atmospheric stability classes considered.

Examples of the modelled data are plotted in Fig. 6 and Fig. 7. In Fig. 6 a plot is displayed for the concentration estimate of one scenario at a distance of 200 m from the source origin and for a wind speed of 2 m s^{-1} and a stability class C. In this plot 21 lines are shown representing the dose received directly downwind of the source at the locations displayed in Fig. 3. In this figure it is apparent that there is a considerable difference in the concentration predicted at each of the 21 receptors. It should be noted that the distance of 200 m is defined from the origin of the source area (0, 0) as displayed in Fig. 3. At this distance emission sources at 100 m will cause significantly higher concentrations than those occurring at positions toward the origin. In comparison the concentrations predicted at the receptor array 1 km from the source show more normally defined distributions with maxima occurring towards the middle receptors as a result of crosswind diffusion. Receptors toward the edge of the sample array receive less crosswind influence and are, therefore, smaller in concentration. Also apparent in these two figures is the considerable difference in the predicted peak concentrations with the values at 1 km up to 25 times lower than at 200 m. When viewing Table 2, the peak values at 5 km approach ambient levels for all but the most stable conditions which are quite commonly over predicted with Gaussian models. For future studies it is recommended that a long path technique on a mining lease boundary may provide both a measure of the model accuracy as well as a direct measure of the impact in areas directly surrounding the mining area.

The data presented in this study represent a dose directly downwind of the source and as such are a worst case scenario for exposure. The averages of the 21 receptors (i.e. the average concentration directly downwind of the source) for each of the 120 scenarios modelled were used to determine the selected data. The number of scenarios modelled was arbitrarily chosen to allow 10 scenarios to be run on each machine in a cluster of 12 computers. The maximum concentration in Table 2 is the maximum ensemble average obtained from the average of the 21 receptors for the 120 scenarios modelled. Maximum concentrations at individual locations directly downwind of hot spots are obviously higher than the values reported in this table.

When viewing Table 2 it is apparent that the peak concentrations drop dramatically as the receptor moves away from the source. It is also apparent that the peak concentrations vary little as a function of wind speed although the plume width will vary. In AFTOX a downwind concentration is determined in two steps. In the first step the size of the initial plume envelope is estimated. In its default mode AFTOX determines the size of the envelope (assumed to be a cylinder of equal height and width) from the magnitude of the emission rate. In this report the size is set at 10 m to match the grid structure used for the area

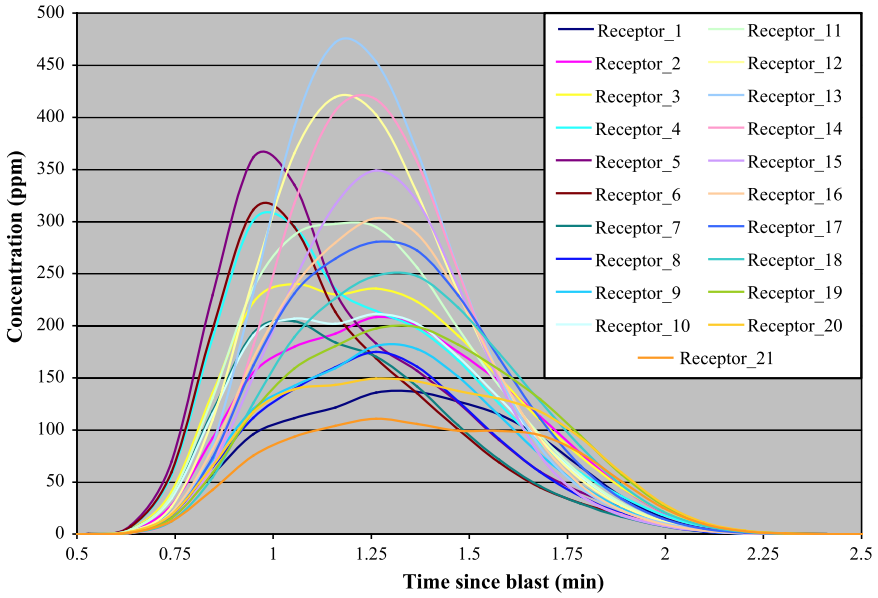

Fig. 6. Calculated NO_2 concentration profiles 200 m from source.

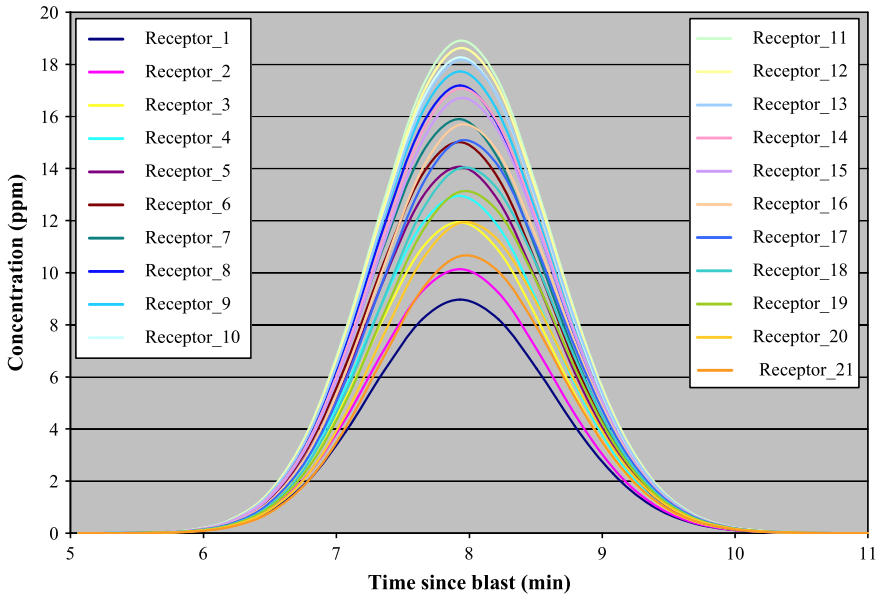

Fig. 7. Calculated NO_2 concentration profiles 1 km from source.

source. AFTOX in this regard ignores the effect of wind speed on the size of the initial envelope and as such the initial concentration of the plume is identical irrespective of wind speed by ignoring longitudinal (i.e. downwind) spread of the initial release. In the second step the concentration downwind of the initial release is determined by estimating the growth of a puff in three dimensions which in this case explicitly includes longitudinal plume spread which is assumed to be equal to the degree of crosswind spread. The degree of this spread is determined solely from the prescribed atmospheric stability class which ignores any wind speed dependence.

While the peak concentrations are similar, the dose received at a receptor is linearly dependent on wind speed. Emissions released into an atmosphere with higher wind speeds result in a receptor receiving doses for a smaller period of time. It should be noted that some of the differences in the peak concentrations displayed in Table 2 result from the number of discrete time steps used to calculate the concentrations. This was set at 25 intervals between the onset and finish of a plume as it passes by the receptor. This time is dependent on atmospheric stability and the distance from the source. In AFTOX, the puffs are assumed to disperse in the direction of plume travel proportionally with the degree of crosswind spread. As such, portions of the plume arrive before and after the main bulk of the emissions and the effect clearly demonstrated in Figs. 6 and 7. The moderate number of discrete times modelled to capture this effect while generally adequate may have led to a degree of variation particularly at larger distances from the source.

Again it should be noted that the modelled figures assume an area wide flux of 100 kg which is larger than observed in the blast recorded during this study. It should also be noted that while some of the concentrations are high close to the source the concentration at a particular location occurs for a brief period of time which is determined by the wind speed.

4. Conclusions

A portable open-path spectroscopic method was found to be effective for measuring NO_2 emissions from blasting. Overall this technique was found to be simpler, safer and more successful than other approaches that in the past have proved to be ineffective in monitoring these short lived plumes.

Quantitative measurements of NO_2 in plumes from blasting were made at two open-cut mines. The results showed that NO_2 was present in most of the plumes but in relatively low concentrations (typically ranging between 0 and 7 ppm). The highest concentration measured during all the field campaigns was about 17 ppm at ground level.

Based on field measurements, the emission factor currently used in compiling the Australian National Pollutant Inventory was found to be approximately eight times greater than that observed in our investigation. This would suggest that an over estimation of NO_x is made if the current factor is used.

Numerical modelling of the behaviour of plumes resulting from blasting was made to assess the possible downwind concentrations of NO_2. These results were compared to ambient NO_x measurements made in Muswellbrook.

- Modelling results were consistent with concentration measurements within the plumes at relatively short distances from the blast (i.e. up to about 1 km).
- Ambient monitoring did not detect NO_x events that could be attributed to individual blasts. Modelling suggested that these emissions would be very low at

distances greater than 5 km from the blast and may be indistinguishable from background levels; typically of the order of several parts per billion, in most cases.

Acknowledgements

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APPENDIX F. EMISSIONS WORKBOOK AND MODEL FILES

ALL FILES PROVIDED IN ORIGINAL ELECTRONIC FORMAT

APPENDIX G. PARTICLE SIZE DISTRIBUTIONS

1. PARTICLE SIZE DISTRIBUTIONS

The following sections describe the methodology used to estimate the particle size distributions for various emission sources.

1.1 Haul Roads

Section 13.2.4 of AP 42 lists the emission factors for emissions from unpaved roads. These emission factors were used to determine the distribution of emissions for particles with nominal diameters less than 30, 10 and 2.5 μm. Figure E.1 shows the distribution.

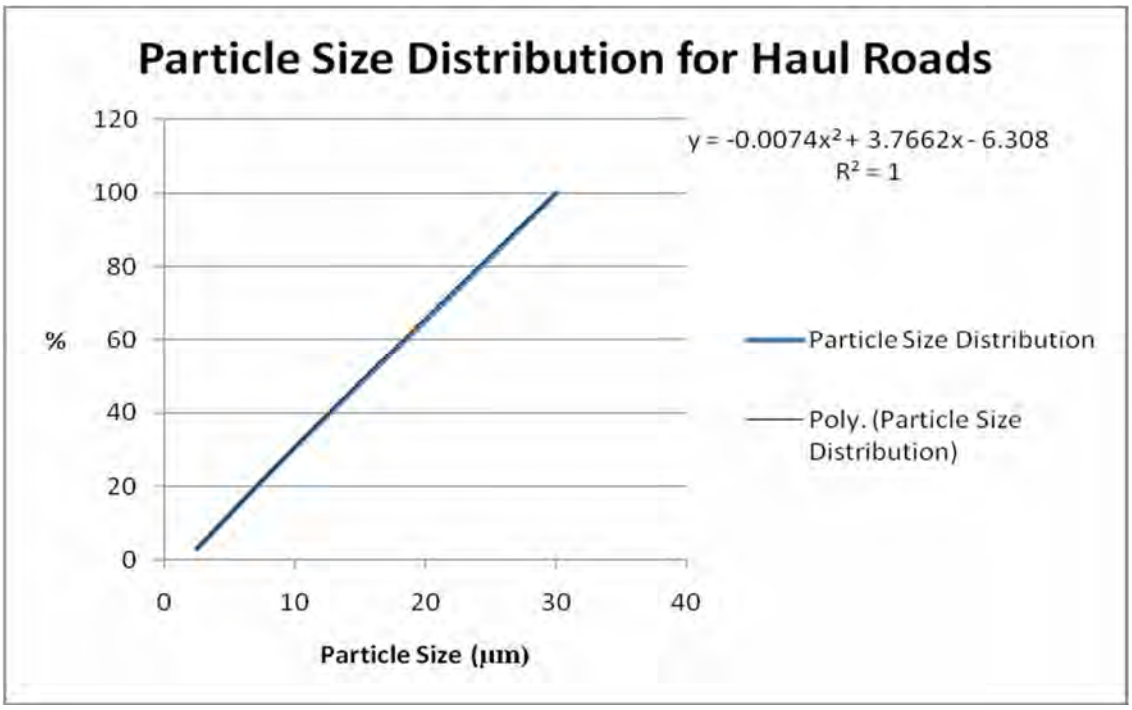

Figure E.1 Average size distribution for air borne dust generated by haul trucks for entire study period.

A 2nd degree polynomial equation was used to fit the data and determine particle size distributions for use with haul road emissions from the Rosemont mine. Table A.1 shows the calculated particle size distribution that will be used for haul road emissions.

Table E.1 Particle Size Distribution - Haul Road Emissions		
Diameter (microns)	**Mass Fraction**	**Density (gm/cm3)**
2.2	0.069	2.44
3.17	0.128	2.44
6.1	0.385	2.44
7.82	0.224	2.44
9.32	0.194	2.44

1.2 Material Transfer

Section 13.2.4 of AP 42 lists the emission factors for Aggregate Handling process. These emission factors were used to determine the distribution of emissions for particles with nominal diameters less than 30, 15, 10, 5 and 2.5 μm. Figure E.2 shows the distribution.

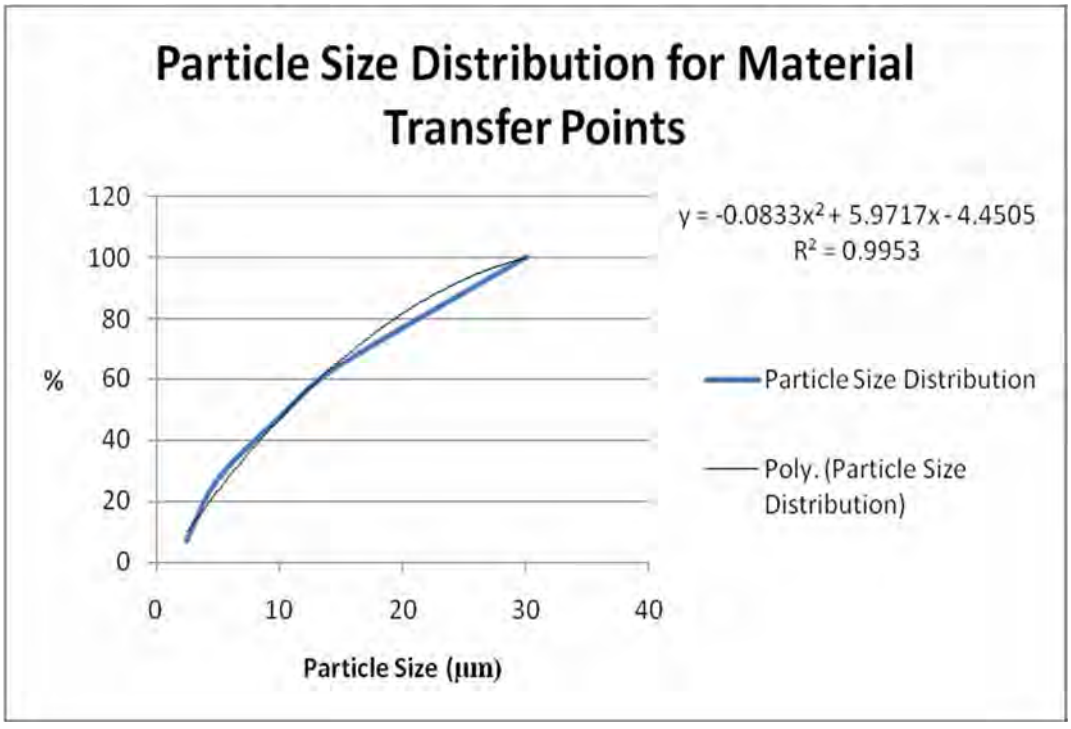

Figure E.2 Material Transfer Emissions (tpy) vs Particle Size (μm)

A 2nd degree polynomial was used to fit this data and determine the size distribution for other particle sizes. Table E.2 shows the calculated particle size distribution that will be used for material transfer emissions.

Table E.2 Particle Size Distribution - Material Transfer Points		
Diameter (microns)	**Mass Fraction**	**Density (gm/cm3)**
2.2	0.188	2.44
3.17	0.122	2.44
6.1	0.347	2.44
7.82	0.188	2.44
9.32	0.155	2.44

1.3 Blasting

Table 11.9-1 from section 11.9 of AP 42 lists the emission factors for Western Surface Coal Mining processes. The Blasting emission factors were used to determine the distribution of emissions for particles with nominal diameters less than 30, 10 and 2.5 μm. Figure E.3 shows the distribution.

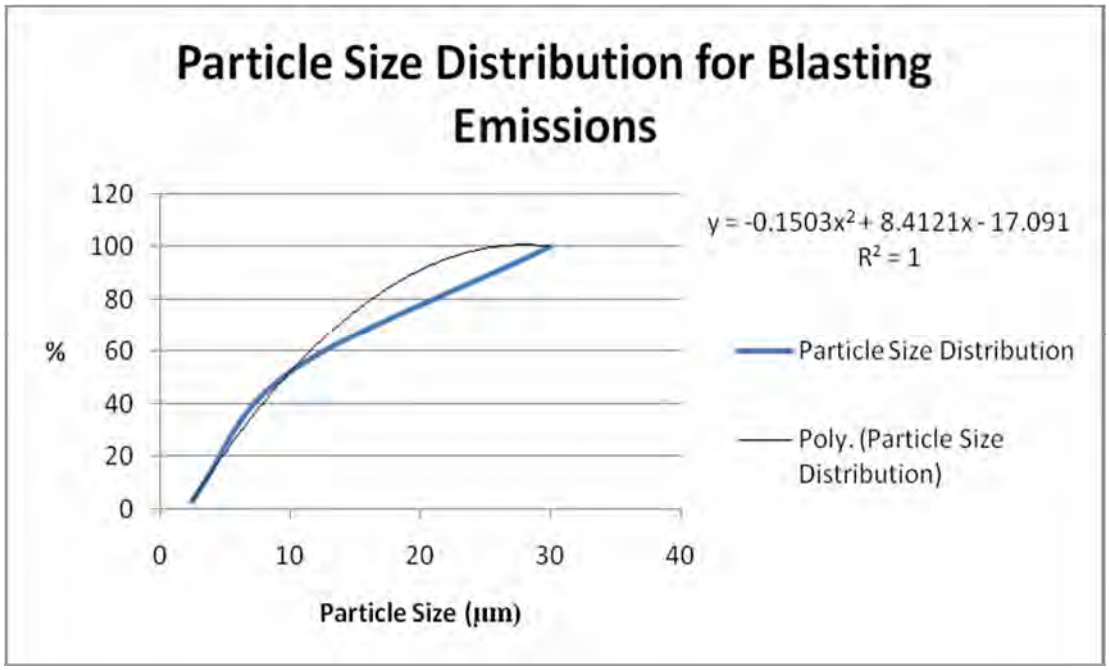

Figure E.3 Blasting Emissions (tpy) vs Particle Size (μm)

A 2nd degree polynomial was used to fit this data and determine the size distribution for other particle sizes. Table E.3 shows the calculated particle size distribution that will be used for material transfer emissions.

Table E.3 Particle Size Distribution - Blasting Emissions		
Diameter (microns)	**Mass Fraction**	**Density (gm/cm3)**
2.2	0.015	2.44
3.17	0.153	2.44
6.1	0.426	2.44
7.82	0.225	2.44
9.32	0.181	2.44

1.4 Point Sources

Page B.2-6, Appendix B.2 of AP 42 lists the collection efficiency of fabric filters used in baghouses for various particle sizes. These collection efficiencies were used along with particle size fractions for Aggregate handling processes (Section 13.2.4 of AP 42) to the calculate particle size distribution that will be used for point source emissions. Figure E.4 shows the distribution.

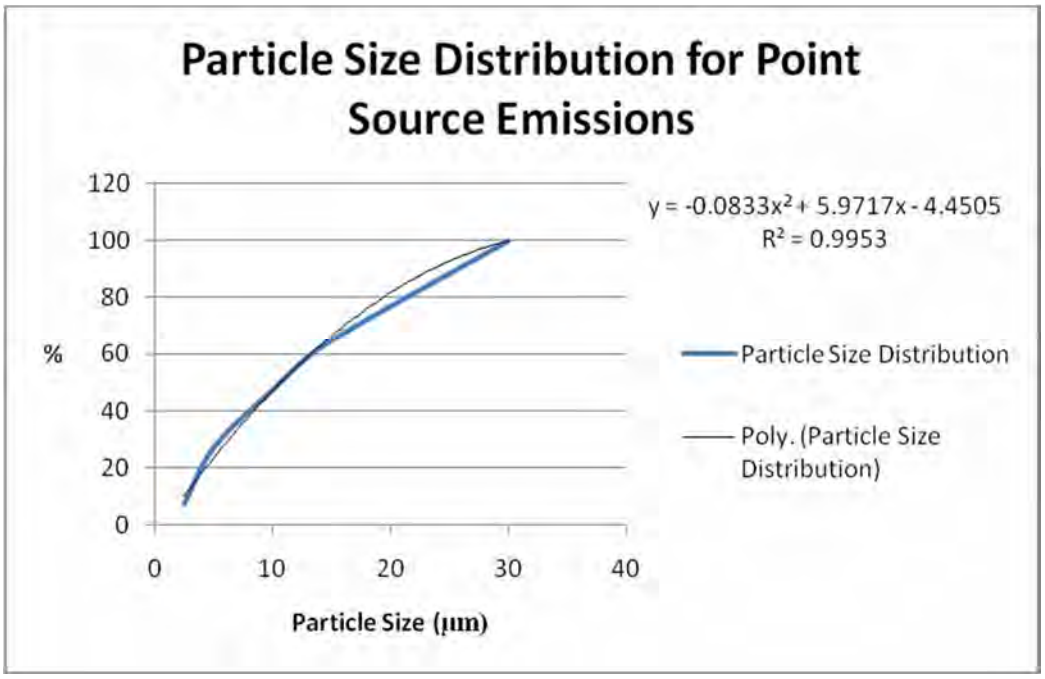

Figure E.4 Point Source Emissions (tpy) vs Particle Size

A 2nd degree polynomial was used to fit this data and determine the size distribution for other particle sizes. The obtained size distribution was then used along with the collection efficiency of the

baghouses for various sizes of particles. Table E.4 shows the collection efficiencies of fabric filters used in baghouses.

Table E.4 Collection Efficiency of Fabric Filters	
Diameter (microns)	**Collection Efficiency (%)**
0 - 2.5	99.0
2.5 – 6	99.5
6 - 10	99.5

Table E.5 shows the calculated particle size distribution that will be used for point source emissions.

Table E.5 Particle Size Distribution – Point Source Emissions		
Diameter (microns)	**Mass Fraction**	**Density (gm/cm3)**
2.2	0.317	2.44
3.32	0.103	2.44
6.1	0.292	2.44
7.8	0.158	2.44
9.32	0.130	2.44

APPENDIX H. HAUL TRUCK TRAVEL AND VMTS

List of Mobile Equipment - Year 2

Mobile Equipment Name	Year 2 Fleet Size	Equipment Detail	Value	Source	VMT/year (per vehicle)	VMT - Y2			Hours Used - Y2		
						Hourly	Daily	Annual	Hourly	Daily	Annual
Main Mine Equipment											
Haulage Trucks, 255 tons (Tier 4)	4	Horsepower	2,650	HB Mine Ops June 2019	---	---	---	---	4.0	96	28,380
		Empty Weight (tons)	167	HB Mine Ops June 2019							
		Loaded Weight (tons)	422	HB Mine Ops June 2019							
		Payload (tons)	255	HB Mine Ops June 2019							
Crawler Dozers, PL87 Class	0	Horsepower	366	Cat Website	---	0	0	0	0.0	0	0
Crawler Dozers, D10T Class	2	Horsepower	580	Cat Website	Information Not Needed	Information Not Needed			1.3	31	11,388
		Operating Weight (tons)	73	Cat Website							
Crawler Dozer, D8 Class	0	Horsepower	310	Cat Website	---	0	0	0	0.0	0	0
Rubber Tired Dozers, 834 Class	1	Horsepower	531	Cat Website	Information Not Needed	Information Not Needed			0.7	16	5,694
		Operating Weight (tons)	53	Cat Website							
Motor Graders, 16M Class	2	Horsepower	297	Cat Website	--	1.30	31	11,388	1.3	31	11,388
		Operating Weight (tons)	36	Cat Website							
Water Trucks, 30,000 gallons	2	Horsepower	1,348	Cat Website	--	7	175	63948.00	1.5	35	12,790
		Empty Weight (tons)	125	Cat Website							
		Loaded Weight (tons)	248	Add 30,000 gal water							

List of Mobile Equipment - Year 8

Mobile Equipment Name	Fleet Size	Equipment Detail	Value	Source	VMT/year (per vehicle)	VMT - Y8			Hours Used - Y8		
						Hourly	Daily	Annual	Hourly	Daily	Annual
Main Mine Equipment											
Haulage Trucks, 255 tons (Tier 4)	21	Horsepower	2,650	HB Mine Ops June 2019	---	---	---	---	21	504	134,291
		Empty Weight (tons)	167	HB Mine Ops June 2019							
		Loaded Weight (tons)	422	HB Mine Ops June 2019							
		Payload (tons)	255	HB Mine Ops June 2019							
Crawler Dozers, PL87 Class	0	Horsepower	366	Cat Website	---	0	0	0	0	0	0
Crawler Dozers, D10T Class	4	Horsepower	580	Cat Website	Information Not Needed	Information Not Needed			2.6	62	22,776
		Operating Weight (tons)	73	Cat Website							
Crawler Dozer, D8 Class	0	Horsepower	310	Cat Website	---	0	0	0	0	0	0
Rubber Tired Dozers, 834 Class	3	Horsepower	531	Cat Website	Information Not Needed	Information Not Needed			2.0	47	17,082
		Operating Weight (tons)	53	Cat Website							
Motor Graders, 16M Class	4	Horsepower	297	Cat Website	--	2.60	62	22,776	2.6	62	22,776
		Operating Weight (tons)	36	Cat Website							
Water Trucks, 30,000 gallons	6	Horsepower	1,348	Cat Website	--	21.90	525.60	191844.00	4.38	105	38,369
		Empty Weight (tons)	125	Cat Website							
		Loaded Weight (tons)	248	Add 30,000 gal water							

List of Mobile Equipment - Year 14

Mobile Equipment Name	Fleet Size	Equipment Detail	Value	Source	VMT/year (per vehicle)	VMT - Y14			Hours Used - Y14		
						Hourly	Daily	Annual	Hourly	Daily	Annual
Main Mine Equipment											
Haulage Trucks, 255 tons (Tier 4)	25	Horsepower	2,650	HB Mine Ops June 2019	---	---	---	---	25	600	159,870
		Empty Weight (tons)	167	HB Mine Ops June 2019							
		Loaded Weight (tons)	422	HB Mine Ops June 2019							
		Payload (tons)	255	HB Mine Ops June 2019							
Crawler Dozers, PL87 Class	0	Horsepower	366	Cat Website	---	0	0	0	0	0	0
Crawler Dozers, D10T Class	5	Horsepower	580	Cat Website	Information Not Needed	Information Not Needed			3.3	78	28,470
		Operating Weight (tons)	73	Cat Website							
Crawler Dozer, D8 Class	0	Horsepower	310	Cat Website	---	0	0	0	0	0	0
Rubber Tired Dozers, 834 Class	3	Horsepower	531	Cat Website	Information Not Needed	Information Not Needed			2.0	47	17,082
		Operating Weight (tons)	53	Cat Website							
Motor Graders, 16M Class	4	Horsepower	297	Cat Website	--	2.60	62	22,776	2.6	62	22,776
		Operating Weight (tons)	36	Cat Website							
Water Trucks, 30,000 gallons	6	Horsepower	1,348	Cat Website	--	21.90	525.60	191844.00	4.38	105	38,369
		Empty Weight (tons)	125	Cat Website							
		Loaded Weight (tons)	248	Add 30,000 gal water							

Copper World Project

Emissions Inventory For Haul Trucks

CAT	793F	793F	793F

Year		CW	HW	PE1	PE2	TOTAL		
Total Truck Fleet	Copper World	4	4	4	4			
Trucks - metered hours per shift	Copper World	9	9	9	9			
Truck Shifts Ore to Crusher	Copper World	473	1,998	1,635	235			
Truck Shifts Ore to HLP	Copper World	1,469	0	342	2,213			
Truck Shifts Waste	Copper World	696	641	661	191			
Mining and Transferring of Ore to be Concentrated (sulfide ore)	**Quantity of ore mined per year**	**982,544**	**3,553,783**	**5,701,265**	**712,408**	**10,950,000**	tons/year	Quantity of sulfide ore mined per year
	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1	2,692	9,736	15,620	1,952	**30,000**	tons/day	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1
	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly mill capacity	122	441	707	88	**1,358**	tons/hour	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly crusher capacity
	Type of transfer to the haul trucks	In the Pit	In the Pit	In the Pit	In the Pit		--	Type of transfer to the haul trucks
	Type of transfer from the haul trucks	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks
Mining and Transferring of Waste Rock to be Placed in Storage Areas	**Quantity of waste rock mined per year**	**1,444,835**	**1,140,516**	**2,305,579**	**579,166**	**5,470,096**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 2 shifts/day	3,958	3,125	6,317	1,587	**14,987**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 24 hours/day)	165	130	263	66	**624**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 23 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit	In the Pit	In the Pit	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mining and Transferring of ROM to be Placed in HLP	**Quantity of ROM ore mined per year**	**3,049,319**	**0**	**1,192,255**	**6,708,426**	**10,950,000**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of ROM mined per day. Entire fleet operating at 100% efficiency, 2 shifts/day	8,354	0	3,266	18,379	**30,000**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of ROM mined per hour (based on the maximum daily mining rate divided by 24 hours/day)	348	0	136	766	**1,250**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 23 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit	In the Pit	In the Pit	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mobile Equipment for Mining								
	Maximum quantity of Tier 2 trucks used during the year	0	0	0	0		trucks	Maximum quantity of Tier 2 trucks used during the year
	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)	3.569435751	3.569435751	3.569435751	3.569435751		trucks	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)
	Total fleet size (Tier 4F trucks)	4	4	4	4		--	Total fleet size (Tier 4F trucks)
	Empty weight of trucks MSD bodies are assumed	166.7	166.7	166.7	166.7		tons	Empty weight of trucks MSD bodies are assumed
	Capacity of trucks (Payload)	255	255	255	255		tons	Capacity of trucks (Payload)
	Horsepower rating (HP) - From HB Mine Ops Jun2019	2,650	2,650	2,650	2,650		hp	Horsepower rating (HP) - From HB Mine Ops Jun2019

Haul Trucks - General Information	Hours of operation per year for the Tier 4F fleet	22,826	22,826	22,826	22,826		hours/year	Hours of operation per year for the Tier 4F fleet (hours from IMC truck fleet estimate, metered hours)
	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)	86	86	86	86		hours/day	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)
	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)	4	4	4	4		hours/hour	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)
	Load factor (from equipment list emailed by David on 04/16/14)	0.32	0.32	0.32	0.32		--	Load factor (from equipment list emailed by David on 04/16/14)
	Gasoline or Diesel (same as the Old MPO)	Diesel	Diesel	Diesel	Diesel		--	Gasoline or Diesel (same as the Old MPO)
	On-road or Nonroad engine (same as the Old MPO)	Nonroad	Nonroad	Nonroad	Nonroad		--	On-road or Nonroad engine (same as the Old MPO)
	Tier Rating (from equipment list emailed by David on 04/16/14)	Tier 4I/Tier 4F	Tier 4I/Tier 4F	Tier 4I/Tier 4F	Tier 4I/Tier 4F		--	Tier Rating (from equipment list emailed by David on 04/16/14)
Haul Trucks - Hauling Ore	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**	**2,524**	**1,330**	**1,187**	**1,212**	6,254	**feet**	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**
	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	3,683	7,023	10,055	1,283	22,044	VMT/year	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	10	19	28	4	60	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	0	1	1	0	3	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.	**7,726**	**3,570**	**1,771**	**3,519**	16,586	**feet**	**One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.**
	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	11,276	18,846	14,995	3,724	48,841	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	31	52	41	10	134	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	1	2	2	0	6	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled in the pit when hauling ore to the ROM HLP (Weighted average distance, LG ore hauled from several locations in pit)	**1,816**	**0**	**1,031**	**1,005**	3,852	**feet**	**One way distance traveled in the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled from several locations in pit)**

Vehicle miles traveled per year in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	8,226	0	1,826	10,016	20,067	VMT/year	Vehicle miles traveled per year in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	23	0	5	27	55	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	1	0	0	1	2	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
One way distance traveled out of the pit when hauling ore to the ROM Stockpile - LHP (Weighted average distance, LG ore hauled to different lifts in stockpile)	**11,064**	**0**	**5,108**	**6,857**	23,029	**feet**	**One way distance traveled out of the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled to different lifts in stockpile)**
Vehicle miles traveled per year out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	50,114	0	9,047	68,329	127,490	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	137	0	25	187	349	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	6	0	1	8	15	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
One way distance traveled in the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different location in pit)	**0**	**0**	**0**	**0**	0	**feet**	**One way distance traveled in the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different location in pit)**
One way distance traveled out of the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different locations in pit)	**0**	**0**	**0**	**0**	0	**feet**	**One way distance traveled out of the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different locations in pit)**
Percent of waste rock that is for tailings buttresses	0%	0%	0%	0%	0%	%	Percent of waste rock that is for tailings buttresses
One way distance traveled in the pit when hauling waste rock to storage areas (Weighted average distance, rock hauled from different locations in pit)	**2,586**	**1,612**	**1,240**	**1,271**	6,708	**feet**	**One way distance traveled in the pit when hauling waste rock to storage areas (Weighted average distance, rock hauled from different locations in pit)**
One way distance traveled out of the pit when hauling waste rock to storage areas (Weighted average distance, rock hauled to different locations from pit)	**11,507**	**7,351**	**5,551**	**7,300**	31,709	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage areas (Weighted average distance, rock hauled to different locations from pit)**
Percent of waste rock that is sent to storage areas	100%	100%	100%	100%	100%	%	Percent of waste rock that is sent to storage areas
Vehicle miles traveled per year in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	5,550	2,730	4,247	1,093	13,620	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)

	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	15	7	12	3	37	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	0.6	0.3	0.5	0.1	2	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	24,696	12,454	19,012	6,280	62,443	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	68	34	52	17	171	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)	3	1	2	1	7	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock (based on mining rates, distances traveled, percentages of the different types of waste rock)

Rosemont Project

Emissions Inventory For Haul Trucks

Hudbay, RP21

CAT 793F

Year		BT	RO1	TOTAL		
Total Truck Fleet	RP21Jul	21	21			
Trucks - metered hours per shift	RP21Jul	9	9			
Truck Shifts Ore to Crusher	RP21Jul	8,379	3,138			
Truck Shifts Ore to HLP	RP21Jul	2,813	3,770			
Truck Shifts Waste	RP21Jul	4,332	8,615			
Mining and Transferring of Ore to be Concentrated (sulfide ore)	**Quantity of ore mined per year**	**11,421,984**	**10,478,016**	**21,900,000**	tons/year	Quantity of sulfide ore mined per year
	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1	31,293	28,707	**60,000**	tons/day	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1
	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly mill capacity	1,422	1,305	**2,727**	tons/hour	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly crusher capacity
	Type of transfer to the haul trucks	In the Pit	In the Pit		--	Type of transfer to the haul trucks
	Type of transfer from the haul trucks	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks
Mining and Transferring of Waste Rock to be Placed in Storage Areas	**Quantity of waste rock mined per year**	**5,904,615**	**28,770,385**	**34,675,000**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 2 shifts/day	16,177	78,823	**95,000**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 24 hours/day)	674	3,284	**3,958**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 24 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mining and Transferring of ROM to be Placed in HLP	**Quantity of ROM ore mined per year**	**3,834,398**	**12,590,602**	**16,425,000**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of ROM mined per day. Entire fleet operating at 100% efficiency, 2 shifts/day	10,505	34,495	**45,000**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of ROM mined per hour (based on the maximum daily mining rate divided by 24 hours/day)	438	1,437	**1,875**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 24 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mobile Equipment for Mining						
	Maximum quantity of Tier 2 trucks used during the year	0	0		trucks	Maximum quantity of Tier 2 trucks used during the year
	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)	21	21	21	trucks	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)
	Total fleet size (Tier 4F trucks)	21	21	21	--	Total fleet size (Tier 4F trucks)
	Empty weight of trucks MSD bodies are assumed	166.7	166.7	167	tons	Empty weight of trucks MSD bodies are assumed
	Capacity of trucks (Payload)	255	255	255	tons	Capacity of trucks (Payload)
	Horsepower rating (HP) - From HB Mine Ops Jun2019	2,650	2,650	2,650	hp	Horsepower rating (HP) - From HB Mine Ops Jun2019
					hours/year	
					hours/day	
					hours/hour	

Haul Trucks - General Information	Hours of operation per year for the Tier 4F fleet	134,291	134,291	134,291	hours/year	Hours of operation per year for the Tier 4F fleet (hours from IMC truck fleet estimate, metered hours)
	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)	504	504	504	hours/day	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)
	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)	21	21	21	hours/hour	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)
	Load factor (from equipment list emailed by David on 04/16/14)	0.32	0.32	0.32	--	Load factor (from equipment list emailed by David on 04/16/14)
	Gasoline or Diesel (same as the Old MPO)	Diesel	Diesel	Diesel	--	Gasoline or Diesel (same as the Old MPO)
	On-road or Nonroad engine (same as the Old MPO)	Nonroad	Nonroad	Nonroad	--	On-road or Nonroad engine (same as the Old MPO)
	Tier Rating (from equipment list emailed by David on 04/16/14)	Tier 4I/Tier 4F	Tier 4I/Tier 4F	Tier 4I/Tier 4F	--	Tier Rating (from equipment list emailed by David on 04/16/14)
Haul Trucks - Hauling Ore	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**	**798**	**2,383**	3,181	**feet**	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**
	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	13,540	37,093	50,633	VMT/year	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	37	102	139	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	2	5	6	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.	**13,726**	**21,508**	35,234	**feet**	**One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.**
	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	232,884	334,758	567,642	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	638	917	1,555	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	29	42	71	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled in the pit when hauling ore to the ROM HLP (Weighted average distance, LG ore hauled from several locations in pit)	**1,467**	**2,633**	4,100	**feet**	**One way distance traveled in the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled from several locations in pit)**
	Vehicle miles traveled per year in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	8,357	49,250	57,606	VMT/year	Vehicle miles traveled per year in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	23	135	158	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)

Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	1	6	7	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
One way distance traveled out of the pit when hauling ore to the ROM Stockpile - LHP (Weighted average distance, LG ore hauled to different lifts in stockpile)	**17,120**	**24,902**	42,022	**feet**	**One way distance traveled out of the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled to different lifts in stockpile)**
Vehicle miles traveled per year out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	97,511	465,727	563,238	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	267	1276	1,543	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	11	53	64	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
One way distance traveled in the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled from different locations in pit)	**3,137**	**5,578**	8,714	**feet**	**One way distance traveled in the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled from different locations in pit)**
One way distance traveled in the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled from different locations in pit)	**3,137**	**5,578**	8,714	**feet**	**One way distance traveled in the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled from different locations in pit)**
One way distance traveled out of the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled to different locations from pit)	**9,217**	**16,999**	26,215	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled to different locations from pit)**
One way distance traveled out of the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled to different locations from pit)	**6,629**	**14,411**	21,040	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled to different locations from pit)**
Percent of waste rock that is sent to storage areas	100%	100%		%	Percent of waste rock that is sent to storage areas
Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	13,755	119,182	132,937	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	38	327	364	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	2	14	15	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	13,755	119,182	132,937	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)

Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	38	327	364	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	2	14	15	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	40420	363233	403,653	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	111	995	1,106	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	5	41	46	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	29071	307935	337,006	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	80	844	923	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	3	35	38	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)

Copper World Project

Emissions Inventory For Haul Trucks

CAT 793F

Year		**Yr14**	**TOTAL**		
Total Truck Fleet	Copper World	25			
Trucks - metered hours per shift	Copper World	9			
Truck Shifts Ore to Crusher	Copper World	5,831			
Truck Shifts Ore to HLP	Copper World	0			
Truck Shifts Waste	Copper World	12,407			
Mining and Transferring of Ore to be Concentrated (sulfide ore)	**Quantity of ore mined per year**	**21,900,000**	**21,900,000**	tons/year	Quantity of sulfide ore mined per year
	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1	60,000	**60,000**	tons/day	Maximum quantity of sulfide ore mined per day (based on the maximum mill throughput rate) after ramp up in year 1
	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly mill capacity	2,715	**2,715**	tons/hour	Maximum quantity of sulfide ore mined per hour. Based on maximum hourly crusher capacity
	Type of transfer to the haul trucks	In the Pit		--	Type of transfer to the haul trucks
	Type of transfer from the haul trucks	Unprotected from Wind		--	Type of transfer from the haul trucks
Mining and Transferring of Waste Rock to be Placed in Storage Areas	**Quantity of waste rock mined per year**	**46,600,000**	**46,600,000**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 2 shifts/day	127,671	**127,671**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 24 hours/day)	5,320	**5,320**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 23 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mining and Transferring of ROM to be Placed in HLP	**Quantity of ROM ore mined per year**	**0**	**0**	tons/year	Quantity of waste rock mined per year
	Maximum quantity of ROM mined per day. Entire fleet operating at 100% efficiency, 2 shifts/day	0	**0**	tons/day	Maximum quantity of waste rock mined per day, including oxide heap. Entire fleet operating at 100% efficiency, 11.5 metered hours per shift, 2 shifts/day
	Maximum quantity of ROM mined per hour (based on the maximum daily mining rate divided by 24 hours/day)	0	**0**	tons/hour	Maximum quantity of waste rock mined per hour, including oxide ore (based on the maximum daily mining rate divided by 23 hours/day)
	Type of transfer to the haul trucks (same as the Old MPO)	In the Pit		--	Type of transfer to the haul trucks (same as the Old MPO)
	Type of transfer from the haul trucks (same as the Old MPO)	Unprotected from Wind		--	Type of transfer from the haul trucks (same as the Old MPO)
Mobile Equipment for Mining					
	Maximum quantity of Tier 2 trucks used during the year	0		trucks	Maximum quantity of Tier 2 trucks used during the year
	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)	24.67081786		trucks	Maximum quantity of Tier 4F trucks used during the year. (Number of trucks in fleet)
	Total fleet size (Tier 4F trucks)	25		--	Total fleet size (Tier 4F trucks)
	Empty weight of trucks MSD bodies are assumed	166.7		tons	Empty weight of trucks MSD bodies are assumed
	Capacity of trucks (Payload)	255		tons	Capacity of trucks (Payload)
	Horsepower rating (HP) - From HB Mine Ops Jun2019	2,650		hp	Horsepower rating (HP) - From HB Mine Ops Jun2019

Haul Trucks - General Information	Hours of operation per year for the Tier 4F fleet	157,765		hours/year	Hours of operation per year for the Tier 4F fleet (hours from IMC truck fleet estimate, metered hours)
	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)	592		hours/day	Maximum hours of operation per day for the Tier 4F fleet (assume 24 hours/day for each haul truck)
	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)	25		hours/hour	Maximum hours of operation per hour for the Tier 4F fleet (assume 60 minutes/hour per haul truck)
	Load factor (from equipment list emailed by David on 04/16/14)	0.32		--	Load factor (from equipment list emailed by David on 04/16/14)
	Gasoline or Diesel (same as the Old MPO)	Diesel		--	Gasoline or Diesel (same as the Old MPO)
	On-road or Nonroad engine (same as the Old MPO)	Nonroad		--	On-road or Nonroad engine (same as the Old MPO)
	Tier Rating (from equipment list emailed by David on 04/16/14)	Tier 4I/Tier 4F		--	Tier Rating (from equipment list emailed by David on 04/16/14)
Haul Trucks - Hauling Ore	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**	**9,586**	9,586	**feet**	**One way distance traveled in the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance, ore hauled from several locations in pit)**
	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	311,854	311,854	VMT/year	Vehicle miles traveled per year in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	854	854	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	39	39	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.	**21,566**	21,566	**feet**	**One way distance traveled out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (Weighted average distance.**
	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	701,558	701,558	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	1,922	1,922	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)	87	87	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore directly to the Primary Crusher Dump Hopper (based on mining rates and distance traveled)
	One way distance traveled in the pit when hauling ore to the ROM HLP (Weighted average distance, LG ore hauled from several locations in pit)	**0**	0	**feet**	**One way distance traveled in the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled from several locations in pit)**
	Vehicle miles traveled per year in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/year	Vehicle miles traveled per year in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)

	Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	One way distance traveled out of the pit when hauling ore to the ROM Stockpile - LHP (Weighted average distance, LG ore hauled to different lifts in stockpile)	**0**	0	**feet**	**One way distance traveled out of the pit when hauling ore to the ROM Stockpile - Low Grade ore (Weighted average distance, LG ore hauled to different lifts in stockpile)**
	Vehicle miles traveled per year out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/year	Vehicle miles traveled per year out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM LHP (based on mining rates and distance traveled)	0	0	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling ore to the ROM Low Grade Ore Stockpile (based on mining rates and distance traveled)
	One way distance traveled in the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different location in pit)	**0**	0	**feet**	**One way distance traveled in the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different location in pit)**
	One way distance traveled out of the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different locations in pit)	**0**	0	**feet**	**One way distance traveled out of the pit when hauling waste rock for tailings buttresses (Weighted average distance, rock hauled from different locations in pit)**
	Percent of waste rock that is for tailings buttresses	0%	0%	%	Percent of waste rock that is for tailings buttresses
	One way distance traveled in the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled from different locations in pit)	**11,658**	11,658	**feet**	**One way distance traveled in the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled from different locations in pit)**
	One way distance traveled in the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled from different locations in pit)	**11,658**	11,658	**feet**	**One way distance traveled in the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled from different locations in pit)**
	One way distance traveled in the pit when hauling waste rock to storage area F (Weighted average distance, rock hauled from different locations in pit)	**11,658**	11,658	**feet**	**One way distance traveled in the pit when hauling waste rock to storage area F (Weighted average distance, rock hauled from different locations in pit)**
	One way distance traveled in the pit when hauling waste rock to storage areaG (Weighted average distance, rock hauled from different locations in pit)	**11,658**	11,658	**feet**	**One way distance traveled in the pit when hauling waste rock to storage areaG (Weighted average distance, rock hauled from different locations in pit)**
	One way distance traveled out of the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled to different locations from pit)	**14,779**	14,779	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area C (Weighted average distance, rock hauled to different locations from pit)**
	One way distance traveled out of the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled to different locations from pit)	**14,779**	14,779	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area D (Weighted average distance, rock hauled to different locations from pit)**
	One way distance traveled out of the pit when hauling waste rock to storage area F (Weighted average distance, rock hauled to different locations from pit)	**8,434**	8,434	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area F (Weighted average distance, rock hauled to different locations from pit)**

	One way distance traveled out of the pit when hauling waste rock to storage area G (Weighted average distance, rock hauled to different locations from pit)	**7,721**	7,721	**feet**	**One way distance traveled out of the pit when hauling waste rock to storage area G (Weighted average distance, rock hauled to different locations from pit)**
	Percent of waste rock that is sent to storage areas	100%	100%	%	Percent of waste rock that is sent to storage areas
	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	201,746	201,746	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	553	553	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	23	23	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	201,746	201,746	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	553	553	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	23	23	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	201,746	201,746	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	553	553	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	23	23	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	201,746	201,746	VMT/year	Vehicle miles traveled per year in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	553	553	VMT/day	Maximum vehicle miles traveled per day in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)

	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	23	23	VMT/hour	Maximum vehicle miles traveled per hour in the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	255,762	255,762	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	701	701	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)	29	29	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile C (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	255,762	255,762	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	701	701	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)	29	29	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile D (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	145,950	145,950	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	400	400	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)	17	17	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile F (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	133,621	133,621	VMT/year	Vehicle miles traveled per year out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	366	366	VMT/day	Maximum vehicle miles traveled per day out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)
	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)	15	15	VMT/hour	Maximum vehicle miles traveled per hour out of the pit when hauling all types of waste rock to Pile G (based on mining rates, distances traveled, percentages of the different types of waste rock)

APPENDIX I. OZONE AND SECONDARY $PM_{2.5}$ GUIDANCE

UNITED STATES ENVIRONMENTAL PROTECTION AGENCY
RESEARCH TRIANGLE PARK, NC 27711

OFFICE OF
AIR QUALITY PLANNING
AND STANDARDS

July 29, 2022

MEMORANDUM

SUBJECT: Guidance for Ozone and Fine Particulate Matter Permit Modeling

FROM: Richard Wayland, Division Director
Air Quality Assessment Division

Scott Mathias, Division Director
Air Quality Policy Division

TO: Regional Air Division Directors, Regions 1 – 10

The Environmental Protection Agency (EPA) is pleased to release the attached "Guidance for Ozone and Fine Particulate Matter Permit Modeling" (final guidance) in a final form to the state, local, and tribal air agencies, as well as the public. The final guidance reflects the EPA's recommendations for how a stationary source seeking a Prevention of Significant Deterioration (PSD) permit may demonstrate that it will not cause or contribute to a violation of the National Ambient Air Quality Standards (NAAQS) for ozone (O_3) and fine particulate matter ($PM_{2.5}$) and PSD increments for $PM_{2.5}$, as required under Section 165(a)(3) of the Clean Air Act and 40 CFR sections 51.166(k) and 52.21(k).

The final guidance does not substitute for provisions or regulations of the Clean Air Act, nor is it a regulation itself. As the term "guidance" suggests, it provides recommendations on how to implement the modeling requirements of a PSD compliance demonstration. Thus, it does not impose binding, enforceable requirements on any party, nor does it assure that the EPA will approve all instances of its application, as the guidance may not apply to a particular situation based upon the circumstances. Final decisions by the EPA regarding a particular PSD compliance demonstration will only be made based on the statute and applicable regulations and will only be made following a final submission by air agencies and after notice and opportunity for public review and comment.

BACKGROUND

On December 20, 2016, the Administrator signed a final rule[1] that revised the *Guideline on Air Quality Models*.[2] The final rule was published in the Federal Register on January 17, 2017, and the effective date of this action was deferred to May 22, 2017. The 2017 *Guideline* provides EPA-recommended models and other techniques, as well as guidance on their use, for predicting ambient concentrations of air pollutants. For this final revision to the 2017 *Guideline*, the EPA determined that advances in chemical transport modeling science indicate that it is now reasonable to provide more specific, generally applicable guidance that identifies particular models or analytical techniques that may be used under specific circumstances for assessing the impacts of an individual source on secondary formation of O_3 and $PM_{2.5}$.

As discussed in the preamble of the 2017 revisions to the EPA's *Guideline on Air Quality Models*:

> "…the EPA has determined that advances in chemical transport modeling science indicate it is now reasonable to provide more specific, generally-applicable guidance that identifies particular models or analytical techniques that may be used under specific circumstances for assessing the impacts of an individual or single source on ozone and secondary $PM_{2.5}$. For assessing secondary pollutant impacts from single sources, the degree of complexity required to appropriately assess potential impacts varies depending on the nature of the source, its emissions, and the background environment. In order to provide the user community flexibility in estimating single-source secondary pollutant impacts that allows for different approaches to credibly address these different areas, the EPA proposed a two-tiered demonstration approach for addressing single-source impacts on ozone and secondary $PM_{2.5}$."

This recommended two-tiered demonstration approach was promulgated as part of the 2017 *Guideline* revisions.

DRAFT AND REVISED DRAFT GUIDANCE

On February 10, 2020, the EPA provided an initial "DRAFT Guidance for Ozone and Fine Particulate Matter Permit Modeling"[3] (draft guidance) to the state, local, and tribal air agencies, as well as the public, for consideration, review, and comment. Upon consideration of the comments received, and consistent with Executive Order 13990, the EPA decided to revise one important aspect of that draft guidance and, as a result, provided a "Revised Draft Guidance for

[1] https://www.epa.gov/scram/2017-appendix-w-final-rule.

[2] *Guideline on Air Quality Models*. 40 CFR Part 51, Appendix W (82 FR 5182, Jan. 17, 2017). https://www.epa.gov/sites/production/files/2020-09/documents/appw_17.pdf. Also known as the "2017 *Guideline*."

[3] "DRAFT Guidance for Ozone and Fine Particulate Matter Permit Modeling." February 10, 2020. Publication No. EPA 457-P-20-002. Office of Air Quality Planning and Standards, Research Triangle Park, NC. https://www.epa.gov/scram/draft-guidance-ozone-and-fine-particulate-matter-permit-modeling.

Ozone and Fine Particulate Matter Permit Modeling"[4] (revised draft guidance) on September 20, 2021 for additional consideration, review and comment. The revision reflected a change in EPA policy with respect to determining which regulated New Source Review (NSR) pollutants should be included in PSD compliance demonstration for O_3 and $PM_{2.5}$.

In the February 10, 2020 draft guidance, EPA's recommended compliance demonstration approach was that sources only include those precursors (or the direct component, in the case of $PM_{2.5}$) that would be emitted in a significant amount for purposes of determining whether a source will cause or contribute to a NAAQS or PSD increment violation. The September 20, 2021 revised guidance communicated EPA's current policy that, in order to make the required demonstration that the allowable emissions increases from a source or modification would not cause or contribute to a NAAQS or PSD increment violation, sources should provide a full accounting of the combined impacts of their allowable precursor (and direct component, in the case of $PM_{2.5}$) emissions on ambient concentrations of the relevant NAAQS (*i.e.*, O_3 or $PM_{2.5}$) if any precursor(s) (or the direct component, in the case of $PM_{2.5}$) would be emitted in a significant amount. In other words, for O_3, if either NO_X or VOC precursor emissions would be emitted in a significant amount, then both precursors should be included in the assessment of O_3 impacts. Analogously, for $PM_{2.5}$, if a source would emit a significant amount of one or more of: NO_X, SO_2, or direct $PM_{2.5}$ emissions, then the source should include NO_X and SO_2 precursor and direct $PM_{2.5}$ emissions in the assessment of $PM_{2.5}$ impacts.

As described in the revised draft guidance, this holistic approach to the PSD compliance demonstrations for O_3 and $PM_{2.5}$ is supported both scientifically and legally. This is because it ensures that the source provides a full accounting of its projected air quality impacts for the relevant NAAQS pollutant, including all precursor (and direct component, in the case of $PM_{2.5}$) emissions. Therefore, it better aligns with the requirements in the PSD regulations that the owner or operator of a proposed new major stationary source or major modification demonstrate that it will not cause or contribute to a NAAQS or PSD increment violation.

FINAL GUIDANCE

Based on the feedback received to both the draft and revised draft guidance documents and subsequent revisions, the EPA is now able to finalize and provide the attached "Guidance for Ozone and Fine Particulate Matter Permit Modeling" in a final form to the state, local, and tribal air agencies, as well as the public. We are maintaining the holistic compliance demonstration approach and all other recommendations from the revised draft guidance. We have made a few clarifications and associated updates to the final guidance based on the external comments, but the overall nature of the final guidance remains unchanged from the revised draft guidance.

[4] "Revised Draft Guidance for Ozone and Fine Particulate Matter Permit Modeling." September 20, 2021. Publication No. EPA 454-P-21-001. Office of Air Quality Planning and Standards, Research Triangle Park, NC. https://www.epa.gov/scram/revised-draft-guidance-ozone-and-fine-particulate-matter-permit-modeling.

This final guidance is now the full replacement to the previous "Guidance for $PM_{2.5}$ Permit Modeling"[5] reflecting the 2017 revisions to the *Guideline* and incorporation of appropriate sections for addressing O_3 along with, or in additional to, $PM_{2.5}$. The final guidance also replaces the February 10, 2020 draft and September 20, 2021 revised guidance documents and the recommendations contained within.

As additional experience is gained with O_3 and $PM_{2.5}$ PSD compliance demonstrations, the EPA may update this and related guidance and provide further specificity on procedures for assessing the impacts of a single source on O_3 and secondary $PM_{2.5}$ concentrations. The EPA still highly recommends consultation with the appropriate permitting authority and EPA Regional Office for any permit applicants developing O_3 and $PM_{2.5}$ PSD compliance demonstrations. Such consultation can resolve potential issues early in the permitting process and alleviate unnecessary work with developing an acceptable compliance demonstration.

WEBINAR AND CONTACT INFORMATION

The EPA will conduct a release webinar providing an overview of the final guidance allowing for an open exchange on Thursday, August 11th at 3pm EDT. Additional information on how to connect to the webinar is posted on the EPA's SCRAM website, https://www.epa.gov/scram, under the Announcements section and will be shared with the regulatory air quality modeling community through typical email distributions.

For convenience, the final guidance document is available electronically on the EPA's SCRAM website at:
https://www.epa.gov/scram/guidance-ozone-and-fine-particulate-matter-permit-modeling.

If there are any questions regarding the final guidance, please contact George Bridgers of EPA's Air Quality Modeling Group at (919) 541-5563 or *bridgers.george@epa.gov*.

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Attachment

[5] "Guidance for PM2.5 Modeling." May 20, 2014. Publication No. EPA-454/B-14-001. Office of Air Quality Planning and Standards, Research Triangle Park, NC.
https://www.epa.gov/sites/production/files/2020-09/documents/guidance_for_pm25_permit_modeling.pdf.

Guidance for Ozone and Fine Particulate Matter Permit Modeling

EPA-454/R-22-005
July 2022

Guidance for Ozone and Fine Particulate Matter Permit Modeling

U.S. Environmental Protection Agency
Office of Air Quality Planning and Standards
Air Quality Assessment Division
Research Triangle Park, NC

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I. Introduction

The U.S. Environmental Protection Agency (EPA) is providing this "Guidance for Ozone and Fine Particulate Matter Permit Modeling" to fulfill a need for additional guidance on demonstrating compliance with the ozone (O_3) and fine particulate matter ($PM_{2.5}$) National Ambient Air Quality Standards (NAAQS) and the Prevention of Significant Deterioration (PSD) increments for $PM_{2.5}$ in the context of PSD permit applications. Because of the complex chemistry of secondary formation of O_3 and $PM_{2.5}$, the EPA's judgment in the past was that it was not technically sound to specify with "reasonable particularity" air quality models that must be used to assess the impacts of a single source on O_3 and secondary $PM_{2.5}$ concentrations. Instead, the EPA employed a case-by-case process for determining analytical techniques that should be used for these secondary pollutants. Under the former process, the EPA recommended that the "[c]hoice of methods used to assess the impact of an individual source depends on the nature of the source and its emissions. Thus, model users should consult with their Regional Office to determine the most suitable approach on a case-by-case basis" (2005 *Guideline on Air Quality Models,* U.S. EPA, 2005; hereafter referred to as 2005 *Guideline*; sections 5.2.1.c and 5.2.2.1.c). As such, under the 2005 *Guideline*, the appropriate methods for assessing O_3 and secondary $PM_{2.5}$ impacts were determined as part of the normal consultation process with the appropriate permitting authority.

On January 4, 2012, the EPA granted a petition submitted on behalf of the Sierra Club on July 28, 2010 (U.S. EPA, 2012), which requested that the EPA initiate rulemaking regarding the establishment of air quality models for O_3 and $PM_{2.5}$ for use by all major sources applying for a PSD permit. In granting that petition, the EPA committed to engage in rulemaking to evaluate whether updates to the 2005 *Guideline* were warranted and, as appropriate, incorporate new

analytical techniques or models for O_3 and secondarily formed $PM_{2.5}$. As discussed in the preamble of the 2017 revisions to the EPA's *Guideline on Air Quality Models* (U.S. EPA, 2017a; hereafter referred to as 2017 *Guideline*), "the EPA has determined that advances in chemical transport modeling science indicate it is now reasonable to provide more specific, generally-applicable guidance that identifies particular models or analytical techniques that may be used under specific circumstances for assessing the impacts of an individual or single source on ozone and secondary $PM_{2.5}$. For assessing secondary pollutant impacts from single sources, the degree of complexity required to appropriately assess potential impacts varies depending on the nature of the source, its emissions, and the background environment. In order to provide the user community flexibility in estimating single-source secondary pollutant impacts that allows for different approaches to credibly address these different areas, the EPA proposed a two-tiered demonstration approach for addressing single-source impacts on ozone and secondary $PM_{2.5}$." This recommended two-tiered demonstration approach was promulgated as part of the 2017 *Guideline* revisions.

As presented in section 5.2 of the 2017 *Guideline*, the first tier involves use of technically credible relationships between precursor emissions and a source's impacts. Such information may be published in peer-reviewed literature; developed from modeling that was previously conducted for an area by a source, a governmental agency, or some other entity that is deemed sufficient; or generated by a peer-reviewed reduced form model. To assist permitting authorities, the EPA released the "Guidance on the Development of Modeled Emission Rates for Precursors (MERPs) as a Tier 1 Demonstration Tool for Ozone and $PM_{2.5}$ under the PSD Permitting Program" (U.S. EPA, 2019; hereafter referred to as MERPs Guidance) that provides a

framework to develop MERPs for consideration and use as a Tier 1 demonstration tool, as described in the preamble of the 2017 *Guideline*.

The second tier, also presented in section 5.2 of the 2017 *Guideline*, involves application of more sophisticated case-specific chemical transport models (CTMs), *e.g.*, photochemical grid models, to be determined in consultation with the EPA Regional Offices. The EPA provided guidance to permitting authorities on procedures for applying CTMs in the "Guidance on the Use of Models for Assessing the Impacts of Emissions from Single Sources on the Secondarily Formed Pollutants: Ozone and $PM_{2.5}$" (U.S. EPA, 2016; hereafter Single-source Modeling Guidance). The Single-source Modeling Guidance is intended to inform that second tier approach by providing appropriate technical methods to assess O_3 and secondary $PM_{2.5}$ impacts associated with the precursor emissions from the new or modifying source. The appropriate tier for a given application should be selected in consultation with the appropriate permitting authority and be consistent with EPA guidance.

This guidance provides an update to the previous "Guidance for $PM_{2.5}$ Permit Modeling" (U.S. EPA, 2014) to reflect the 2017 revisions to the *Guideline* and incorporate appropriate sections for O_3. As experience is gained with these types of PSD compliance demonstrations, the EPA expects to update this and related guidance and provide further specificity on procedures for assessing the impacts of a single source on O_3 and secondary $PM_{2.5}$ concentrations.

This guidance document is organized in three primary areas:

1. Guidance Overview – Section II provides a general overview of the steps that a permit applicant should take under the PSD program for demonstrating compliance with the O_3 NAAQS and/or the $PM_{2.5}$ NAAQS and PSD increments.

2. PSD Compliance Demonstrations for the O_3 and $PM_{2.5}$ NAAQS – Sections III and IV provide a detailed framework for conducting a source impact analysis and a cumulative impact analysis, respectively, to appropriately address O_3 and $PM_{2.5}$ impacts from the proposed source[1] in determining whether it may cause or contribute to a NAAQS violation.
3. PSD Compliance Demonstrations for $PM_{2.5}$ Increments – Section V provides a detailed discussion of the assessment of primary and secondary $PM_{2.5}$ impacts of a new or modifying source with respect to the $PM_{2.5}$ increments.

This document recommends procedures for permit applicants and permitting authorities to follow to show that they have satisfied some of the criteria for obtaining or issuing a permit under applicable PSD regulations. This document is not a rule or regulation, and the guidance it contains may not apply to a particular situation based upon the individual facts and circumstances. This guidance does not change or substitute for any law, regulation, or any other legally binding requirement, may refer to regulatory provisions without repeating them in their entirety, and is not legally enforceable. The use of non-mandatory language such as "guidance," "recommend," "may," "should," and "can," is intended to describe EPA policies and recommendations. Mandatory terminology such as "must" and "required" are intended to describe requirements under the terms of the CAA and EPA regulations, but this document does not establish or alter any legally binding requirements in and of itself.

This guidance does not create any rights or obligations enforceable by any party or impose binding, enforceable requirements on any PSD permit applicant, PSD permitting

[1] The term "proposed source" as used in this guidance document should be read to mean the proposed source or modification for which the compliance demonstration is being conducted.

authority, the EPA, or any other person. Since each permitting action will be considered on a case-by-case basis, this document does not limit or restrict any particular justifiable approach that permit applicants and permitting authorities may take to conduct the required compliance demonstrations. Each individual decision to issue a PSD permit must be supported by a record sufficient to demonstrate that the proposed construction and operation of a stationary source will not cause or contribute to a violation of the applicable NAAQS and PSD increments. While this document illustrates a particular approach that the EPA considers appropriate and acceptable as a general matter, permit applicants and permitting authorities should examine all relevant information regarding air quality in the area that may be affected by a proposed new or modifying source and evaluate whether alternative or additional analysis may be necessary in a given case to demonstrate that the regulatory criteria for a PSD air quality analysis are satisfied. This document does not represent a conclusion or judgment by the EPA that the technical approaches recommended in this document will be sufficient to make a successful compliance demonstration in every permit application or circumstance.

Permitting authorities retain the discretion to address particular issues discussed in this document in a different manner than the EPA recommends so long as the approach is adequately justified, supported by the permitting record and relevant technical literature, and consistent with the applicable requirements in the CAA and implementing regulations, including the terms of an approved State Implementation Plan (SIP) or Tribal Implementation Plan (TIP). Furthermore, this guidance is not a final agency action and does not determine applicable legal requirements or the approvability of any particular permit application.

The EPA Regional Offices may seek clarification from the EPA's Office of Air Quality Planning and Standards (OAQPS) on issues and areas of concern in a modeling protocol or PSD

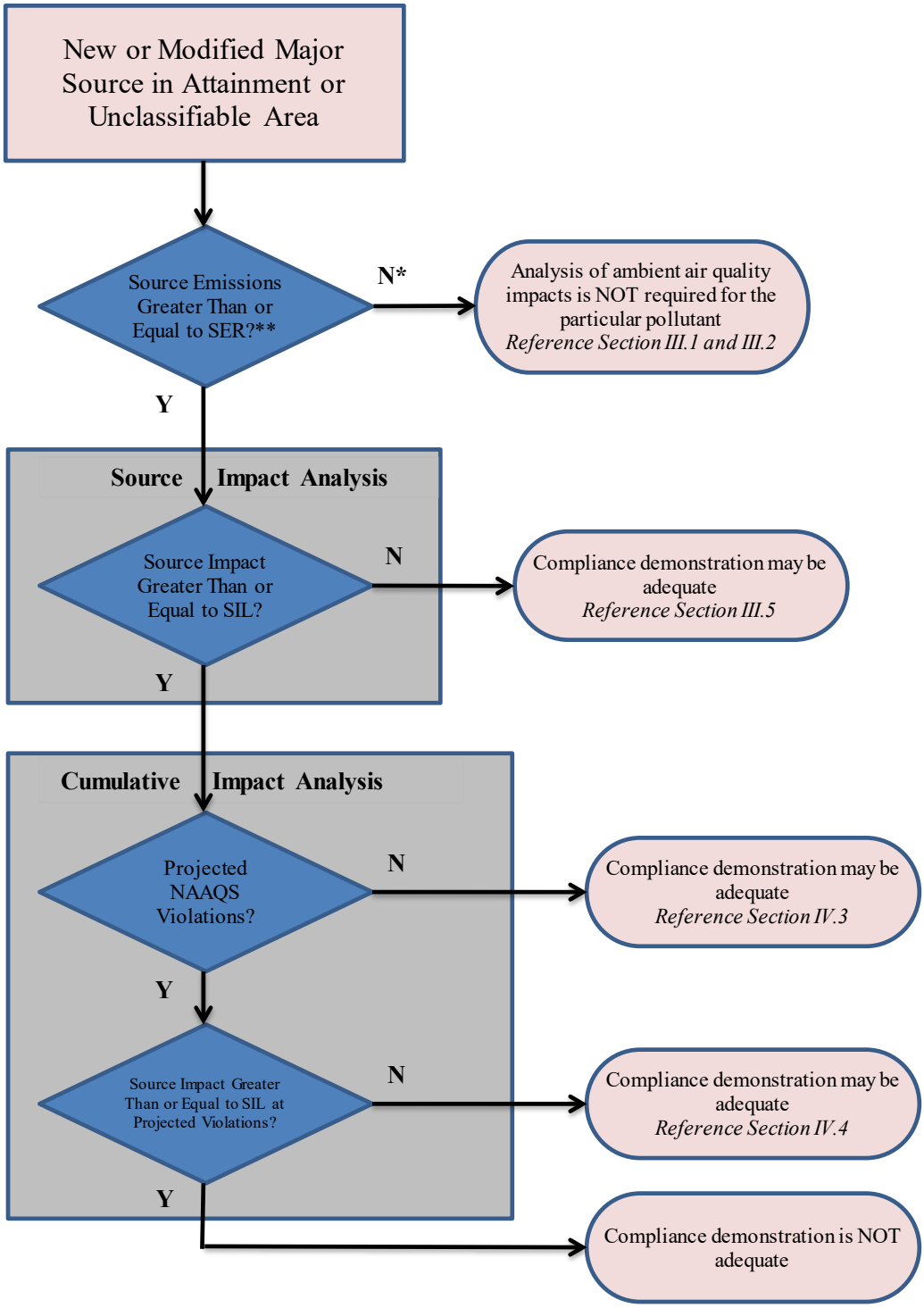
compliance demonstration. Through these interactions and subsequent resolutions of specific issues, clarifications of preferred modeling procedures can become additional EPA guidance. This can happen in several ways: 1) the preferred procedures are published as regulations or guidelines; 2) the preferred procedures are formally transmitted as guidance to the Air Division Directors in the EPA Regional Offices; 3) the preferred procedures are formally transmitted as guidance to the EPA Regional Office modeling contacts; or 4) the preferred procedures are relied upon in decisions by the EPA's Model Clearinghouse that establish national precedent that the approach is technically sound. The Model Clearinghouse is the EPA focal point for the review of the technical adequacy of pollutant modeling to satisfy regulatory criteria and other NAAQS compliance demonstration techniques. Model Clearinghouse memoranda involving interpretation of modeling guidance for specific applications, as well as other clarification memoranda addressing modeling more generally, are available at the Support Center for Regulatory Atmospheric Modeling (SCRAM) website at: https://www.epa.gov/scram/air-quality-model-clearinghouse.

II. Guidance Overview

This guidance is appropriate for proposed new or modifying sources locating in, or located in, an area classified as attainment or unclassifiable for O_3 and/or $PM_{2.5}$. It is intended to provide recommendations on how to conduct compliance demonstrations for the O_3 NAAQS and the $PM_{2.5}$ NAAQS and PSD increments under the PSD program following the progressive steps shown in Figure II-1 (for O_3 and $PM_{2.5}$ NAAQS) and Figure II-2 (for $PM_{2.5}$ increments). Since each permitting action is considered on a case-by-case basis, this guidance does not limit or restrict any particular justifiable approach that permit applicants and permitting authorities may take to conduct the required compliance demonstrations. Prospective permit applicants should recognize the importance of the consultation process with the appropriate permitting authority. This process will help identify the most appropriate analytical techniques to be used for conducting a compliance demonstration for the O_3 NAAQS and the $PM_{2.5}$ NAAQS and PSD increments.

The EPA has historically supported the use of screening tools to facilitate the implementation of the PSD program and streamline the permitting process in circumstances where proposed construction is projected to have an insignificant impact on air quality. These screening tools include significant emissions rates (SERs) and significant impact levels (SILs). The use of these screening tools at each progressive step, as demonstrated in Figure II-1 and Figure II-2, is described in more detail throughout Section II.

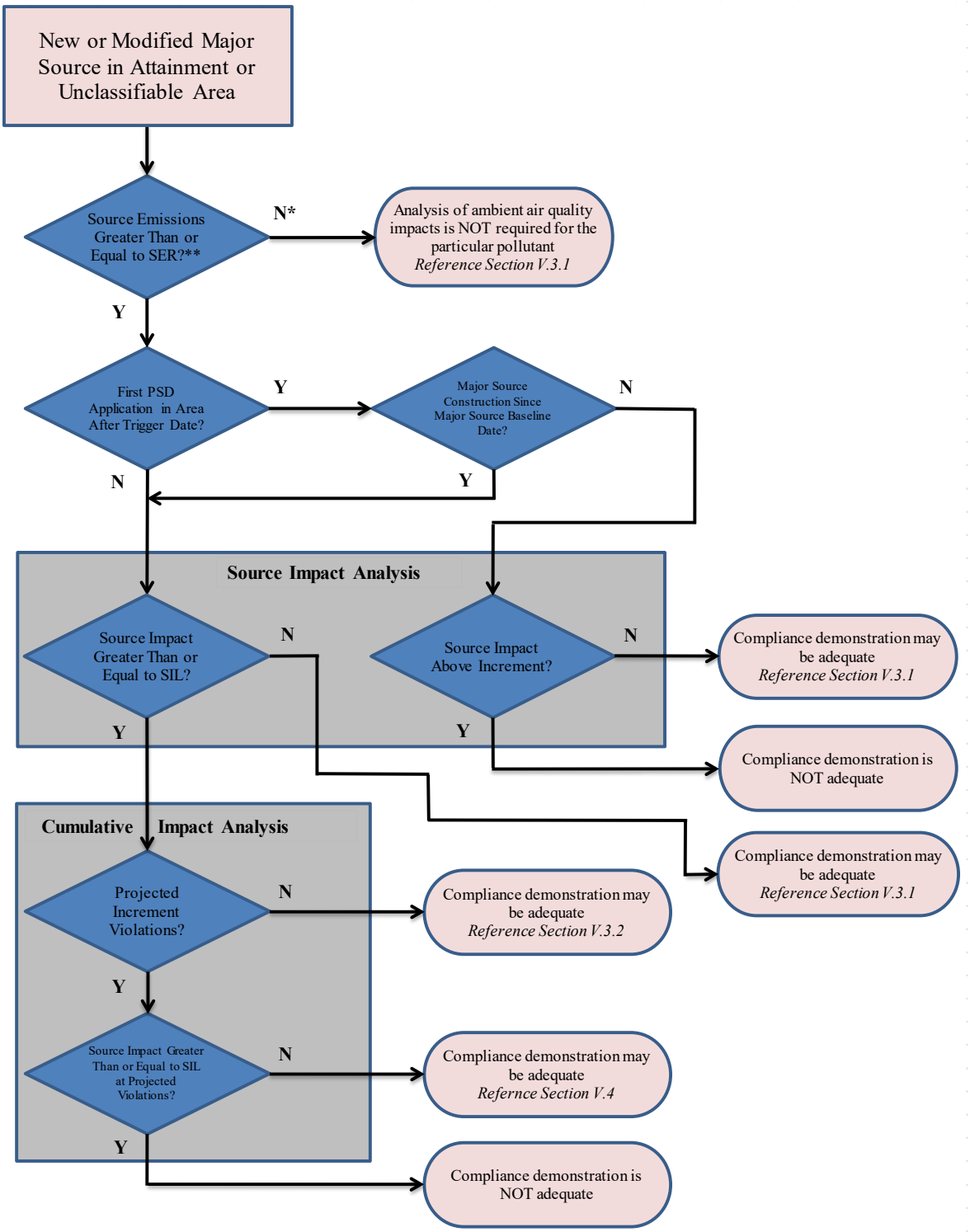
Figure II-1. Overview of O_3 and $PM_{2.5}$ NAAQS Compliance Demonstration for New or Modifying Sources under PSD Programs



* State, local, and tribal permit authorities may have specific regulations that require alternative or additional analyses and processes for assuring NAAQS and PSD Increments compliance.

** Any emissions rate or any net emissions increase associated with a major stationary source or major modification, which would construct within 10 kilometers of a Class I area, and have an impact on such area equal to or greater than 1 $\mu g/m^3$ (24-hour average), is considered significant and should proceed with an appropriate air quality assessment. *See* 40 CFR 52.21(b)(23)(iii).

Figure II-2. Overview of $PM_{2.5}$ PSD Increments Compliance Demonstration for New or Modifying Sources under PSD Programs



* State, local, and tribal permit authorities may have specific regulations that require alternative or additional analyses and processes for assuring NAAQS and PSD Increments compliance.

** Any emissions rate or any net emissions increase associated with a major stationary source or major modification, which would construct within 10 kilometers of a Class I area, and have an impact on such area equal to or greater than 1 $\mu g/m^3$ (24-hour average), is considered significant and should proceed with an appropriate air quality assessment. *See* 40 CFR 52.21(b)(23)(iii).

II.1 Significant Emissions Rates for O_3 and $PM_{2.5}$

O_3 and $PM_{2.5}$ are "regulated NSR pollutant[s]" as that term is defined in the PSD regulations.[2] Pursuant to that definition, ambient concentrations of O_3 are generally addressed through the regulation of its two precursors, nitrogen oxides (NO_X) and volatile organic compounds (VOC), while ambient concentrations of $PM_{2.5}$ are generally addressed through the regulation of direct $PM_{2.5}$ and its precursors, NO_X and sulfur dioxide (SO_2).[3] "Significant" is defined in the EPA regulations at 40 CFR 52.21(b)(23) in reference to a source's potential to emit (or in the case of a modification, the emissions increase[4] and net emissions increase) of a regulated NSR pollutant. That definition specifies the pollutant and the corresponding emissions rate that, if equaled or exceeded, would qualify as "significant." For ozone, the significant emissions rate is defined as 40 tpy of VOC or NO_X, and for $PM_{2.5}$, the significant emission rate is defined as 10 tpy of direct $PM_{2.5}$ emissions, 40 tpy of SO_2 emissions, or 40 tpy of NO_X emissions.[5]

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[2] 40 CFR 52.21(b)(50). The regulations at 40 CFR 52.21 apply to the federal PSD program. This guidance document generally cites those regulations for simplicity, but the guidance reflected here may also be considered when applying EPA-approved state regulations modeled on 40 CFR 51.166, which contains the PSD program requirements for an approvable SIP that parallel the requirements of 40 CFR 52.21. This guidance may also cite the regulations at 40 CFR 51.166 when specifically discussing requirements for state PSD programs.

[3] *See* 73 FR 28321, 28333 (May 16, 2008). The EPA's PSD regulations do not establish a presumption that VOC be treated as a precursor to $PM_{2.5}$ in the PSD program. However, a state, or the EPA, may demonstrate that VOC emissions in a specific area are a significant contributor to that area's ambient $PM_{2.5}$ concentrations and, thus, should be treated as a regulated NSR pollutant subject to the PSD permitting requirements. 40 CFR 51.166(b)(49)(i)(b)(4); 40 CFR 52.21(b)(50)(i)(b)(4).

[4] While section 52.21(b)(23) explicitly defines "significant" for purposes of a net emissions increase or potential to emit, section 52.21(b)(40) defines "significant emissions increase" by reference to the definition of "significant" found in paragraph (b)(23).

[5] A significance rate for VOC as a $PM_{2.5}$ precursor is not defined in the PSD regulations. However, the preamble to EPA's final rule on implementing the PSD permitting requirements for $PM_{2.5}$ and its precursors indicated that any state making a demonstration that VOC is a significant contributor to an area's ambient $PM_{2.5}$ concentrations under 40 CFR 51.166(b)(49)(i)(b)(4) "would be required to adopt the 40-tpy significant emissions rate [for VOC as a $PM_{2.5}$ precursor] unless it demonstrates that a more stringent significant emissions rate (lower rate) is more appropriate." 73 FR at 28333.

II.2 Pollutant Applicability for O_3 and $PM_{2.5}$ PSD Air Quality Assessments

The EPA's PSD regulations apply specific permitting requirements to regulated New Source Review (NSR) pollutants that would be emitted in a significant amount by a proposed new or modified major stationary source.[6] For a new major stationary source, PSD permitting requirements apply to any regulated NSR pollutant for which the source would have the potential to emit a significant amount. For a modification at an existing major stationary source, PSD permitting requirements apply to any regulated NSR pollutant for which the modification would result in a significant emissions increase *and* a significant net emissions increase (*i.e.*, a "major modification") of that pollutant.[7] Regulated NSR pollutants include pollutants for which a NAAQS has been promulgated, such as O_3 and $PM_{2.5}$, including any pollutant identified in the regulations as a constituent or precursor of a pollutant subject to a NAAQS, *i.e.*, NO_X and VOC in the case of O_3, and $PM_{2.5}$ direct emissions, SO_2, and NO_X in the case of $PM_{2.5}$.[8] As described in Section II.1, SERs for direct $PM_{2.5}$ emissions and each precursor of O_3 and $PM_{2.5}$ are defined in the regulations.[9]

The CAA and the EPA's implementing regulations require a PSD permit applicant to demonstrate that emissions from the proposed source or modification will not cause or contribute

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[6] *See* 40 CFR 52.21(a)(2) for applicability procedures for new or modified major stationary sources. State, local, and tribal permit authorities may also have specific regulations that require alternative or additional analyses and processes for assuring NAAQS and PSD Increments compliance.

[7] Elsewhere in this document, simplified language may be used referring to a pollutant emitted in a significant amount or a source that would emit a significant amount of a pollutant. Where such language is used, it should be read to apply equally to the potential to emit of a new major stationary source and the emissions increase and net emissions increase from a modification at an existing major stationary source.

[8] *See* 40 CFR 52.21(b)(50).

[9] *See* 40 CFR 52.21(b)(23)(i). Individual O_3 precursors (*i.e.*, NO_X and VOC) are not summed when determining a significant emissions increase for O_3. Likewise, emissions of individual $PM_{2.5}$ precursors (*i.e.*, SO_2 and NO_X) are not summed when determining a significant emissions increase for $PM_{2.5}$; nor are emissions of a $PM_{2.5}$ precursor summed with direct $PM_{2.5}$ emissions when determining a significant emissions increase for $PM_{2.5}$. See 57 FR 55620, 55624 (Nov. 25, 1992); 80 FR 65292, 65441 (Oct. 26, 2015); *see also* 73 FR 28321, 28331 (May 16, 2008).

to a violation of any NAAQS or PSD increment and to provide an analysis of the impact of those emissions on ambient air quality based on monitoring data and air quality modeling.[10] The provisions at 40 CFR 52.21(k)(1) and (m)(1) describe the preconstruction air quality analysis requirements of the PSD program. Paragraph (k)(1) implements section 165(a)(3) of the CAA and provides that the owner or operator "shall demonstrate that allowable emission increases from the proposed source or modification. . . would not cause or contribute to air pollution in violation of [any NAAQS or PSD increment]." Paragraph (m)(1) implements section 165(e) of the CAA and provides that any PSD permit application shall contain an analysis of ambient air quality for each NAAQS pollutant that the source or modification would emit or increase in a significant amount and for each non-NAAQS pollutant as the Administrator determines necessary. Paragraph (m)(1)(iii) further provides that, for each NAAQS pollutant, the analysis shall contain continuous air quality monitoring data for determining whether emissions of that pollutant would cause or contribute to a violation of any NAAQS or PSD increment. For O_3 or $PM_{2.5}$, that analysis should examine the impact of the proposed source or modification on ambient concentrations of the NAAQS pollutant, as opposed to the impact of each individual precursor or direct component in isolation.

To make the required NAAQS or PSD increment compliance demonstration or air quality assessment, sources should provide a full accounting of the combined impacts of their allowable precursor (and direct component in the case of $PM_{2.5}$) emissions on ambient concentrations of the relevant NAAQS (*i.e.*, O_3 or $PM_{2.5}$) if any precursor(s) (or the direct component in the case of $PM_{2.5}$) would be emitted in a significant amount. In other words, for O_3, if either NOx or VOC precursor emissions would be emitted in a significant amount, then both precursors should be

[10] *See* CAA § 165(a)(3), CAA § 165(e), 40 CFR 52.21(k) and 40 CFR 52.21(m).

included in the assessment of O_3 impacts. Analogously, for $PM_{2.5}$, if a source would emit a significant amount of one or more of: NOx, SO_2, or direct $PM_{2.5}$ emissions, then the source should include NOx and SO_2 precursor and direct $PM_{2.5}$ emissions in the assessment of $PM_{2.5}$ impacts.[11] This approach is supported both scientifically, because it ensures that the source provides a full accounting of its projected air quality impacts for the relevant NAAQS, including all precursor (and direct component, in the case of $PM_{2.5}$) emissions, and legally, because it is needed to meet the requirements in the PSD regulations that the owner or operator of a proposed new major stationary source or major modification demonstrate that it will not cause or contribute to a NAAQS or PSD increment violation. The definition of "major modification" provides that any significant emissions increase or net emissions increase at a major stationary source that is significant for VOC *or* NO_X shall be considered significant for ozone.[12] This regulatory definition clearly states that if the emissions increase from a proposed modification at a major stationary source is significant for either VOC or NOx, then it shall be treated as significant not solely for the specific precursor that would exceed the SER but also for ozone in general. For purposes of the air quality assessment, this means that emissions of both ozone precursors should be evaluated to determine the proposed source or modification's impact on ambient ozone levels. Also, as discussed in Section II.1, the SER for ozone is defined as 40 tpy

[11] *See* Tables III-1 and III-2 for EPA recommended approaches for assessing ozone and $PM_{2.5}$ impacts by assessment case. This holistic approach is necessary for PSD air quality assessments for O_3 and $PM_{2.5}$ but not other substantive PSD permitting requirements, such as BACT, that apply directly to source emissions, and are not based on the source's projected impact on ambient air quality. The EPA regulations and longstanding EPA policy make clear that BACT limitations apply to directly emitted NAAQS pollutants or precursor pollutants (or both in the case of $PM_{2.5}$) that would be emitted from the proposed source (or increased by a modification) in a significant amount. *See* 40 CFR 52.21(j)(2), (3) and *In re Footprint Power Salem Harbor Development, LP*, PSD Appeal No. 14-02 (EAB 2014).

[12] *See* 40 CFR 52.21(b)(2)(ii). Similarly, the definition of "major stationary source" provides that a major source that is major for VOC *or* NO_X shall be considered major for ozone. *See* 40 CFR 52.21(b)(1)(ii).

of VOC *or* NO_X.[13] Thus, it is EPA's position that both scientific considerations and the regulatory language support a full accounting of the air quality impact of a pollutant and its precursors that would be emitted by a proposed source or modification, *i.e.*, all precursors, and the direct component in the case of $PM_{2.5}$, if any one of those would be emitted or would increase in a significant amount.

The EPA believes that adopting a narrower approach that would limit the air quality assessment to only the individual direct or precursor components with emissions equal to or greater than the corresponding SER, and excluding direct or precursor components with emissions less than the corresponding SER, would provide an incomplete and potentially deficient demonstration that the projected emissions from the proposed source or modification would not cause or contribute to a NAAQS or PSD increment violation. A reviewing authority considering only the impacts associated with a subset of direct and precursor emissions that would be emitted by the proposed source or modification may come to an incompletely supported determination that the required source impact demonstration had been made, whereas a more complete assessment that includes the impacts of all direct and precursor emissions may show that the proposed source or modification would cause or contribute to a NAAQS or PSD increment violation. Such a limited air quality assessment would be incomplete and therefore technically and legally flawed. A full accounting of the air quality impact of direct and precursor emissions, as applicable, is necessary to make the required demonstration that the allowable

[13] The SER definition for $PM_{2.5}$ is less clear because each pollutant-specific value is separated by a semicolon without using a connector such as "or;" however, the EPA reads the $PM_{2.5}$ SER definition consistently with the clearly stated ozone SER definition, meaning that for both ozone and $PM_{2.5}$, if the emissions of any precursor (or the direct emissions component in the case of $PM_{2.5}$) equals or exceeds the respective SER, all precursor emissions (and direct emissions in the case of $PM_{2.5}$) are treated as significant with respect to assessing air quality impacts for the corresponding NAAQS pollutant.

emissions increases would not cause or contribute to a violation of the NAAQS or PSD increments.

II.3 Significant Impact Levels for O_3 and $PM_{2.5}$

The EPA has issued guidance recommending that permitting authorities consider the use of appropriate pollutant-specific concentration levels known as "significant impact levels" as a compliance demonstration tool for O_3 and $PM_{2.5}$ air quality assessments on a case-by-case basis in PSD permitting actions (U.S. EPA, 2018a). The "SILs Guidance" identified recommended SIL values for the O_3 and $PM_{2.5}$ NAAQS and the $PM_{2.5}$ PSD increments and included a policy document, as well as supporting technical and legal analyses, that the EPA and other permitting authorities may use in case-by-case PSD permitting actions. As explained in the guidance, if a permitting authority chooses to use a recommended SIL value to support a PSD permitting decision, it should justify the SIL value and its use in the administrative record for the permitting action and may choose to rely upon the EPA's SILs Guidance, including the supporting technical and legal documents, in doing so.

The EPA's recommended SIL values from the SILs Guidance for the O_3 and $PM_{2.5}$ NAAQS are presented in Table II-1 and for the $PM_{2.5}$ PSD increments in Table II-2. It is important to note that the $PM_{2.5}$ NAAQS has two averaging periods: 24-hour and annual. There are no PSD increments established for O_3 and, thus, no O_3 increment SIL values. For a full discussion of the basis and purpose of the recommended O_3 and $PM_{2.5}$ SIL values, see the SILs Guidance and supporting documents (U.S. EPA, 2018a).

Table II-1. EPA Recommended SIL Values for O_3 and $PM_{2.5}$ NAAQS

Criteria Pollutant (NAAQS Level)	NAAQS SIL Concentration
Ozone 8-hour (70 ppb)	1.0 ppb
$PM_{2.5}$ 24-hour (35 μg/m^3)	1.2 μg/m^3*
$PM_{2.5}$ Annual (12 μg/m^3 or 15 μg/m^3)**	0.2 μg/m^3***

* The table accounts for the significant level for the 24-hour $PM_{2.5}$ NAAQS in 40 CFR 51.165(b)(2).

** Primary and secondary annual PM2.5 NAAQS, respectively.

*** The EPA recommends 0.2 μg/m3 as the SIL value. This value is lower than the value of 0.3 μg/m3 listed in 40 CFR 51.165(b)(2). Reference the SILs Gudiance for more information.

Table II-2. EPA Recommended SIL Values for $PM_{2.5}$ PSD Increments

Criteria Pollutant	PSD Increment SIL Concentration		
	Class I	Class II	Class III
$PM_{2.5}$ 24-hour	0.27 μg/m^3	1.2 μg/m^3	1.2 μg/m^3
$PM_{2.5}$ Annual	0.05 μg/m^3	0.2 μg/m^3	0.2 μg/m^3

As explained in the SILs Guidance, SILs are designed to have a role throughout the PSD air quality compliance demonstration. A permitting authority that chooses to use SILs should initially compare the modeled concentrations resulting from the proposed source's emissions increase at the affected emissions units to the appropriate SIL. The EPA calls this initial comparison the "Source Impact Analysis." Where the proposed source's predicted impacts on air quality concentrations are found at this first stage to be greater than or equal to the appropriate SIL, the analysis should then proceed to a second stage, which involves a cumulative assessment of the air quality in the affected area. The "Cumulative Impact Analysis" considers the combined impact of the proposed source or modification and other relevant sources in determining whether there would be a violation of any NAAQS or PSD increment in the affected area and, if so, whether the proposed source or modification would cause or contribute to such violation based on the appropriate SIL.

II.4 Source Impact Analysis

As described in section 9.2.3 of the 2017 *Guideline*, the EPA's recommended procedure for conducting a PSD air quality assessment is a multi-stage approach. The first stage is a single-source impact analysis or a source impact analysis.[14] This involves assessing whether the allowable emissions increase(s) from the affected emissions units at the proposed new or modifying source could cause or contribute to a NAAQS or PSD increment violation. As discussed in section II.3, the EPA issued the SILs Guidance containing recommendations on how to compare the impact from the source or modification alone to the appropriate SIL.

The owner or operator of a new major stationary source should perform a source impact analysis to inform the demonstration required for each regulated NSR pollutant that the source would have the potential to emit in a significant amount. The owner or operator of an existing source proposing a major modification should perform the analysis to inform the demonstration requirement for each regulated NSR pollutant that would result in a significant emissions increase and a significant net emissions increase, as determined by the PSD applicability procedures (see Section II.2 of this document). For O_3 or $PM_{2.5}$, which can be formed from precursor emissions, a significant increase of direct (for $PM_{2.5}$) or any precursor (for O_3 or $PM_{2.5}$) emissions would mean that the source should perform the required demonstration for all precursors (for O_3 or $PM_{2.5}$) and the primary pollutant (for $PM_{2.5}$) emitted. For O_3 this should

[14] This is consistent with the EPA's overall approach for the use of screening techniques in air quality modeling. See 40 CFR part 51, Appendix W, sections 2.2 ("Levels of Sophistication of Air Quality Analyses and Models") and 4.2.1 ("Screening Models and Techniques"). In section 2.2.a, the *Guideline* observes that "[it] is desirable to begin an air quality analysis by using simplified and conservative methods followed, as appropriate, by more complex and refined methods. The purpose of this approach is to streamline the process and sufficiently address regulatory requirements by eliminating the need of more detailed modeling when it is not necessary in a specific regulatory application. For example, in the context of a PSD permit application, a simplified and conservative analysis may be sufficient where it shows the proposed construction clearly will not cause or contribute to ambient concentrations in excess of either the NAAQS or the PSD increments."

include both NOx and VOC if either would be emitted in a significant amount. For $PM_{2.5,}$ this should include direct emissions of $PM_{2.5}$, as well as emissions of both NOx and SO_2 if any one or more of the three pollutants would be emitted in a significant amount. This holistic approach ensures that all relevant impacts from a proposed new major stationary source or major modification (*i.e.*, the combined effect of the source's direct and precursor emissions of O_3 or $PM_{2.5}$) are accounted for in a demonstration that the proposed new or modified major source will not cause or contribute to a NAAQS or PSD increment violation.

It is important to note that in many cases, the emissions rate(s) used for the source impact analysis should not be the same as the rate calculated for applicability purposes converted into equivalent short-term model input rates. First, as part of the 2002 NSR Reform Rule, the EPA made clear that "baseline actual emissions" and the "actual-to-projected-actual applicability test" should not be used for PSD air quality analyses.[15] Instead, for major modifications, the definition of "actual emissions" at 40 CFR 52.21(b)(21) continues to apply and post-project emissions should be based on potential to emit or allowable emissions.[16] Second, the "allowable emission increases" that must be evaluated pursuant to 40 CFR 52.21(k) should correspond with the averaging time of the applicable standard.[17] For major modifications, this may also depend on the type of emissions unit (new or existing) and the effect the project has on the emissions unit (*e.g.*, increase in short-term potential to emit vs. increase in annual utilization).

In a source impact analysis, as illustrated in Figure II-1 and Figure II-2 and further explained in this guidance, a permitting authority should compare the modeled concentrations

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[15] *See* 40 CFR 52.21(b)(21)(i) and 67 FR 80186 (December 31, 2002) at 80190-91, 80196.

[16] "In general, actual emissions as of a particular date shall equal the average rate, in tons per year, at which the unit actually emitted the pollutant during a consecutive 24-month period which precedes the particular date and which is representative of normal source operation." 40 CFR 52.21(b)(21)(ii).

[17] *See* Table 8-2 of the *Guideline*.

resulting from the proposed source's emissions increase to an appropriate O_3 or $PM_{2.5}$ SIL. If the proposed source's maximum modeled impacts are found to be below the level of the O_3 or $PM_{2.5}$ SIL at every modeled receptor, this finding of the source impact analysis may be sufficient to demonstrate that the source will not cause or contribute to a violation of the O_3 NAAQS, $PM_{2.5}$ NAAQS, or the $PM_{2.5}$ PSD increment, as necessary to receive a PSD permit. On the other hand, where the proposed source's predicted impacts on air quality concentrations are estimated to be greater than or equal to the level of an appropriate O_3 or $PM_{2.5}$ SIL at any modeled receptor, the demonstration should proceed to the second stage, conducting a cumulative impact analysis.

II.5 Cumulative Impact Analysis

This section provides an overview of cumulative impact analyses for O_3 and $PM_{2.5}$ NAAQS, as well as $PM_{2.5}$ PSD increments compliance. The cumulative impact analysis is illustrated in Figure II-1 and Figure II-2 and further explained in this guidance.

II.5.1 O_3 and $PM_{2.5}$ NAAQS Compliance

For either O_3 or $PM_{2.5}$, where the source impact analysis described in Section II.4 is insufficient to show that a proposed new or modifying PSD source will not cause or contribute to a violation of the respective NAAQS, a cumulative impact analysis is then necessary to make the required NAAQS demonstration, as described in section 9.2.3 of the 2017 *Guideline*. A cumulative impact analysis should account for the combined impacts of the following:

1. All direct and precursor emissions of a pollutant (*i.e.*, O_3 or $PM_{2.5}$) from the new or modifying source if the source would emit any direct or precursor emissions of the pollutant in a significant amount;[18]
2. Direct emissions from nearby sources (for primary $PM_{2.5}$ impacts only), as appropriate; and
3. Monitored background levels or concentrations that account for secondary impacts from regional background sources, secondary impacts from precursor emissions from nearby sources, and, in the case of primary $PM_{2.5,}$ $PM_{2.5}$ impacts from direct emissions from background sources, and nearby sources not explicitly modeled.[19]

Once the direct and precursor emissions impacts are taken into account, the estimated cumulative impact should then be compared to the NAAQS to determine if there is a modeled violation. If not, then the NAAQS compliance demonstration should be sufficient to show that the proposed source or modification will not cause or contribute to a violation. If there are predicted NAAQS violations, then the impacts of the direct and precursor emissions increases from the new or modifying source at those locations can be compared to the appropriate SIL to determine whether that increase will cause or contribute to the modeled violation of the NAAQS. Several aspects of the cumulative impact analysis for O_3 and $PM_{2.5}$ will be comparable to

[18] For a new major stationary source, this includes all direct and precursor pollutants if the source has the potential to emit any direct or precursor pollutant in an amount greater than or equal to the SER and for a modification to an existing major stationary source, it includes all direct and precursor pollutants, if the modification would result in a significant emissions increase and a significant net emissions increase of any direct or precursor pollutant.

[19] The emissions impact of any nearby source that has received a permit but is not yet operational should be included in the air quality assessment. In such cases, consultation with the appropriate permitting authority on the appropriate assessment approach is recommended. Consideration should also be given to the potential for some double-counting of the impacts from modeled emissions that may be also included in the background monitored concentrations.

analyses conducted for other criteria pollutants, while other aspects will differ due to the issues identified earlier.

II.5.2 $PM_{2.5}$ PSD Increments Compliance

For $PM_{2.5}$, where the source impact analysis described in Section II.4 is insufficient to show that a source will not cause or contribute to a violation of any $PM_{2.5}$ PSD increment, a cumulative impact analysis is necessary to make the PSD increment demonstration, as described in section 9.2.3 of the 2017 *Guideline*. A cumulative impact analysis for an increment differs from the NAAQS cumulative impact analysis in that the increment assessment only accounts for the combined impact of the new or modifying source's emissions increase and certain previous emissions changes from sources (including the modifying source) that affect the PSD increment under the EPA's PSD regulations. A more complete description of the types of emissions that affect increment consumption and other aspects of the PSD increment system is contained in Section V.1 of this guidance document. The cumulative impacts are then compared to the appropriate $PM_{2.5}$ PSD increments to determine whether the new or modifying source emissions will cause or contribute to a violation of any $PM_{2.5}$ PSD increment. The cumulative analysis for $PM_{2.5}$ PSD increments is described in greater detail in Section V.3.2.

For $PM_{2.5}$ PSD increments, since the requirement for calculating the amount of increment consumed was established relatively recently in comparison to the increments for other pollutants, a new or modified source being evaluated for $PM_{2.5}$ PSD increments compliance may still find that it is the first source, or one of only a few sources, with increment-consuming emissions in a particular attainment or unclassifiable area. As shown in Figure II-2, for such situations, a permitting authority may have sufficient reason (based on the approach for

conducting source impact analysis described below) to conclude that the impacts of the new or modified source may be compared directly to the allowable increments, without the need for a cumulative modeling analysis. This would be the case where it can be shown that any other increment-consuming sources in the same baseline area, if any, do not have much or any overlapping impact with the proposed new or modified source.[20]

Another important consideration for $PM_{2.5}$ PSD increments is the differences in the EPA recommended SIL values for Class I and Class II / III areas, as presented in Table II-2. Given substantially lower recommended SIL values for Class I areas, there is a greater likelihood that a proposed new or modifying source would have a predicted impact that equals or exceeds an EPA recommended SIL for $PM_{2.5}$ PSD increments in a Class I area, even at distances beyond the nominal 50 km near-field application distance. Section 4.2 of the 2017 *Guideline* provides screening and compliance assessment approaches for near-field (50 km or less) and long-range transport (beyond 50 km) situations. The MERPs Guidance (*i.e.*, Tier 1 Assessment Approach) and the Single-source Modeling Guidance (*i.e.*, Tier 2 Assessment Approach) should be referenced for assessing secondary $PM_{2.5}$ impacts. There is also distance-weighted empirical relationship information (*i.e.*, precursor contributions to secondary impacts by distance from source) provided within the MERPs Guidance that may be particularly useful for assessing secondary $PM_{2.5}$ impacts in long-range transport situations. Consultation with the appropriate permitting authority and the appropriate EPA Regional Office is highly recommended for any permit applicants demonstrating long-range Class I area increment compliance per the requirements of section 4.2.c.ii of the 2017 *Guideline*.

[20] The term "increment-consuming source," as used in this guidance, is intended to refer to any type of source whose emissions changes (increases or decreases) affects the amount of increment consumed or expanded.

III. PSD Compliance Demonstrations for the O_3 and $PM_{2.5}$ NAAQS: Source Impact Analysis

This section provides details regarding the EPA's recommended approaches for conducting the source impact analysis as part of a PSD compliance demonstration for the O_3 and/or $PM_{2.5}$ NAAQS.

III.1 O_3 NAAQS

This section provides details regarding the EPA's recommended approaches for conducting the source impact analysis for the O_3 NAAQS associated with each of the two assessment cases presented in Table III-1. In each of the assessment cases, the analysis should begin by evaluating whether the impacts of either O_3 precursor (VOC or NO_X) would be emitted in a significant amount, *i.e.*, equal to or greater than the respective SER (40 tpy).

Table III-1. EPA Recommended Approaches for Assessing O_3 Impacts by Assessment Case

Assessment Case	Description of Assessment Case		Secondary Impacts Approach*
Case 1: No Air Quality Analysis	NO_X emissions and VOC emissions < 40 tpy SER		N/A
Case 2*: Secondary Air Quality Impacts	NO_X emissions or VOC emissions ≥ 40 tpy SER		Include both precursors of O_3, see Section II.2. • **Tier 1 Approach** (*e.g.*, MERPs) • **Tier 2 Approach** (*e.g.*, Chemical Transport Modeling)
* In unique situations (*e.g.*, in parts of Alaska where photochemistry is not possible for portions of the year), it may be acceptable for the applicant to rely upon a qualitative approach to assess the secondary impacts. Any qualitative assessments should be justified on a case-by-case basis in consultation with the appropriate permitting authority and the appropriate EPA Regional Office.			

For Case 1, a modeled O_3 NAAQS compliance demonstration is not required since neither O_3 precursor (NO_X or VOC) is proposed to be emitted in an amount equal to or greater than the applicable SER. For Case 2, where either NO_X or VOC precursor emissions are greater than the applicable SER, the permit applicant would need to conduct a compliance demonstration for secondary impacts for both O_3 precursors based on the two-tiered demonstration approach in the EPA's 2017 *Guideline*. Permit applicants are encouraged to consult with the appropriate permitting authority and Regional Office to avoid any unnecessary steps or overly conservative assumptions regarding any O_3 demonstrations.

III.2 $PM_{2.5}$ NAAQS

This section provides details regarding the EPA's recommended approaches for conducting the source impact analysis for the $PM_{2.5}$ NAAQS associated with each of the two assessment cases presented in Table III-2. In each of the assessment cases, the analysis should begin by evaluating whether direct $PM_{2.5}$would be emitted in a significant amount, *i.e.*, equal to or greater than the SER (10 tpy), or whether either precursor (NO_X or SO_2) would be emitted in a significant amount, *i.e.*, equal to or greater than the respective SER (40 tpy).

Table III-2. EPA Recommended Approaches for Assessing Primary and Secondary $PM_{2.5}$ Impacts by Assessment Case

Assessment Case	Description of Assessment Case		Primary Impacts Approach	Secondary Impacts Approach*
Case 1: No Air Quality Analysis	Direct $PM_{2.5}$ emissions < 10 tpy SER and NO_X emissions and SO_2 emissions < 40 tpy SER		N/A	N/A
Case 2*: Primary and Secondary Air Quality Impacts	Direct $PM_{2.5}$ emissions ≥ 10 tpy SER or NO_X emissions or SO_2 emissions ≥ 40 tpy SER		**Appendix W preferred or approved alternative dispersion model**	Include both precursors of $PM_{2.5}$, see Section II.2. • **Tier 1 Approach** (*e.g.*, MERPs) • **Tier 2 Approach** (*e.g.*, Chemical Transport Modeling)

* In unique situations (*e.g.*, in parts of Alaska where photochemistry is not possible for portions of the year), it may be acceptable for the applicant to rely upon a qualitative approach to assess the secondary impacts. Any qualitative assessments should be justified on a case-by-case basis in consultation with the appropriate EPA Regional Office or other applicable permitting authority.

A modeled $PM_{2.5}$ NAAQS compliance demonstration is not required for Case 1 since neither direct $PM_{2.5}$, nor any $PM_{2.5}$ precursor (NO_X or SO_2), is proposed to be emitted in an amount equal to or greater than the applicable SER. Case 1 is the only assessment case that does not require conducting a source impact analysis.

For Case 2, where direct $PM_{2.5}$ emissions or NO_X or SO_2 precursor emissions are greater than or equal to the applicable SER, the primary $PM_{2.5}$ impacts from direct $PM_{2.5}$ emissions can be estimated based on application of AERMOD or another appropriate preferred model listed in Appendix A of the 2017 *Guideline*, or an alternative model subject to the provisions of section 3.2 of the 2017 *Guideline*. However, AERMOD and other preferred models currently listed in Appendix A of the 2017 *Guideline* do not account for secondary formation of $PM_{2.5}$ associated with the source's precursor emissions. The assessment of NO_X and SO_2 precursor emission

impacts on secondary $PM_{2.5}$ formation should be conducted based on the two-tiered demonstration approach in EPA's 2017 *Guideline*. Permit applicants are encouraged to consult with the appropriate permitting authority and Regional Office to avoid any unnecessary steps or overly conservative assumptions regarding any secondary $PM_{2.5}$ formation demonstrations.

III.3 Assessing Primary $PM_{2.5}$ Impacts

The assessment of primary $PM_{2.5}$ impacts from the proposed new or modifying source is generally the same for the $PM_{2.5}$ NAAQS and PSD increments. Section 4.2.3.5 of the 2017 *Guideline* identifies the AERMOD modeling system as the preferred model for addressing direct $PM_{2.5}$ emissions unless another preferred model listed in the *Guideline* is more appropriate, such as the Offshore and Coastal Dispersion Model (OCD), or the use of an alternative model is justified consistent with section 3.2 of the 2017 *Guideline*.

The AERMOD modeling system includes the following regulatory components:

- AERMOD: the dispersion model (U.S. EPA, 2022a);
- AERMAP: the terrain processor for AERMOD (U.S. EPA, 2018b); and
- AERMET: the meteorological data processor for AERMOD (U.S. EPA, 2022b).

Other components that may be used, depending on the application, are:

- BPIPPRIME: the building input processor (U.S. EPA, 2004);
- AERSURFACE: the surface characteristics processor for AERMET (U.S. EPA, 2020);
- AERSCREEN: a screening version of AERMOD (U.S. EPA, 2021; U.S. EPA, 2011a); and
- AERMINUTE: a pre-processor to calculate hourly average winds from Automated Surface Observing System (ASOS) 2-minute observations (U.S. EPA, 2015).

Before applying AERMOD, the applicant should become familiar with the user's guides associated with the modeling components listed above and the most recent version of the AERMOD Implementation Guide (U.S. EPA, 2022c). In addition to these documents, detailed guidance on the use of the AERMOD modeling system for estimating primary $PM_{2.5}$ impacts is provided in Appendix B. Because AERMOD is limited to modeling direct $PM_{2.5}$ emissions, additional or alternative approaches are needed to provide an assessment of secondary $PM_{2.5}$ impacts from the proposed new or modifying source, as discussed in more detail in the following sections.

III.4 Assessing O_3 and Secondary $PM_{2.5}$ Impacts

This section provides more detail on the EPA's recommended approaches for assessing the impacts of precursor emissions on O_3 and/or secondary $PM_{2.5}$ formation.

III.4.1 Conceptual Model

Each NAAQS compliance demonstration is unique and may require multiple factors to be considered and assumptions to be thoroughly justified as a part of the technical assessment. A well-developed modeling protocol that includes a detailed conceptual description of the current air pollutant concentrations in the area (see Appendix A for examples of elements of a conceptual description) and of the nature of the emissions sources within proximity of the new or modifying emissions source is essential for determining the necessary components of an acceptable assessment of the impact from O_3 and/or secondary $PM_{2.5}$ formation.[21] The

[21] For more detailed information on the development of such conceptual descriptions for an area, please refer to the following:

development of this conceptual description and understanding does not need to be an onerous task and can build upon previous conceptual descriptions generated for other projects in the same region With timely and appropriate consultation between the applicant and the appropriate permitting authority, along with the submittal and subsequent approval, if required, of the modeling protocol by the appropriate permitting authority, many potential problems and unintended oversights in the technical assessment can be resolved early in the process or avoided all together.

In the development of an appropriate conceptual description to support an assessment, it is important to fully characterize the current O_3 and/or $PM_{2.5}$ concentrations in the region where the new or modifying source is to be located and not just the most current design values, which historically has been used as background concentrations in a cumulative modeling demonstration. For O_3, this characterization should take into consideration episodic high O_3 concentrations and any trends in the area. For $PM_{2.5}$, this characterization should take into consideration the seasonality and speciated composition of the current $PM_{2.5}$ concentrations and any long-term trends that may be occurring. It may also be important to describe the typical background concentrations of certain chemical species that participate in the photochemical reactions that form O_3 and secondary $PM_{2.5}$. It is possible that there are mitigating factors for

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Chapter 10 of "Particulate Matter Assessment for Policy Makers: A NARSTO Assessment." P. McMurry, M. Shepherd, and J. Vickery, eds. Cambridge University Press, Cambridge, England (NARSTO, 2004).

Section 11, "How Do I Get Started? 'A Conceptual Description'" of "Guidance on the Use of Models and Other Analyses for Demonstrating Attainment of Air Quality Goals for Ozone, $PM_{2.5}$, and Regional Haze." U.S. Environmental Protection Agency, Research Triangle Park, North Carolina (U.S. EPA, 2007a).

In addition, relevant regional examples include: "Conceptual Model of $PM_{2.5}$ Episodes in the Midwest," January 2009, Lake Michigan Air Directors Consortium; and "Conceptual Model of Particulate Matter Pollution in the California San Joaquin Valley," Document Number CP045-1-98, September 8, 1998.

secondary $PM_{2.5}$ formation given limitations of other chemical species important in the photochemical reactions, *e.g.*, minimal ammonia (NH_3) in the ambient environment that could limit any precursor pollutant from readily reacting to form secondary $PM_{2.5}$. This understanding of the atmospheric environment will provide important insights on the potential for secondary formation and highlight aspects that will need to be accounted for in the source impact and/or cumulative impact assessment.

A good conceptual description will also characterize the meteorological conditions that are representative of the region and are associated with periods and/or seasons of higher and lower ambient O_3 and/or 24-hour $PM_{2.5}$ concentrations. For example, identification of meteorological phenomena that typically occur during periods of high daily 8-hour O_3 or 24-hour $PM_{2.5}$ concentrations, such as low-level temperature inversions, stagnant high pressure systems, low-level jets, etc., can be extremely important in understanding the importance, or lack thereof, of photochemistry and secondary $PM_{2.5}$ formation for the higher ambient O_3 and $PM_{2.5}$ concentrations. The analysis and understanding of meteorological conditions will also inform the assessment of high O_3 episodes and seasonal 24-hour $PM_{2.5}$ concentrations in the region.

III.4.2 Tier 1 Assessment Approach

As discussed in the section 5.2 of the 2017 *Guideline*, the EPA has determined that advances in chemical transport modeling science make it reasonable to provide more specific, generally-applicable guidance that identifies particular models or analytical techniques that may be appropriate for use under specific circumstances for assessing the impacts of an individual proposed source on O_3 and secondary $PM_{2.5}$ concentrations. There is not a preferred model or technique for estimating O_3 or secondary $PM_{2.5}$ for specific source impacts. Instead, for assessing

secondary pollutant impacts from individual proposed sources, the degree of complexity required to appropriately assess potential single-source impacts varies depending on the nature of the source, its proposed emissions, and the background environment. In order to provide the user community flexibility in estimating single-source secondary pollutant impacts, which allows for different approaches to credibly address these different areas, the 2017 *Guideline* recommends a two-tiered demonstration approach for addressing single-source impacts on ambient concentrations of O_3 and secondary $PM_{2.5}$.

To inform a Tier 1 assessment,[22] the existing air quality model-based information that is used should be appropriate in terms of representing the type of source, its precursor emissions, its geographic location, and a current composition of regional emissions, in addition to those elements of the conceptual description discussed above. The air quality modeling information may be available from past or current SIP attainment demonstration modeling, published modeling studies, or peer-reviewed literature with estimates of model responsiveness to precursor emissions in contexts that are relevant to the new or modifying source. The estimates of model responsiveness, such as impact on O_3 concentrations per ton of NO_X or impact on $PM_{2.5}$ concentrations per ton of SO_2 emissions, could then be used in conjunction with the precursor emissions estimates for the proposed new or modifying source to provide a quantitative estimate of the impact of such precursor emissions on the formation of O_3 and/or secondary $PM_{2.5}$ concentrations. The estimates of responsiveness should be technically credible

[22] A Tier 1 assessment involves the use of technically credible relationships between precursor emissions and a source's secondary impacts, *e.g.*, as demonstrated in modeling for a source impact analysis, that may be published in the peer-reviewed literature, developed from modeling that was previously conducted for an area by a source, a governmental agency, or some other entity and that is deemed sufficient for evaluating a proposed source's impacts, or generated by a peer-reviewed reduced form model. In such cases, the EPA expects that existing air quality model-based information regarding the potential for NO_X and VOC precursor emissions to form O_3 and for SO_2 and NO_X precursor emissions to form secondary $PM_{2.5}$ concentrations may be used to establish an appropriate estimate of O_3 and/or secondary $PM_{2.5}$ impacts from the proposed new or modifying source.

in representing such impacts and it may be advisable for the estimate to reflect an upper bound of potential impacts.

To assist in the development of appropriate Tier 1 demonstration tools, the EPA developed the MERPs Guidance to provide a framework for permitting authorities to develop area-specific MERPs. The MERPs Guidance illustrates how permitting authorities may appropriately develop MERPs for specific areas and use them as a Tier 1 compliance demonstration tool for O_3 and secondary $PM_{2.5}$ under the PSD permitting program. The MERPs Guidance also addresses the appropriate use of MERPs to reflect the combined ambient impacts across O_3 or $PM_{2.5}$ precursors and, in the case of $PM_{2.5}$, the combined primary and secondary ambient impacts. Such an approach includes flexibility with respect to the use of Tier 1 demonstration tools to generate information relevant for specific regions or areas and representative of secondary formation in a particular region or area.

Specifically, the MERPs Guidance provides information about how to use CTMs to estimate single-source impacts on O_3 and secondary $PM_{2.5}$ and how such model simulation results for specific areas can be used to develop empirical relationships between a source's O_3 and $PM_{2.5}$ precursor emissions and its secondary impacts that may be appropriate for use as a Tier 1 demonstration tool. It also provides results from EPA photochemical modeling of a set of more than 100 hypothetical sources across geographic areas and source types that may be used in developing MERPs as discussed in the guidance. This flexible and scientifically credible approach allows for the development of area-specific Tier 1 demonstration tools that better represent the chemical and physical characteristics and secondary pollutant formation within that region or area.

As discussed in the MERPs Guidance, the EPA's Single-source Modeling Guidance

provides information to stakeholders about how to appropriately address the variety of chemical and physical characteristics regarding a project scenario and key receptor areas in conducting photochemical modeling to inform development of MERPs. The development of MERPs for O_3 and secondary $PM_{2.5}$ precursors is just one example of a suitable Tier 1 demonstration tool. The EPA will continue to engage with the modeling community to identify credible alternative approaches for estimating single-source secondary pollutant impacts, which provide flexibility and are less resource intensive for PSD permit demonstrations.

As an example, a Tier 1 assessment of secondary O_3 and $PM_{2.5}$ impacts was developed by a permit applicant, the Tennessee Valley Authority (TVA), for a major modification at their Gleason facility in Tennessee in 2018. The TVA and the Tennessee Department of Environment and Conservation (TDEC) worked closely with EPA Region 4 to ensure that the ambient impacts analysis was technically sound and consistent with applicable PSD regulations and EPA guidance. The PSD air quality modeling analysis was submitted to TDEC in late 2018 using an approach that was consistent with the MERPs Guidance to relate facility emissions to potential downwind impacts of secondary O_3 and $PM_{2.5}$. A more detailed discussion of the TVA's technical assessment is provided in Appendix C.

The National Association of Clean Air Agencies (NACAA) Workgroup final report (NACAA, 2011) provides details on potential approaches to quantify the secondary $PM_{2.5}$ impacts from a proposed new or modifying source that may be appropriate to inform a Tier 1 assessment of $PM_{2.5}$ impacts (see Appendices C and D of NACAA, 2011). One suggested method in the final report is to convert emissions of precursors into equivalent amounts of direct $PM_{2.5}$ emissions using "pollutant offset ratios" and then use a dispersion model to assess the impacts of the combination of direct $PM_{2.5}$ emissions and the equivalent direct $PM_{2.5}$ emissions.

The "pollutant offset ratios" referenced in the NACAA Workgroup report were from the EPA's 2008 "Implementation of the New Source Review (NSR) Program for Particulate Matter Less Than 2.5 Micrometers ($PM_{2.5}$)" final rule notice (73 Fed. Reg. 28321, May 16, 2008) concerning the development and adoption of interpollutant trading (offset) provisions for $PM_{2.5}$ under state nonattainment area NSR programs for $PM_{2.5}$. The EPA's July 23, 2007, technical analysis titled "Details on Technical Assessment to Develop Interpollutant Trading Ratios for $PM_{2.5}$ Offsets" describes the method used to develop the original "preferred" precursor offset ratios (U.S. EPA, 2007b).[23]

The EPA does not support using the specific results from the EPA's 2007 technical assessment in the context of PSD compliance demonstrations without additional technical demonstration specific to the source(s) and area(s) for which the ratios would be applied. As described in the EPA's July 21, 2011 memorandum changing its policy on use of the "preferred" interpollutant offset trading ratios included in the preamble to the 2008 final rule, the EPA acknowledged that existing models and techniques are adequate to "conduct local demonstrations leading to the development of area-specific ratios for $PM_{2.5}$ nonattainment areas" and provided a general framework for efforts that may be relevant in developing appropriate "pollutant offset ratios" for use in hybrid qualitative/quantitative assessment of secondary $PM_{2.5}$ impacts (U.S. EPA, 2011b). A similar general framework is embodied in the MERPs Guidance in which the EPA addresses how to conduct modeling to inform the development of a MERP for

[23] In the preamble to the 2008 final rule, the EPA included preferred or presumptive offset ratios, applicable to specific $PM_{2.5}$ precursors that the EPA said at that time state/local air agencies could adopt in conjunction with the new interpollutant offset provisions for $PM_{2.5}$, and for which the state could rely on the EPA's technical work to demonstrate the adequacy of the ratios for use in any $PM_{2.5}$ nonattainment area. In a July 21, 2011 memorandum, EPA changed its policy and stated that it no longer supported the ratios provided in the preamble to the 2008 final rule as presumptively approvable ratios for adoption in SIPs containing nonattainment NSR programs for $PM_{2.5}$. Memorandum from Gina McCarthy, Assistant Administrator, to Regional Air Division Directors, "Revised Policy to Address Reconsideration of Interpollutant Trading Provisions for Fine Particles ($PM_{2.5}$)" (U.S. EPA, 2011b).

a particular area.

The EPA also notes that the NACAA Workgroup "considered, but rejected, other methods for assessing secondary $PM_{2.5}$ impacts, including use of a simple emissions divided by distance (Q/D) metric and use of AERMOD with 100 percent conversion of SO_2 and NO_X concentrations to $(NH_4)_2SO_4$ and $(NH_4)NO_3$." The EPA has reviewed the detailed discussion provided in Appendix E of the NACAA Workgroup final report and agrees with these technical conclusions.

III.4.3 Tier 2 Assessment Approach

As discussed in the 2017 *Guideline*, a Tier 2 assessment involves application of more sophisticated, case-specific CTMs in consultation with the appropriate permitting authority and conducted consistent with the recommendations in the most current version of the Single-source Modeling Guidance. Where it is necessary to estimate O_3 and/or secondary $PM_{2.5}$ impacts with case-specific air quality modeling, a candidate model should be selected for estimating single-source impacts on O_3 and/or secondarily formed $PM_{2.5}$ that meets the general criteria for an "alternative model" where there is no preferred model as outlined in section 3.2.2.e of the 2017 *Guideline*. The general criteria include:

i. The model has received a scientific peer review;

ii. The model can be demonstrated to be applicable to the problem on a theoretical basis;

iii. The databases that are necessary to perform the analysis are available and adequate;

iv. Appropriate performance evaluations of the model have shown that the model is not biased toward underestimates; and

iv. A protocol on methods and procedures to be followed has been established.

Section 3.2.2 further provides that the appropriate EPA Regional Office, in consultation with the EPA Model Clearinghouse, is authorized to approve a particular model and approach as an alternative model application.

Both Lagrangian puff models and photochemical grid models may be appropriate for this purpose where those models satisfy alternative model criteria in section 3.2.2 of the 2017 *Guideline*. That said, the EPA believes photochemical grid models are generally most appropriate for addressing O_3 and secondary $PM_{2.5}$ impacts because they provide a spatially and temporally dynamic realistic chemical and physical environment for plume growth and chemical transformation. Publicly available and documented Eulerian photochemical grid models such as the Comprehensive Air Quality Model with Extensions (CAMx) (Ramboll Environ, 2018) and the Community Multiscale Air Quality (CMAQ) (Byun and Schere, 2006) model treat emissions, chemical transformation, transport, and deposition using time and space variant meteorology. These modeling systems include primarily emitted species and secondarily formed pollutants such as O_3 and $PM_{2.5}$ (Chen et al., 2014; Civerolo et al., 2010; Russell, 2008; Tesche et al., 2006). In addition, these models have been used extensively to support O_3 and $PM_{2.5}$ SIPs and to explore relationships between inputs and air quality impacts in the United States and elsewhere (Cai et al., 2011; Civerolo et al., 2010; Hogrefe et al., 2011).

On August 4, 2017, the EPA released a memorandum (U.S. EPA, 2017b) providing information specific to how the CAMx and the CMAQ model systems were relevant for each of these elements. This memorandum provides an alternative model demonstration for the CAMx

and CMAQ photochemical transports models establishing their fit for purpose in PSD compliance demonstrations for O_3 and $PM_{2.5}$ and in NAAQS attainment demonstrations for O_3, $PM_{2.5}$ and Regional Haze. The memorandum also provides support for their general applicability for use in PSD compliance demonstrations; however, it does not replace the need for such demonstrations to provide model protocols describing model application choices or the evaluation of model inputs and baseline predictions against measurements relevant for their specific use by permit applicants and state, local, and tribal air agencies.

For those situations where a refined Tier 2 demonstration is necessary, the EPA has also provided the Single-source Modeling Guidance that provides recommended, credible procedures to estimate single-source secondary impacts from sources for permit related assessments. Extensive peer-reviewed literature demonstrates and documents that photochemical grid models have been applied for assessing single-source impacts and that the models adequately represent secondary pollutant impacts from a specific facility, in comparison to near-source downwind in-plume measurements. The literature shows that these models can clearly differentiate impacts of a specific facility from those of other sources (Baker and Kelly, 2014; Zhou et al., 2012). Other peer-reviewed research has clearly shown that photochemical grid models are able to simulate impacts from single sources on secondarily-formed pollutants (Baker et al., 2015; Bergin et al., 2008; Kelly et al., 2015). Further, single-source secondary impacts have been provided in technical reports that further support the utility of these tools for single-source scientific and regulatory assessments (ENVIRON 2012a; ENVIRON 2012b; Yarwood et al., 2011). The EPA firmly believes that the peer-reviewed science clearly demonstrates that photochemical grid models can adequately assess single-source impacts. The EPA recognizes that ongoing

evaluations in this area will lead to continual improvements in science and associated predictive capabilities of these models.

For the purposes of conducting a Tier 2 assessment, the application of a CTM will involve case-specific factors that should be part of the consultation process with the appropriate permitting authority and reflected in the agreed-upon modeling protocol. Consistent with the Single-source Modeling Guidance and section 9.2.1 of the 2017 *Guideline*, the EPA recommends that the modeling protocols for this purpose should include the following elements:

1. Overview of Modeling/Analysis Project
    - Participating organizations
    - Schedule for completion of the project
    - Description of the conceptual model for the project source/receptor area
    - Identify how modeling and other analyses will be archived and documented
    - Identify specific deliverables to the appropriate permitting authority
2. Model and Modeling Inputs
    - Rationale for the selection of air quality, meteorological, and emissions models
    - Modeling domain
    - Horizontal and vertical resolution
    - Specification of initial and boundary conditions
    - Episode selection and rationale for episode selection
    - Rationale for and description of meteorological model setup
    - Basis for and development of emissions inputs
    - Methods used to quality assure emissions, meteorological, and other model inputs
3. Model Performance Evaluation

- Describe ambient database(s)
- Describe evaluation procedures and performance metrics

As stated previously, the EPA expects that the EPA Regional Offices, with assistance from the OAQPS, may assist reviewing authorities, as necessary, to structure appropriate technical demonstrations leading to the development of appropriate CTM applications for the purposes of estimating potential O_3 and/or secondary $PM_{2.5}$ impacts.

III.5 Comparison to the SIL

This section provides recommendations for source impact analyses where a permit applicant compares the proposed source's ambient O_3 or $PM_{2.5}$ impacts to an appropriate SIL as part of the required demonstration that a proposed source or modification will not cause or contribute to a violation of the O_3 or $PM_{2.5}$ NAAQS. These recommendations are also generally applicable for demonstrations that a proposed source or modification will not cause or contribute to a violation of the $PM_{2.5}$ PSD increments, see Section V.4. The EPA's recommended SIL values for O_3 and $PM_{2.5}$ NAAQS and $PM_{2.5}$ PSD increments are listed in Table II-1 and Table II-2. (U.S. EPA, 2018a).

III.5.1 SIL Comparison for O_3

For Assessment Case 2, an analysis of secondary O_3 impacts should be conducted where the proposed source's precursor emissions of NO_X or VOC are equal to or greater than the respective SERs. The EPA recommends that the assessment of the combined precursor emissions impacts on O_3 formation be conducted based on the two-tiered demonstration approach specific to O_3 in section 5.3 of the 2017 *Guideline*. Under the Tier 1 approach, for source impact

analyses, the highest of the multi-season (or episode) averages of the maximum modeled daily 8-hour O_3 concentrations predicted each season (or episode) at each grid cell or location should be compared to the appropriate O_3 SIL, since this metric represents the maximum potential daily 8-hour O_3 impact from the proposed source or modification. A source impact analysis applied consistently with the MERPs Guidance is also an acceptable Tier 1 approach. Under the Tier 2 approach, where a CTM is directly applied to estimate the source impacts, the comparison should be done at each receptor, *i.e.*, each modeled grid cell. If the source impact is less than the SIL, then the source impact analysis is generally sufficient to support a finding that the source will not cause or contribute to a NAAQS violation. However, if the source impact is equal to or greater than the SIL, then the analysis is insufficient to show that a source will not cause or contribute to a violation of the NAAQS and a cumulative impact assessment is necessary.

III.5.2 SIL Comparison for $PM_{2.5}$

For Assessment Case 2, analyses of both primary and secondary $PM_{2.5}$ impacts are necessary because the proposed source's direct $PM_{2.5}$ emissions or emissions of at least one $PM_{2.5}$ precursor are equal to or greater than the respective SERs. In this case, the combined primary and secondary $PM_{2.5}$ impacts from the proposed source or modification should be included in the comparison to the appropriate $PM_{2.5}$ SIL in the source impact analysis.

The assessment of the primary $PM_{2.5}$ concentrations due to direct emissions should be conducted using the EPA preferred AERMOD dispersion model (or other acceptable preferred or approved alternative model). The dispersion modeling methods here are similar to the methods used for other primary pollutants, including the use of maximum allowable emissions, following Table 8-2 of the 2017 *Guideline*. However, due to the form of the $PM_{2.5}$ NAAQS, the EPA

recommends that one of the following be included in the combined $PM_{2.5}$ SIL comparison for the source impact analysis, depending on the meteorological data used in the analysis:

- The highest of the 5-year averages of the maximum modeled annual 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or highest of the 5-year averages of the annual average $PM_{2.5}$ concentrations (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 5 years of representative National Weather Service (NWS) data;
- The highest modeled 24-hour $PM_{2.5}$ concentration (for the 24-hour $PM_{2.5}$ NAAQS) or the highest modeled average $PM_{2.5}$ concentration (for the annual $PM_{2.5}$ NAAQS) predicted at each receptor based on 1 year of site-specific meteorological data; or the highest of the multi-year averages of the maximum modeled annual 24-hour $PM_{2.5}$ concentration (for the 24-hour $PM_{2.5}$ NAAQS) or the highest of the multi-year averages of the maximum modeled annual average $PM_{2.5}$ concentrations (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 2 or more years, up to 5 complete years, of available site-specific meteorological data; or
- The highest of the 3-year averages of the maximum modeled annual 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or highest of the 3-year averages of the annual average $PM_{2.5}$ concentrations (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 3 years of prognostic meteorological data.

These metrics represent the maximum potential 24-hour or annual $PM_{2.5}$ impacts from the proposed source or modification at any receptor, given the form of the NAAQS, and therefore provide an appropriate part of the basis for determining whether a cumulative modeling analysis would be needed.

For the assessment of the precursor emission impacts on $PM_{2.5}$ formation, the EPA recommends that this part of the assessment be conducted based on the two-tiered demonstration approach specific to $PM_{2.5}$ in section 5.4 of the 2017 *Guideline*. The MERPs Guidance is available to assist with the secondary $PM_{2.5}$ impact aspects of a Tier 1 approach; whereas a Tier 2 approach would directly apply a CTM to estimate the source secondary $PM_{2.5}$ impacts. The resulting combined primary and secondary $PM_{2.5}$ impact included in the comparison to the appropriate $PM_{2.5}$ SIL will depend on the type of assessment conducted for the secondary $PM_{2.5}$ impacts from the source.

In the SIL comparison for Case 2, the primary and secondary $PM_{2.5}$ impacts may be combined in various ways that may entail greater or lesser degrees of conservatism. For example, combining the peak estimated primary $PM_{2.5}$ impact with the peak estimated secondary $PM_{2.5}$ impact, unpaired in time and space, would tend to be a conservative estimate of combined impacts since, as noted above, peak impacts associated with a source's direct $PM_{2.5}$ and precursor emissions are not likely well-correlated in time or space. The conservatism associated with combining peak estimated primary and secondary impacts for comparison to a SIL makes this an appropriate initial approach to combining estimated primary and secondary $PM_{2.5}$ impacts.

Other approaches for combining primary and secondary $PM_{2.5}$ impacts for comparison to a SIL will vary based on the degree of temporal and spatial pairing of estimated primary and secondary $PM_{2.5}$ impacts. Full temporal and spatial pairing may not be feasible in many cases, given that the dispersion modeling and chemical transport modeling may be based on different data periods. Furthermore, full temporal and spatial pairing of primary and secondary $PM_{2.5}$ impacts may not be appropriate in many cases because photochemical grid modeling represents

gridded concentration estimates whereas dispersion modeling produces estimates at discrete receptor locations and because of the limitations of both the dispersion model and the photochemical grid model to accurately predict impacts on a paired in time and space basis. As a result, consideration of some degree of temporal pairing of primary and secondary $PM_{2.5}$ impacts is most appropriate on a seasonal or monthly basis with considerations of spatial pairing that reflects the general lack of correlation between primary and secondary impacts, *i.e.*, primary impacts being higher near the source while secondary impacts being higher at some distance away from the source.

The permitting authority and the permit applicant should thoroughly discuss the details regarding combining modeled primary and secondary $PM_{2.5}$ impacts for Case 2 situations and should reach agreement during the initial review of the modeling protocol. The permitting authority should ensure that any approach for combining estimated primary and secondary $PM_{2.5}$ impacts for comparison to a SIL for Case 2 conforms to the recommendations described above regarding the form of the modeled estimate. Accordingly, the approach should be based on the highest of the multi-year averages of the maximum modeled 24-hour or annual $PM_{2.5}$ concentrations predicted each year at each receptor, which represents the maximum potential impact from the proposed source or modification.

Ultimately, if the combined primary and secondary $PM_{2.5}$ impacts are less than the SIL, then the analysis is generally sufficient to support a finding that the source will not cause or contribute to a NAAQS violation. However, if the combined primary and secondary $PM_{2.5}$ impacts are equal to or greater than the SIL, then the analysis is insufficient to show that a source will not cause or contribute to a violation of the NAAQS and a cumulative impact assessment is necessary to make the NAAQS compliance demonstration.

IV. PSD Compliance Demonstrations for the O_3 and $PM_{2.5}$ NAAQS: Cumulative Impact Analysis

Where the source impact analysis described in Section III is insufficient to show that a source will not cause or contribute to a violation of the O_3 or $PM_{2.5}$ NAAQS, a cumulative impact assessment is necessary to make the NAAQS compliance demonstration. A cumulative assessment accounts for the combined impacts of the proposed new or modifying source's emissions, emissions from other nearby sources, and representative background levels of O_3 or $PM_{2.5}$ within the modeling domain. The cumulative impacts are then compared to the O_3 or $PM_{2.5}$ NAAQS to determine whether there is a modeled NAAQS violation. If not, then the NAAQS compliance demonstration is sufficient. If there are modeled violations, then the source impact at the location of these predicted violations is compared to the appropriate SIL to determine if the proposed new or modifying source emissions will cause or contribute to a violation of the NAAQS. This section provides details on conducting an appropriate cumulative impact assessment for the O_3 and $PM_{2.5}$ NAAQS.

O_3

The cumulative impact assessment should include the following components of O_3 impacts, as appropriate, for comparison to the NAAQS:

- Proposed new or modifying source
    - Impacts on O_3 from each precursor (NO_X and VOC)
- Nearby sources
    - Impacts on O_3 from precursors (NO_X and VOC) are typically accounted

for through representative monitored background[24]

- Monitored background concentrations of O_3 that accounts for O_3 impacts from regional transport and from nearby sources, and O_3 impacts from background sources not included in the modeled inventory, *e.g.*, minor and mobile sources.

$PM_{2.5}$

The cumulative impact assessment should include the following components of $PM_{2.5}$ impacts, as appropriate, for comparison to the NAAQS:

- Proposed new or modifying source
    - Primary impacts on $PM_{2.5}$, *i.e.*, from direct $PM_{2.5}$ emissions
    - Secondary impacts on $PM_{2.5}$ from each precursor (NO_X and SO_2)
- Nearby sources
    - Primary impacts on $PM_{2.5}$[25]
    - Impacts on $PM_{2.5}$ from precursors (NO_X and SO_2) are typically accounted for through representative monitored background
- Monitored background concentrations of $PM_{2.5}$ that accounts for secondary $PM_{2.5}$ impacts from regional transport and from nearby sources, and primary $PM_{2.5}$ impacts from background sources not included in the modeled inventory, *e.g.*, minor sources.

[24] The emissions impact of any nearby source that has received a permit but is not yet operational should be included in the air quality assessment. In such cases, consultation with the appropriate permitting authority on the appropriate assessment approach is recommended.

[25] The emissions impact of any nearby source that has received a permit but is not yet operational should be included in the air quality assessment. In such cases, consultation with the appropriate permitting authority on the appropriate assessment approach is recommended

As with the source impact analysis, the primary impacts of direct $PM_{2.5}$ emissions from the proposed new or modifying source and nearby sources in a cumulative impact analysis should be estimated based on the AERMOD dispersion model (or other acceptable preferred or approved alternative model). In addition, EPA recommends that the estimate of secondary $PM_{2.5}$ impacts from the proposed new or modifying source be conducted based on the two-tiered demonstration approach described in section 5.2 of the 2017 *Guideline*. As noted above, secondary impacts on $PM_{2.5}$ from regional transport, precursor emissions from nearby sources, and primary $PM_{2.5}$ impacts from background sources not included in the modeled inventory should be accounted for through representative monitored background concentrations.

IV.1 Modeling Inventory

Section 8 of the 2017 *Guideline* provides the current required and recommended approaches for characterizing source emissions and developing the O_3 and/or $PM_{2.5}$ modeling inventory for purposes of NAAQS compliance modeling in PSD air quality assessments. Section 8.2 and Table 8-2 of the 2017 *Guideline* address the appropriate emissions limit, operating level, and operating factor to be modeled, which is the maximum allowable emissions rate for the proposed new or modifying source in most cases and an allowable emissions rate adjusted for actual operations for any nearby sources. For applications that require the assessment of secondarily formed O_3 or $PM_{2.5}$ through a case-specific CTM, information regarding the development of the appropriate modeling inventory can be found in the Single-source Modeling Guidance.

Section 8.3.3 of the 2017 *Guideline* emphasizes the importance of professional judgment in the identification of nearby and other sources "that are not adequately represented by ambient

monitoring data" that should be included in the modeled emission inventory and identifies "a significant concentration gradient in the vicinity of the [proposed] source" as a primary criterion for this selection. Additionally, the 2017 *Guideline* suggests that "the number of nearby sources to be explicitly modeled in the air quality analysis is expected to be few except in unusual situations" and that "[i]n most cases, the few nearby sources will be located within the first 10 to 20 km from the [proposed] source." The EPA also provided modeling guidance in March 2011 (U.S. EPA, 2011c) that includes a detailed discussion of the significant concentration gradient criterion. However, several application-specific factors should be considered when determining the appropriate inventory of nearby sources to include in the cumulative modeling analysis, including the potential influence of terrain characteristics on concentration gradients and the availability and adequacy of ambient monitoring data to account for impacts from nearby sources as well as other background sources.

Consistent with the 2017 revisions to the *Guideline*, the EPA cautions against the application of very prescriptive procedures for identifying which nearby sources should be included in the modeled emission inventory for NAAQS compliance demonstrations, such as the procedures described in Chapter C, Section IV.C.1 of the draft "New Source Review Workshop Manual" (U.S. EPA, 1990). Our main concern is that following such procedures in a literal and uncritical manner may, in many cases, increase the likelihood of double-counting modeled and monitored concentrations, resulting in cumulative impact assessments that are overly conservative and would unnecessarily complicate the permitting process. The identification of which sources to include in the modeled emissions inventory should be addressed in the modeling protocol and, as necessary, discussed in advance with the permitting authority.

Since modeling of direct $PM_{2.5}$ emissions has been limited and infrequent, the availability

of an adequate direct $PM_{2.5}$ emission inventory for nearby sources may not exist in all cases. Recommendations for developing $PM_{2.5}$ emission inventories for use in PSD applications will be addressed separately, but existing SIP inventories for $PM_{2.5}$ or statewide PSD inventories of sources for refined modeling are expected to provide a useful starting point for this effort.

IV.2 Monitored Background

Section 8.3 of the 2017 *Guideline* provides recommendations for determination of monitored background concentrations to include in cumulative impact assessments for NAAQS compliance, which should account for impacts from existing sources that are not explicitly included in the modeled inventory and natural sources. From newly-acquired, pre-construction monitoring data and/or existing representative air quality data gathered for purposes of a permitting analysis, permit applicants should assess and document what the background monitoring data represent to the extent possible, including any information that may be available from the state or other agency responsible for siting and maintaining the monitor.[26]

Determining the monitored background concentrations of O_3 and/or $PM_{2.5}$ to include in the cumulative impact assessment may entail different considerations from those for other criteria pollutants lacking secondary formation. Given that the monitored background determination can be a complex process with many uncertainties based on unique situations, permit applicants are encouraged to consult with the appropriate permitting authority.

[26] Please note that in the case of an existing source seeking a permit for a modification, there is potential overlap across secondary impacts from monitored background and from precursor emissions from the existing source. In such cases, recommendations for excluding monitored values when the source in question is impacting the monitor in section 8.3.2.c of the 2017 *Guideline* may need to be modified to avoid overcompensating when the monitored concentrations are also intended to account for the existing source's impacts on secondary $PM_{2.5}$. Additionally, permit applicants should consult with the appropriate permitting authority.

An important aspect of the monitored background concentrations for O_3 or $PM_{2.5}$ is that the ambient monitoring data should in most cases account for the impact of secondary formation of either pollutant from precursor emissions of existing sources impacting the modeling domain. Due to the nature of O_3 and secondary $PM_{2.5}$, monitored background concentrations of O_3 and $PM_{2.5}$ are more likely to be homogeneous across the modeling domain in most cases compared to most other pollutants. Additionally, for $PM_{2.5}$, ambient monitoring data should account for the component of the background levels of primary $PM_{2.5}$ from direct $PM_{2.5}$ emissions of nearby sources that are not included in the modeled inventory. As with other criteria pollutants, consideration should also be given to the potential for some double-counting of the impacts from modeled emissions that may be also included in the background monitored concentrations. This should generally be of less importance than the representativeness of the monitor for secondary formation of O_3 and $PM_{2.5}$, unless the monitor is located relatively close to nearby sources of primary $PM_{2.5}$ that could be impacting the monitor.

Depending on the nature of local $PM_{2.5}$ levels within the modeling domain, it may be appropriate to account for seasonal variations in monitored background $PM_{2.5}$ levels, which may not be correlated with seasonal patterns of the modeled primary $PM_{2.5}$ levels. For example, maximum modeled primary $PM_{2.5}$ impacts associated with low-level emission sources are likely to occur during winter months due to longer periods of stable atmospheric conditions, whereas maximum ambient levels of secondary $PM_{2.5}$ typically occur during spring and summer months due to high levels of sulfates (particularly in the eastern United States). The use of temporally-varying monitored background concentrations in a cumulative impact analysis is discussed in more detail in Section IV.3.

IV.3 Comparison to the NAAQS

As indicated in Figure II-1, the first step of a cumulative impact analysis consists of a comparison of the combined modeled and monitored concentrations, as discussed above, with the applicable NAAQS to determine if there are any predicted violations of the O_3 and/or $PM_{2.5}$ NAAQS.

O_3

Ozone differs from other criteria pollutants because it is secondarily formed by NOx and VOC precursor emissions and there are not direct O_3 emissions to be considered in the NAAQS compliance demonstration. The O_3 design value that is representative for the area, rather than the overall maximum monitored background concentration, should generally be used as the monitored component of the cumulative analysis. The O_3 design value is based on the 3-year average of the annual fourth-highest daily maximum 8-hour average O_3 concentrations (80 FR 65292).

The EPA recommends that the modeled O_3 impacts be added to the monitor-based design value for comparison to the NAAQS, as appropriate. The monitoring data should be representative in that it accounts for O_3 formation associated with existing sources both within and outside of the modeling domain. The EPA recommends that modeled O_3 impacts be based on a Tier 1 or 2 assessment that accounts for the source's precursor emissions of NOx and VOC. The modeled O_3 impacts should be based on the average of the predicted annual fourth-highest daily maximum 8-hour averaged O_3 concentrations. For episodic cases, consultation with the appropriate permitting authority is recommended to determine the most appropriate rank of the daily maximum 8-hour average O_3 concentration to use based on the length of the episode. The

resulting cumulative O_3 concentrations should then be compared to the O_3 NAAQS (0.070 ppm).

$PM_{2.5}$

Combining the modeled and monitored concentrations of $PM_{2.5}$ for comparison to the 24-hour or annual $PM_{2.5}$ NAAQS entails considerations that differ from those for other criteria pollutants due to the issues identified at the end of Section IV.2. The discussion below addresses comparisons to the NAAQS in the context of dispersion modeling of direct $PM_{2.5}$ emissions and a Tier 1 or 2 assessment of secondary $PM_{2.5}$ impacts accounting for the proposed source's $PM_{2.5}$ precursor emissions.

Given the importance of secondary formation of $PM_{2.5}$ and the potentially high background levels relative to the $PM_{2.5}$ NAAQS, greater emphasis should generally be placed on the monitored background concentrations relative to the modeled inventory for $PM_{2.5}$ than for other pollutants. This is true for both $PM_{2.5}$ NAAQS and PSD increments assessments. Also, given the probabilistic form of the $PM_{2.5}$ NAAQS, careful consideration should be given to how the monitored and modeled concentrations are combined to estimate the cumulative impact levels.

The $PM_{2.5}$ design value that is representative for the area, rather than the overall maximum monitored background concentration, should generally be used as the monitored component of the cumulative analysis. The $PM_{2.5}$ design value for the annual averaging period is based on the 3-year average of the annual average $PM_{2.5}$ concentrations, while the $PM_{2.5}$ design value for the 24-hour averaging period is based on the 3-year average of the annual 98^{th} percentile 24-hour average $PM_{2.5}$ concentrations (78 FR 3086). Details regarding the determination of the annual 98^{th} percentile monitored 24-hour value based on the number of days

sampled during the year are provided in the data interpretation procedures for the $PM_{2.5}$ NAAQS in Appendix N to 40 CFR part 50.

It should be noted here that, although the monitored design values for the $PM_{2.5}$ standards are defined in terms of 3-year averages, this definition does not preempt or alter the 2017 *Guideline's* requirement for use of 5 years of representative NWS meteorological data, at least 1 year of site-specific data, or at least 3 years of prognostic meteorological data for purposes of modeling direct emissions of $PM_{2.5}$.[27] The 5-year average based on use of representative NWS meteorological data, the average across one or more (up to 5) complete years of available site-specific data, or the average across 3 years of prognostic meteorological data serves as an unbiased estimate of the 3-year average for purposes of modeling demonstrations of compliance with the NAAQS. Modeling of "rolling 3-year averages," using years 1 through 3, years 2 through 4, and years 3 through 5, as recommended in the EPA's SIP Modeling Guidance, is not required.

The EPA recommends that the modeled design concentrations of primary $PM_{2.5}$ and the Tier 1 or 2 assessed secondary $PM_{2.5}$ impacts should be added to the monitor-based design value for comparison to the NAAQS, as appropriate. The primary $PM_{2.5}$ modeled design concentration should be based on:

- The 5-year average of the modeled annual 98^{th} percentile 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or 5-year average of the modeled annual average $PM_{2.5}$ concentration (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 5 years of representative NWS data;

[27] See 40 CFR part 51, Appendix W, section 8.4.2.e.

- The modeled 98th percentile 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or modeled average $PM_{2.5}$ concentration (for the annual $PM_{2.5}$ NAAQS) predicted at each receptor based on 1 year of site-specific meteorological data, or the multi-year average of the modeled annual 98th percentile 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or modeled annual average $PM_{2.5}$ concentration (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 2 or more years, up to 5 complete years, of available site-specific meteorological data; or
- The 3-year average of the modeled annual 98th percentile 24-hour $PM_{2.5}$ concentrations (for the 24-hour $PM_{2.5}$ NAAQS) or 3-year average of the modeled annual average $PM_{2.5}$ concentration (for the annual $PM_{2.5}$ NAAQS) predicted each year at each receptor, based on 3 years of prognostic meteorological data.

The EPA recommends that secondary $PM_{2.5}$ modeled impacts be based on either a Tier 1 or 2 assessment accounting for the source's $PM_{2.5}$ precursor emissions of NOx and SO_2. The resulting cumulative $PM_{2.5}$ concentrations should then be compared to the 24-hour $PM_{2.5}$ NAAQS (35 $\mu g/m^3$) and/or the annual $PM_{2.5}$ NAAQS (12 $\mu g/m^3$).

Specifically, the cumulative impact for comparison to the NAAQS should be based on the combined modeled design concentration for primary $PM_{2.5}$ impacts based on AERMOD (or other acceptable preferred or approved alternative model) estimates of the proposed source's and other nearby sources' direct $PM_{2.5}$ emissions, the modeled secondary $PM_{2.5}$ impacts (based on a Tier 1 or 2 assessment accounting for the proposed source's $PM_{2.5}$ precursor emissions), and the monitored design value. The monitor should be representative, in that it accounts for secondary $PM_{2.5}$ formation associated with existing sources both within and outside of the modeling

domain, in addition to the background levels of primary $PM_{2.5}$ associated with nearby and background sources that are not included in the modeled inventory.

The recommendations provided above constitute a First Level analysis for $PM_{2.5}$ NAAQS compliance demonstrations. For applications where impacts from direct $PM_{2.5}$ emissions are not temporally correlated with background $PM_{2.5}$ levels, combining the modeled and monitored levels as described above may be overly conservative in some situations. For example, there are areas of the country where background $PM_{2.5}$ levels are substantially higher on average during the summer months as compared to the winter months; however, the predicted impacts from the new or modified source may be substantially greater in the winter rather than in the summer. In such cases, a Second Level modeling analysis may be advisable to account for these temporal relationships. Such an analysis would involve combining the monitored and modeled $PM_{2.5}$ concentrations on a seasonal (or quarterly) basis, as appropriate. The use of a seasonally-varying monitored background component is likely to be a more important factor for the 24-hour $PM_{2.5}$ NAAQS analysis than for the annual $PM_{2.5}$ NAAQS. Careful evaluation of when model projections of $PM_{2.5}$ impacts and background $PM_{2.5}$ levels peak throughout the year is recommended before embarking on a Second Level modeling analysis. This is because the First Level approach may already adequately capture the temporal correlation. As a part of this process to determine the appropriate level of analysis, the permit applicant should consult with the appropriate permitting authority and then reflect the appropriate approach in their modeling protocol.

The AERMOD model provides several options for specifying the monitored background concentration for inclusion in the cumulative impact assessment. The options that are most relevant to $PM_{2.5}$ analyses include:

- For First Level 24-hour or annual $PM_{2.5}$ NAAQS analyses, an option to specify a single annual background concentration that is applied to each hour of the year, and
- For Second Level 24-hour $PM_{2.5}$ NAAQS analyses, an option to specify four seasonal background values that are combined with modeled concentrations on a seasonal basis.

The AERMOD model also allows the user to track the effect of background concentrations on the cumulative modeled design concentration.

For Second Level 24-hour $PM_{2.5}$ NAAQS modeling analyses, EPA recommends that the distribution of monitored data equal to and less than the annual 98th percentile be appropriately divided into seasons (or quarters) for each of the three years that are used to develop the monitored design value. This will result in data for each year of the multi-year data, which contains one season (or quarter) with the 98th percentile value and three seasons (quarters) with maximum values which are less than or equal to the 98th percentile value. The maximum concentration from each of the seasonal (or quarterly) subsets should then be averaged across these three years of monitoring data. The resulting average of seasonal (or quarterly) maximums should then be included as the four seasonal background values within the AERMOD model. Therefore, the monitored concentrations greater than the 98th percentile in each of the three years would not be included in the seasonal (or quarterly) subsets. These excluded monitored concentrations are the same values that are excluded when determining the monitored design value. An example of the calculations for a Second Level 24-hour $PM_{2.5}$ NAAQS modeling analysis is provided in Appendix D.

For a monitor with a daily (1-in-1 day monitor) sampling frequency and 100% data

completeness, the highest seven monitored concentrations for each year should be excluded from the seasonal (or quarterly) subdivided datasets. Similarly, for a monitor with every third day (1-in-3 day monitor) sampling frequency and 100% data completeness, the highest two monitored concentrations for each year should be excluded from the seasonal (or quarterly) subdivided datasets. The monitored concentrations excluded from the subdivided datasets could primarily come from one or two seasons (or quarters) each year or could be evenly distributed across all four seasons (or quarters) each year. Additionally, the monitored concentrations not included in the subdivided datasets could shift seasonally (or quarterly) from one year to the next. Given the reason for considering a Second Level 24-hour analysis (*i.e.*, lack of temporal correlation between modeled and monitored concentrations), it is likely that the monitored data greater than the 98^{th} percentile would be concentrated in one or two seasons as opposed to evenly distributed throughout the year. As mentioned earlier, see Appendix N of 40 CFR part 50 in determining the appropriate 98^{th} percentile rank of the monitored data based on the monitor sampling frequency and valid number of days sampled during each year.

The EPA does not recommend a "paired sums" approach on an hour-by-hour basis because of the spatial and temporal variability throughout a typical modeling domain on an hourly basis and the complexities and limitations of hourly observations from the current $PM_{2.5}$ ambient monitoring network. The implicit assumption underlying this “paired sums’ approach is that the background monitored levels for each hour are spatially uniform and that the monitored concentrations are fully representative of background levels at each receptor for each hour. Such an assumption does not account for the many factors that contribute to the temporal and spatial variability of ambient $PM_{2.5}$ concentrations across a typical modeling domain on an hourly

basis.[28] Furthermore, the pairing of daily monitored background and 24-hour average modeled concentrations is not recommended except in rare cases of relatively isolated sources where the available 1-in-1 day monitor can be shown to be representative of the ambient concentration levels in the areas of maximum impact from the proposed new or modifying source. In most cases, the seasonal (or quarterly) pairing of monitored and modeled concentrations previously described in the Second Level approach should sufficiently address situations in which the impacts from direct $PM_{2.5}$ emissions are not temporally correlated with background $PM_{2.5}$ levels. Any monitor-model pairing approach aside from the First or Second Level methods should be justified on a case-by-case basis in consultation with the appropriate permitting authority and the appropriate EPA Regional Office.

IV.4 Determining Whether Proposed Source Causes or Contributes to Modeled Violations

If the cumulative impact assessment following these recommendations results in predicted violations of the O_3 and/or $PM_{2.5}$ NAAQS, then the permit applicant will need to demonstrate that the proposed source's emissions do not cause or contribute to the modeled NAAQS violations. In the SILs Guidance, the EPA explained that the permitting authority may further evaluate whether the proposed source or modification will cause or contribute to

[28] The complexity of the $PM_{2.5}$ ambient monitoring network presents special challenges with a "paired sum" approach that are not present with other NAAQS pollutants. The Federal Reference Method (FRM) $PM_{2.5}$ monitoring network is based on 24-hour samples that are taken on average every third day at the 1-in-3 day monitors. The frequency of daily or 1-in-1 day $PM_{2.5}$ monitors is steadily increasing but is relatively limited to the largest cities and metropolitan regions of the U.S. Various methods to "data fill" the 1-in-3 day monitoring database to create a pseudo-daily dataset have been explored in a few situations, but none of these data filling methods have been demonstrated to create a representative daily $PM_{2.5}$ dataset that the EPA would consider acceptable for inclusion in a $PM_{2.5}$ NAAQS compliance demonstration. The use of continuous $PM_{2.5}$ monitors, which are more limited in number compared to the FRM monitors and may require careful quality assurance of individual hourly measurements, may be an option but should be discussed in advance with the appropriate permitting authority.

predicted violations by comparing the proposed source's modeled impacts, paired in time and space with the predicted violations, to an appropriate SIL. The proposed source or modification may be considered to not cause or contribute to predicted violations of the O_3 or $PM_{2.5}$ NAAQS where the modeled impacts of the proposed source or modification at those particular times and locations are less than the appropriate O_3 or $PM_{2.5}$ NAAQS SIL. As explained in the SILs Guidance, a permitting authority that chooses to use an O_3 or $PM_{2.5}$ SIL value to support a PSD permitting decision should justify the value and its use in the administrative record for the permitting action.

A demonstration that a proposed source or modification does not cause or contribute to a predicted violation should be based on a comparison of the modeled concentrations (primary and secondary impacts) at the receptor location(s) showing the violation(s) of the O_3 or $PM_{2.5}$ NAAQS to the appropriate O_3 or $PM_{2.5}$ NAAQS SIL. Considering the form of each NAAQS, the following approaches are recommended:

- For a predicted violation of the O_3 NAAQS, the average of the predicted annual (or episodic) fourth-highest daily maximum 8-hour averaged O_3 concentrations at the affected receptor(s) should be compared to an appropriate O_3 NAAQS SIL, *e.g.*, SIL values recommended by EPA in the SILs Guidance (Table II-1).
- For a predicted violation of the annual $PM_{2.5}$ NAAQS, the average of the predicted annual concentrations at the affected receptor(s) should be compared to an appropriate $PM_{2.5}$ annual NAAQS SIL, *e.g.*, SIL values recommended by EPA in the SILs Guidance (Table II.1).
- For a predicted violation of the 24-hour $PM_{2.5}$ NAAQS, the average of the predicted annual 98^{th} percentile 24-hour average concentrations at the affected

receptor(s) should be compared to an appropriate $PM_{2.5}$ 24-hour NAAQS SIL, *e.g.*, SIL values recommended by EPA in the SILs Guidance (Table II-1).

V. PSD Compliance Demonstration for the $PM_{2.5}$ Increments

As summarized in Section II of this guidance, CAA section 165(a)(3) requires that proposed new and modified major stationary sources seeking a PSD permit demonstrate that their proposed emissions increases will not cause or contribute to a violation of any NAAQS or PSD increment. Consistent with the flow diagram presented in Figure II-2, this section describes the EPA's recommendations for completing the required compliance demonstration for the PSD increments for $PM_{2.5}$.

V.1 Overview of the PSD Increment System

This section provides an overview of the PSD increment system by defining basic terms, such as increment, baseline concentration, baseline area, trigger date, minor source baseline date, and major source baseline date. This section also introduces and discusses the concepts of increment consumption and expansion.

V.1.1 PSD Increments and Baseline Concentration

The term "increment" generally refers to what the CAA calls the "maximum allowable increase over baseline concentrations" with respect to a criteria pollutant. CAA section 169(4) defines "baseline concentration," generally, as "the ambient concentration levels which exist at the time of the first application for a [PSD] permit for an area subject to this part…."[29] Accordingly, an increment analysis is generally concerned with the emissions increases affecting air quality in a particular PSD area after the date that the first complete PSD application is

[29] EPA's regulations at 40 CFR 52.21(b)(14)(ii) provide that the application that determines the baseline concentration is to be a complete PSD application. Hence, the term "complete application" will be used throughout this section with regard to the minor source baseline date and increment consumption.

submitted to the permitting authority.[30] When comparing the ambient impact of such total emissions increases against the increment value for a particular pollutant, a cumulative increase in the ambient concentration of that pollutant that is greater than the increment generally is considered "significant deterioration." When the cumulative impact analysis identifies significant deterioration in this way, the permitting authority should determine whether the emissions increase from the proposed new or modifying source will cause or contribute to the predicted violation of the PSD increment.

Based on the statutory definition of baseline concentration, as described above, it is conceptually possible to measure whether there will be significant deterioration in at least two separate ways. The first way involves comparing a direct modeled projection of the change in air quality caused by all increment-consuming and expanding emissions to the increment in the area of concern (known as the baseline area, discussed below in Section V.1.2). The second approach is to make a determination of whether the current monitored ambient air quality concentration in the applicable baseline area, supplemented by the modeled impact of the proposed source, will exceed an allowable ambient air quality ceiling. This latter approach requires comparing such monitored concentration(s) to the sum of the increment and the baseline concentration for the baseline area.

Historically, because of the lack of monitoring data to adequately represent the baseline concentration combined with various other limitations associated with the use of ambient air

[30] The EPA also considers emissions decreases occurring after the date of the first PSD application to affect increment consumption to the extent that such decreases cause an improvement of air quality in the area of concern. Thus, the concept of increment "expansion" is also discussed in this section.

quality monitoring data for measuring increment consumption,[31] the EPA has recommended that the required increment analysis be based exclusively on the first approach, which models the increment-related emissions increases or decreases to determine the resulting ambient air quality change and compares this value with the increments for a particular pollutant.

V.1.2 PSD Baseline Area and Key Baseline Dates

In order to evaluate in a PSD permit review whether a PSD increment would be violated by proposed construction of a stationary source, it is necessary to identify (1) the affected geographic area in which the increment will be tracked and (2) the key baseline dates after which emissions changes affect increment in that area. The relevant geographic area for determining the amount of increment consumed is known as the baseline area. The baseline area is established primarily on the basis of the location of the first major source to submit a complete PSD application after an established "trigger date" (see discussion of key dates below) and may be comprised of one or more areas that are designated as "attainment" or "unclassifiable" pursuant to CAA section 107(d) for a particular pollutant within a state. In accordance with the regulatory definition of baseline area at 40 CFR 52.21(b)(15), the area is an "intrastate area" and does not include any area in another state.[32] At a minimum, the baseline area is the attainment or unclassifiable area in which the first PSD applicant after the trigger date proposes to locate, but additional attainment or unclassifiable areas could be included in a particular baseline area when

[31] The EPA described certain limitations associated with the use of ambient air quality monitoring data for measuring increment consumption in the preamble to its proposed PSD regulations in 1979. For example, the CAA provides that certain emissions changes should not be considered increment consuming. These limitations generally continue to apply to the extent that certain emissions changes detected by an ambient monitor are not considered to consume increment. See 44 Fed. Reg. 51924, 51944 (September 5, 1979).

[32] While baseline dates are established on an intrastate basis, once a baseline area is established, emissions changes from other states may contribute to the amount of increment consumed.

the proposed source's modeled impact in any such additional areas exceeds certain concentrations specified in the regulatory definition of baseline area (*i.e.*, concentrations found in 40 CFR 52.21(b)(15)(i)). For $PM_{2.5}$ this concentration is 0.3 μg/m^3 on an annual average basis. Once a baseline area has been established, subsequent PSD applications for sources located in that area, or sources that could have a significant impact in that area, should rely on the baseline date associated with that baseline area to determine whether the applicant's proposed emissions increase, along with other increment-consuming emissions, would cause or contribute to an increment violation. (See discussion on cumulative increment analysis in Section V.3.2 of this guidance.)

Within any baseline area, the following three key dates are relevant when conducting the required increment analysis: (1) trigger date; (2) minor source baseline date; and (3) major source baseline date. The trigger date is a date fixed by regulation for each pollutant at 40 CFR 52.21(b)(14)(ii). The "minor source baseline date" in a newly established baseline area is the earliest date after the applicable trigger date on which a proposed new or modified major source submits a complete PSD application.[33] The minor source baseline date for a baseline area or adjacent baseline area may also be triggered based on the single source impacts greater than or equal to specified values for NO_2, SO_2, PM_{10}, or $PM_{2.5}$.[34] The minor source baseline date is the date on which tracking of increment consumption must begin. Depending upon the number of

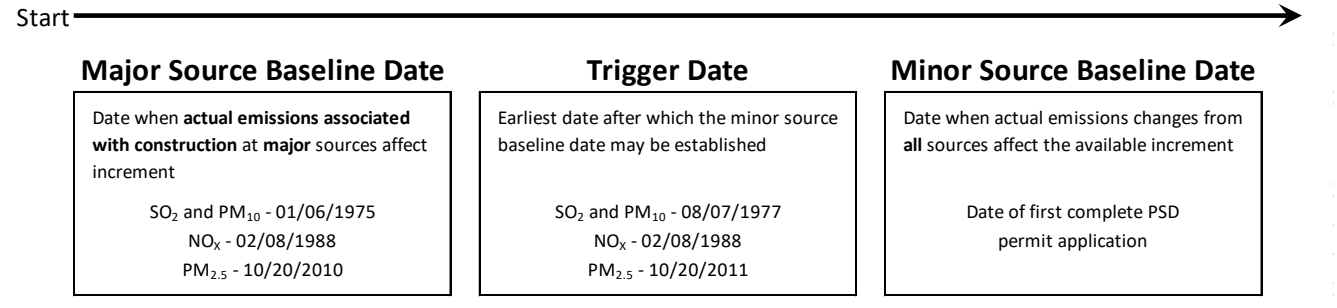
[33] The minor source baseline date is established for each pollutant for which increments have been established if, in the case of a major stationary source, the pollutant would be emitted in significant amounts, or, in the case of a major modification, there would be a significant emissions increase of the pollutant. *See* 40 CFR 52.21(b)(14)(iii). In the PSD program, the pollutant $PM_{2.5}$ includes $PM_{2.5}$ direct emissions and the regulated $PM_{2.5}$ precursors, SO_2 and NO_X. Consequently, the minor source baseline date for $PM_{2.5}$ is established by the first complete PSD application after the trigger date that would have significant direct $PM_{2.5}$ emissions or significant emissions of SO_2 or NO_X as $PM_{2.5}$ precursors.

[34] *See* 40 CFR 52.21(b)(15)(i).

separate attainment and unclassifiable areas that exist for a particular pollutant in a state and the timing of major source construction within the state, there may be a number of minor source baseline dates that apply to different baseline areas established in that state. Beginning with the PSD source whose complete application has established the minor source baseline date in a particular area, any increase or decrease in actual emissions of the pollutant of concern occurring after the minor source baseline date at any source (minor or major) that will affect air quality in the baseline area will affect the amount of PSD increment consumed in that baseline area for that pollutant (in the case of an emissions decrease, see discussion on increment expansion in Section V.1.3 of this guidance, below).

Finally, the "major source baseline date" is a date fixed by regulation for each pollutant at 52.21(b)(14)(i) and *precedes* the trigger date. As further explained below, changes in emissions resulting from construction at major stationary sources only that occur after the major source baseline date, but before the minor source baseline date, will also affect increment. The relationship of these three key dates with each other is further illustrated in Figure V-1.

Figure V-1. Determining Baseline Date(s) and When Increment Consumption Starts



Emissions changes occurring before the minor source baseline date generally do not affect increment in an area (*i.e.*, are not increment-consuming) but are considered to affect the baseline concentration, which, as explained above, represents the ambient pollutant

concentration levels that exist at the time of the minor source baseline date, or the date of the first complete application for a PSD permit in an area after the trigger date. However, as noted above, the CAA provides an exception for certain emissions changes that occur specifically at major stationary sources as a result of construction[35] that commences after the major source baseline date. Specifically, for projects at major stationary sources on which construction commenced on a date prior to the major source baseline date, the changes in emissions from such projects affect the baseline concentration (not the amount of increment consumed) even if the emissions change may not actually occur until after the major or minor source baseline dates. Alternatively, for projects at major stationary sources on which construction commences after the major source baseline date, the project emissions affect increment, even if the new or modified source actually begins operation before the minor source baseline date.

V.1.3 PSD Increment Expansion

The "increment consumption" analysis allows permit applicants and permitting authorities to take into account emissions reductions that occur in the baseline area of concern. Such emissions reductions are generally said to result in the *expansion* of increment in the area; however, not all emissions reductions truly result in an expansion of the increment. Some emissions reductions, instead, result in a *freeing up* of increment that had previously been consumed.

In the case of true "increment expansion," emissions in the area are allowed to increase

[35] CAA section 169(2)(C) indicates that the term "construction," when used in connection with any source or facility, includes modifications defined in CAA section 111(a)(4). "Modification" is defined at section 111(a)(4) to mean "any physical change in, or change in the method of operation of a stationary source which increases the amount of any air pollutant emitted by such source or which results in the emission of any air pollutant not previously emitted."

by the amount allowed by the original increment plus the amount of actual air quality improvement (relative to the baseline concentration) achieved by the reduction of emissions because of its relationship to the established baseline dates for the area.[36] In such cases, it is appropriate to model the actual emissions decrease as a negative amount to effectively lower the baseline concentration to simulate the expansion of the increment.

On the other hand, in cases where a source's emissions contribute to the amount of increment consumed, a reduction in such increment-consuming emissions at some later date results in some amount of the consumed increment being freed up. That is, the resulting air quality improvement is now available for a source to increase its emissions within the limits of the original increment level. A subsequent reduction in increment-consuming emissions should not be modeled as a negative value to determine the amount of increment that has been freed up; instead, such emissions reductions are simply no longer counted in the increment consumption analysis.

V.2 PSD $PM_{2.5}$ Increments

In 2010, the EPA established the $PM_{2.5}$ increments at the levels shown in Table V-1 through the final rule entitled "Prevention of Significant Deterioration (PSD) for Particulate Matter Less Than 2.5 Micrometers ($PM_{2.5}$) – Increments, Significant Impact Levels (SILs) and

[36] The concept of increment expansion is derived from CAA section 163(a), which provides that a PSD applicant must assure "that maximum allowable increases *over baseline concentrations* … shall not be exceeded." [Emphasis added.] The target for determining significant deterioration thus becomes the ambient concentration resulting from the sum of the increment and the baseline concentration. When a decrease in emissions that contributed to the baseline concentration occurs, an emissions increase that simply "restores" the air quality to the baseline concentration in a particular baseline area can be allowed, regardless of the amount of increment otherwise being consumed.

Significant Monitoring Concentration (SMC)."[37] This 2010 rule established October 20, 2011, as the trigger date and October 20, 2010, as the major source baseline date for $PM_{2.5}$ increments. The EPA developed the increment system for $PM_{2.5}$ generally following the same concepts that were previously applied for development of the increments for PM_{10}, SO_2, and nitrogen dioxide (NO_2). As explained above, the framework reflects the statutory concepts set forth in the statutory definition of baseline concentration that was explained in Section V.1 of this guidance.

Table V-1. $PM_{2.5}$ Increments

	Class I	Class II	Class III
Increments, $\mu g/m^3$			
Annual arithmetic mean	1	4	8
24-hour maximum	2	9	18

Source: Prevention of Significant Deterioration (PSD) for Particulate Matter Less Than 2.5 Micrometers (PM2.5) - Increments, Significant Impact Levels (SILs) and Significant Monitoring Concentration (SMC) final rule (75 FR 64864)

The obvious difference between an increment analysis and the NAAQS analysis for $PM_{2.5}$ is that the increment analysis is concerned with the degree of change in air quality caused by a new or modified PSD source rather than the impact of that source on overall air quality (as defined by the applicable NAAQS) in the area of concern (baseline area). With this in mind, it should be noted here that an increment analysis is relevant only to the extent that NAAQS compliance has been ensured. That is, an adequate air quality analysis demonstrating compliance with the statutory requirements must ensure that the proposed PSD source's emissions will not cause or contribute to either the NAAQS or PSD increments.[38]

Another key difference involves the modeling inventory from which the necessary

[37] See 75 FR 64864 (Oct. 20, 2010).

[38] CAA section 163(b)(4) provides that the maximum allowable concentration of any air pollutant allowed in an area shall not exceed the concentration allowed by the primary or secondary NAAQS.

emissions data is derived. That is, only sources that have $PM_{2.5}$ emissions (direct and precursor) that affect the amount of increment consumed in the area of concern should be included in the modeling inventory for the increment analysis. Moreover, from such sources, only those specific emissions changes that affect increment should be included in the actual modeling analysis.

The cumulative impact analysis for $PM_{2.5}$ increments is also different and based on the actual emission changes occurring at existing sources in the baseline area after the pertinent baseline dates (*i.e.*, major and minor source baseline dates), whereas NAAQS analyses are generally based on the cumulative impact associated with the maximum allowable emissions from the new or modifying source and other nearby sources (with specific provisions for operating levels of nearby sources). Furthermore, ambient monitoring data, while useful for establishing background concentration for the NAAQS analysis, may not be particularly useful for the typical increment analysis. The limitations associated with using monitoring data for an increment analysis are discussed in greater detail in Sections V.1 and V.3 of this guidance.

It is also important to note that the $PM_{2.5}$ NAAQS and increments for the 24-hour averaging period are defined in different forms and therefore must be analyzed differently.[39] The 24-hour $PM_{2.5}$ NAAQS is defined based on the 3-year average of the annual 98^{th} percentile of the 24-hour average concentrations, while the 24-hour $PM_{2.5}$ increments are based on the second highest maximum 24-hour concentration.

V.3 PSD Compliance Demonstration for the $PM_{2.5}$ Increments

The initial steps for the $PM_{2.5}$ increment analysis, which include the determination of the allowable emissions increases to model in the source impact analysis and a comparison of the

[39] The annual NAAQS and increments for $PM_{2.5}$ are both measured as annual arithmetic mean values.

modeled impacts against the appropriate $PM_{2.5}$ SILs, may rely, in part, upon the results derived from the $PM_{2.5}$ NAAQS analysis described in Sections III and IV of this guidance. Moreover, the technical approach involving the options and alternatives agreed upon for estimating secondary $PM_{2.5}$ impacts and combining primary and secondary $PM_{2.5}$ impacts for the NAAQS analysis may also be relevant for completing the $PM_{2.5}$ increment analysis to determine whether the allowable emissions increase(s) from the proposed source or modification will cause or contribute to any increment violation.

V.3.1 $PM_{2.5}$ Increments: Source Impact Analysis

The EPA's recommendations on how to complete the required compliance demonstration for the $PM_{2.5}$ PSD increments are based upon the same assessment cases detailed in Section II.4 for $PM_{2.5}$ NAAQS. As shown in Table V-2, a modeled compliance demonstration is not required for Case 1 since neither direct $PM_{2.5}$ emissions nor $PM_{2.5}$ precursor (NO_X or SO_2) emissions are equal to or greater than the respective SERs. Case 1 is the only assessment case that does not require a modeled compliance demonstration for $PM_{2.5}$, whereas Case 2 requires a source impact analysis that should be conducted following the detailed recommendations provided in previous sections for a NAAQS analysis.

Table V-2. EPA Recommended Approaches for Assessing Primary and Secondary $PM_{2.5}$ Impacts by Assessment Case

Assessment Case	Description of Assessment Case		Primary Impacts Approach	Secondary Impacts Approach*
Case 1: No Air Quality Analysis	Direct $PM_{2.5}$ emissions < 10 tpy SER and NO_X emissions and SO_2 emissions < 40 tpy SER		N/A	N/A
Case 2: Primary and Secondary Air Quality Impacts	Direct $PM_{2.5}$ emissions ≥ 10 tpy SER or NO_X emissions or SO_2 emissions ≥ 40 tpy SER		**Appendix W preferred or approved alternative dispersion model**	Include both precursor of $PM_{2.5}$, see Section II.2. • **Tier 1 Approach** (*e.g.*, MERPs) • **Tier 2 Approach** (*e.g.*, Chemical Transport Modeling)

***** In unique situations (*e.g.*, in parts of Alaska where photochemistry is not possible for portions of the year), it may be acceptable for the applicant to rely upon a qualitative approach to assess the secondary impacts. Any qualitative assessments should be justified on a case-by-case basis in consultation with the appropriate EPA Regional Office or other applicable permitting authority.

A modeling analysis based solely on the PSD applicant's proposed emissions increase (*i.e.*, source impact analysis) that does not predict an ambient impact equal to or greater than the appropriate $PM_{2.5}$ SIL at any location generally will satisfy the requirement for a demonstration that the source will not cause or contribute to a violation of the $PM_{2.5}$ increments.

In light of the relatively recent establishment of the fixed dates (*i.e.*, major source baseline date and trigger date) associated with the $PM_{2.5}$ increments (compared to comparable fixed dates for other PSD increments), and the possibility that the minor source baseline date for a particular area has not yet been set, a proposed new or modified source being evaluated for compliance with the $PM_{2.5}$ increments in a particular area may be the first source in the area with increment-consuming emissions. As indicated in Figure II-2, under this situation, a permitting authority may have a sufficient basis to conclude that the $PM_{2.5}$ impacts of the new or modified PSD source, although greater than the appropriate $PM_{2.5}$ SILs, may be compared directly to the

allowable $PM_{2.5}$ increments without the need for a cumulative analysis (described in Section V.3.2 of this guidance below). Reliance on this first-in source impact analysis likely would be appropriate to assess the amount of increment consumed when the proposed new or modified source represents the first complete PSD application since the trigger date, thus establishing the baseline concentration in the area, and there has been no other major source construction since the major source baseline date.

V.3.2 $PM_{2.5}$ Increments: Cumulative Analysis

Where the source impact analysis described above is insufficient to show that a proposed PSD source will not cause or contribute to a violation of the $PM_{2.5}$ PSD increments, a cumulative impact assessment is necessary to complete the required increment analysis. A cumulative assessment of increment consumption accounts for the combined impacts of the following:

1. Direct and precursor *allowable* emissions from the proposed new or modifying source;
2. Direct and precursor *actual* emissions changes that have occurred at existing sources (including the existing source at which a major modification is being proposed, where applicable) since the minor source baseline date for the proposed source's baseline area;
3. Direct and precursor *actual* emissions from any major stationary source on which construction commenced after October 20, 2010 (major source baseline date for $PM_{2.5}$); and
4. Direct and precursor *allowable* emissions of permitted sources that are not yet fully

operative.[40]

Unlike the guidance provided for the cumulative NAAQS analysis for $PM_{2.5}$ in Section IV, it is not typically practical to utilize ambient monitoring data to represent any portion of the impacts that affect the $PM_{2.5}$ increments. Therefore, it is usually necessary to model the applicable emissions from any existing source that will be considered to consume a portion of the $PM_{2.5}$ increments in the baseline area(s) of concern. As part of the determination of which existing sources should be included in the cumulative analysis, it will be necessary to identify the total area in which a significant impact from the new or modified PSD source will occur. A new or modified source with an extensive impact area may affect more than one existing baseline area. Once the affected area has been defined, and the associated minor source baseline dates have been taken into account, the potential sources can be selected from which increment-consuming emissions must be quantified. Existing sources whose actual emissions have not changed substantially since the applicable baseline date may not need to be included for purposes of increment consumption since, as previously explained, increment is consumed by increases in actual emissions that occur from existing sources after the baseline date. It is highly recommended that the PSD applicant work closely with the permitting authority to determine the existing sources (including newly permitted sources) of direct $PM_{2.5}$ and precursor emissions that should be included in the modeling inventory for the increment analysis. Also, if there is reason to believe that an existing source's actual emissions have decreased since the applicable baseline date, the PSD applicant may want to check with the permitting authority to ascertain whether the authority allows for increment expansion to be considered.

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[40] Regarding the use of allowable emissions, see 40 CFR 52.21(b)(21)(iv).

Once the modeling inventory for the increment analysis has been developed and approved, and the increment-consuming emissions have been determined, the modeled cumulative impacts resulting from the increases and decreases in emissions are then compared to the $PM_{2.5}$ increments to determine whether any increment violations will result. This section provides recommendations on conducting an appropriate cumulative impact assessment for $PM_{2.5}$ increments.

V.3.2.1 Assessing Primary $PM_{2.5}$ Impacts

As explained in Section III.3 of this guidance, the assessment of primary $PM_{2.5}$ impacts from the proposed new or modifying PSD source is essentially the same for the $PM_{2.5}$ NAAQS and increments. In both cases, the permit applicant must account for the impacts from the proposed new or modifying source's *allowable* emissions increase of direct $PM_{2.5}$.

To assess the impact of direct $PM_{2.5}$ emissions from existing increment-consuming sources, *actual* emissions increases that have occurred since the applicable minor source baseline date should generally be modeled. Alternatively, existing source impacts from direct $PM_{2.5}$ emissions may be conservatively modeled using an existing source's *allowable* emissions where the PSD applicant determines that such emissions are more readily available and especially when such allowable emissions are not expected to contribute substantially to the amount of increment consumed. In the event that an applicant chooses to conduct the cumulative analysis using *allowable* emissions and identifies potential problems concerning increment consumption, the PSD applicant may then rely on more refined data that better represent a particular source's *actual* emissions.

The $PM_{2.5}$ increments analysis should follow the traditional approach involving modeling

only direct $PM_{2.5}$ emissions changes that affect the increment and should be based on application of AERMOD (or other acceptable preferred or approved alternative model), using actual emission changes associated with any increment-consuming or increment-expanding sources. The AERMOD model allows for inclusion of these emissions (represented as negative emissions for the sources expanding increment)[41] in the same model run that includes the allowable increase in emissions from the proposed source and will, therefore, output the net cumulative concentrations at each receptor established for the modeling domain.[42]

V.3.2.2 Assessing Secondary $PM_{2.5}$ Impacts

To assess the secondary impacts from changes in $PM_{2.5}$ precursor emissions from the new or modified source, as well as from other increment-consuming sources, the EPA recommends the analysis for each applicable precursor of $PM_{2.5}$ be conducted collectively based on the two-tiered demonstration approach outlined in EPA's 2017 *Guideline*.

In recent years, several rules promulgated by the EPA have resulted in control requirements that have significantly reduced NO_X and SO_2 precursor emissions affecting ambient $PM_{2.5}$ concentrations in many areas.[43] This is particularly true in the eastern U.S. As a result, in some cases, the secondary $PM_{2.5}$ impacts may be addressed by a demonstration that provides ambient monitoring data that generally confirms a downward trend in precursor emissions occurring after the applicable $PM_{2.5}$ minor source baseline date (or the major source baseline

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[41] See discussion about increment expansion in Section V.1.3 of this guidance.

[42] The "maximum" cumulative impacts will be output as zero if the cumulative impacts computed in the model are less than zero).

[43] Such rules include the following: the Clean Air Interstate Rule (CAIR) Final Rule, 70 FR 25162 (May 12, 2005); CSAPR Final Rule, 76 FR 48208 (August 8, 2011); CSAPR Update for the 2008 Ozone NAAQS (CSAPR Update) Final Rule, 81 FR 74504 (October 26, 2016); and the Mercury and Air Toxics Standards Rule (MATS), 77 FR 9304 (February 16, 2012).

date). If it can be confirmed that such emissions reductions have occurred in a particular baseline area, it may be possible to complete the $PM_{2.5}$ increments modeling analysis simply by focusing on potential increment consumption associated with direct $PM_{2.5}$ emissions. For areas where $PM_{2.5}$ precursor emission increases from other increment-consuming sources have occurred since the major or minor source baseline dates, and are, thus, likely to have added to $PM_{2.5}$ concentration increases within the baseline area (and, thus, consume $PM_{2.5}$ increment), the Tier 1 and Tier 2 assessment approaches based on CTMs (using the emissions input data applicable to increment analyses) discussed in Section III of this guidance may be appropriate for estimating the portion of $PM_{2.5}$ increment consumed due to secondary $PM_{2.5}$ impacts associated with those increases in precursor emissions.

V.4. Determining Whether a Proposed Source Will Cause or Contribute to an Increment Violation

When a proposed PSD source predicts, through a cumulative impact analysis, that a modeled violation of any $PM_{2.5}$ increment will occur within the baseline area of concern, a closer examination of the proposed source's individual impact(s) at the violating receptor(s) and the time(s) of modeled violation become important considerations. The EPA's longstanding policy is to consider a proposed PSD source to cause or contribute to an increment violation if its impact (primary and secondary) is significant (equal to or greater than the appropriate $PM_{2.5}$ SIL) at the location and time of the modeled violation.[44] Accordingly, if a source can demonstrate to the

[44] *See*, *e.g.*, 43 FR 26380 at 26401, June 19, 1978; EPA memo titled "Interpretation of 'Significant Contribution,'" December 16, 1980; EPA memo titled "Air Quality Analysis for Prevention of Significant Deterioration," July 5, 1988; and more recently, EPA memo titled "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program," April 17, 2018, Attachment at page 18 ("If the modeled impact is below the recommended SIL value *at the violating receptor during the violation*, the EPA believes this will be sufficient in most cases for a permitting authority …to conclude that the source does not cause or contribute to…the predicted violation.")(Emphasis added).

satisfaction of the permitting authority that significant impacts attributable to the source do *not* occur at the location and time of any modeled violation,[45] the proposed source or modification generally may be considered to not cause or contribute to an increment violation. In cases where a proposed PSD source models impacts that equal or exceed the appropriate $PM_{2.5}$ SIL *and* would cause a new violation of any $PM_{2.5}$ increment, it is the EPA's longstanding policy to allow the PSD applicant to obtain sufficient offsets, in the form of emissions reductions internally or from another existing source, to avoid causing the predicted violation at each affected receptor where (and when) a violation is modeled. In an area where a proposed PSD source would cause or contribute to an existing increment violation(s), the PSD source must not be approved for construction unless such existing violation(s) is entirely corrected at each affected receptor prior to the operation of the proposed source.[46]

[45] The difficulties associated with combining primary and secondary impacts spatially and temporally were described in Sections III and IV of this guidance. In the case of a $PM_{2.5}$ increment analysis, as with the $PM_{2.5}$ NAAQS analysis, the applicant and permitting authority will need to agree upon an approach that best satisfies the required compliance demonstration.

[46] *See*, *e.g.*, 43 FR 26380 at 26401, June 19, 1978; 45 FR 52676 at 52678, August 7, 1980; and EPA memo titled "Air Quality Analysis for Prevention of Significant Deterioration," July 5, 1988. ("…for any increment violation (new or existing) for which the proposed source has a significant impact, the permit should not be approved unless the increment violation is corrected prior to operation of the proposed source.) Note that this policy for the PSD increments differs from the policy for sources that contribute to an existing NAAQS violation, for which the proposed sources needs only compensate for its own adverse impact on the NAAQS violation in accordance with 40 CFR 51.165(b)(3).

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Appendix A: Draft Conceptual Description of O_3 and $PM_{2.5}$ Concentrations in the U.S.

This appendix provides a brief summary of the current O_3 and $PM_{2.5}$ monitoring networks. It also characterizes O_3 and PM air quality in terms of their precursor emissions and chemical composition, concentration levels, and spatial and temporal patterns across the nation based on the ambient data and analyses contained in the EPA's "Integrated Science Assessment for Ozone and Related Photochemical Oxidants,"[47] "The Particle Pollution Report,"[48] and "Particulate Matter Staff Paper."[49] Such information may be useful for permit applicants in preparing conceptual descriptions, as discussed in this guidance. Permit applicants also encouraged to reference the EPA's "Air Quality Trends" website at https://www.epa.gov/air-trends for the current O_3 and $PM_{2.5}$ trends and design values.

Conceptual Descriptions of O_3

1. O_3 Monitoring Networks

To monitor compliance with the NAAQS, state, local, and tribal environmental agencies operate O_3 monitoring sites at various locations, depending on the population of the area and typical peak O_3 concentrations. In 2015, there were over 1,300 O_3 monitors reporting O_3 concentration data to EPA. All monitors that currently report O_3 concentration data to the EPA use ultraviolet Federal Equivalent Methods (FEMs). Since the highest O_3 concentrations tend to be associated with particular seasons for various locations, EPA requires O_3 monitoring during specific monitoring seasons which vary by state. The O_3 monitoring seasons for each state are listed in Appendix D to 40 CFR part 58.

Figure A-1 shows the locations of all U.S. ambient O_3 monitoring sites reporting data to EPA during the 2013-2015 period. The gray dots represent State and Local Ambient Monitoring Stations (SLAMS) which are operated by state and local governments to meet regulatory requirements and provide air quality information to public health agencies. SLAMS monitors make up about 80 percent of the ambient O_3 monitoring network in the U.S. The minimum monitoring requirements to meet the SLAMS O_3 network design criteria are specified in Appendix D to 40 CFR part 58. The requirements are based on both population and ambient concentration levels for each Metropolitan Statistical Area (MSA). At least one site for each MSA must be designed to record the maximum concentration for that particular area. The blue dots highlight two important subsets of monitoring sites within the SLAMS network: the "National Core" (NCore) network, which consists of about 80 monitoring sites that collect multi-

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[47] U.S. Environmental Protection Agency (2013). Integrated Science Assessment for Ozone and Related Photochemical Oxidants. U.S. Environmental Protection Agency, Research Triangle Park, NC. EPA/600/R-10/076 (2013 ISA), section 3.2.2 found at https://cfpub.epa.gov/ncea/isa/recordisplay.cfm?deid=247492.

[48] The Particle Pollution Report: Current Understanding of Air Quality and Emissions through 2003. https://www.epa.gov/sites/production/files/2017-11/documents/pp_report_2003.pdf.

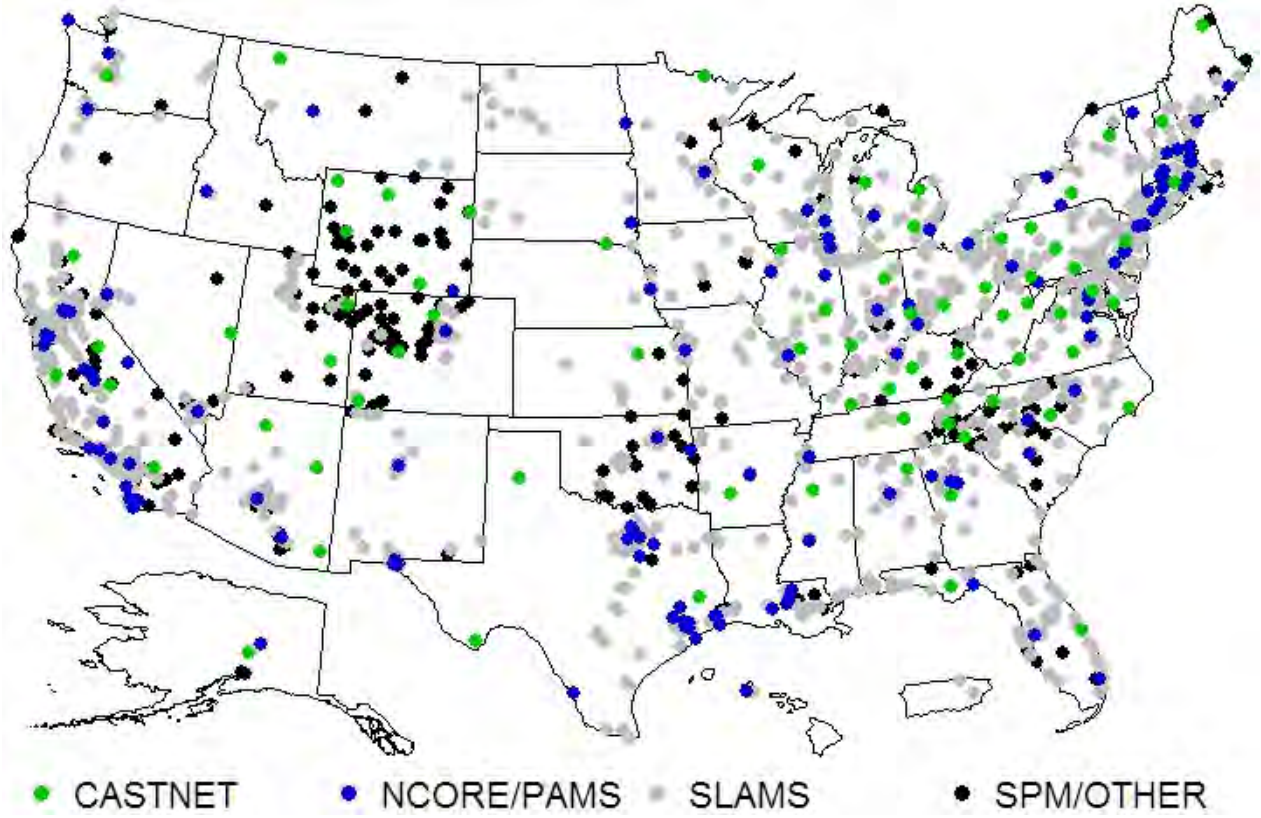
[49] Particulate Matter Staff Paper: Review completed in 2012. https://www.epa.gov/naaqs/particulate-matter-pm-air-quality-standards-documents-review-completed-2012.

pollutant measurements on a year-round basis, and the "Photochemical Assessment Monitoring Stations" (PAMS) network, which consists of about 75 monitoring sites that collect summertime measurements of various precursor gases involved O_3 formation.

The green dots in Figure A-1 represent O_3 monitoring sites in the Clean Air Status and Trends Network (CASTNet) which are mostly located in rural areas. There were about 80 CASTNet sites reporting data to EPA in 2015, with sites in the eastern U.S. generally being operated by the EPA, and sites in the western U.S. generally being operated by the National Park Service (NPS).

Finally, the black dots in Figure A-1 represent "Special Purpose" (SPM) monitoring sites, which generally collect data for research studies, public health reporting, or other non-regulatory purposes, and all other O_3 monitoring sites which includes monitors operated by tribes, industry, and other federal agencies such as the U.S. Forest Service (USFS).

Figure A-1. Locations of U.S. Ambient O_3 Monitoring Sites in 2013-2015



2. O_3 Precursor Emissions and Atmospheric Chemistry

O_3 is formed by photochemical reactions of precursor gases and is not directly emitted from specific sources. In the stratosphere, O_3 occurs naturally and provides protection against harmful solar ultraviolet radiation. In the troposphere, near ground level, O_3 forms through atmospheric reactions involving two main classes of precursor pollutants: volatile organic

compounds (VOCs) and nitrogen oxides (NO_X). Carbon monoxide (CO) and methane (CH_4) are also important for O_3 formation over longer time periods.[50]

Emissions of O_3 precursor compounds can be divided into anthropogenic and natural source categories, with natural sources further divided into biogenic emissions (from vegetation, microbes, and animals) and abiotic emissions (from biomass burning, lightning, and geogenic sources). Anthropogenic sources, including mobile sources and power plants, account for the majority of NO_X and CO emissions. Anthropogenic sources are also important for VOC emissions, though in some locations and at certain times of the year (*e.g.*, southern states during summer), the majority of VOC emissions come from vegetation.[51] In practice, the distinction between natural and anthropogenic sources is often unclear, as human activities directly or indirectly affect emissions from what would have been considered natural sources during the preindustrial era. Thus, emissions from plants, animals, and wildfires could be considered either natural or anthropogenic, depending on whether emissions result from agricultural practices, forest management practices, lightning strikes, or other types of events.[52]

Rather than varying directly with emissions of its precursors, O_3 changes in a nonlinear fashion with the concentrations of its precursors. NO_X emissions lead to both the formation and destruction of O_3, depending on the local quantities of NO_X, VOC, radicals, and sunlight. In areas dominated by fresh emissions of NO_X, radicals are removed, which lowers the O_3 formation rate. In addition, the scavenging of O_3 by reaction with NO is called "titration" and is often found in downtown metropolitan areas, especially near busy streets and roads, as well as in power plant plumes. This short-lived titration results in localized areas in which O_3 concentrations are suppressed compared to surrounding areas, but which contain NO_2 that adds to subsequent O_3 formation further downwind. Consequently, O_3 response to reductions in NO_X emissions is complex and may include O_3 decreases at some times and locations and increases of O_3 at other times and locations. In areas with relatively low NO_X concentrations, such as those found in remote continental areas and rural and suburban areas downwind of urban centers, O_3 production typically varies directly with NO_X concentrations (*e.g.*, decreases with decreasing NO_X emissions). The NOx titration effect is most pronounced in urban core areas which have higher volume of mobile source NO_X emissions from vehicles than do the surrounding areas. It should be noted that such locations, which are heavily NO_X saturated (or radical limited), tend to have much lower observed O_3 concentrations than downwind areas. As a general rule, as NOx emissions reductions occur, one can expect lower O_3 values to increase while the higher O_3 values would be expected to decrease. NOx reductions are expected to result in a compressed O_3 distribution, relative to current conditions.

The formation of O_3 from precursor emissions is also affected by meteorological parameters such as the intensity of sunlight and atmospheric mixing. Major episodes of high ground-level O_3 concentrations in the eastern United States are associated with slow-moving high pressure systems. High pressure systems during the warmer seasons are associated with the

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[50] 2013 ISA, section 3.2.2.

[51] 2013 ISA, section 3.2.1.

[52] 2013 ISA, sections 3.2 and 3.7.1.

sinking of air, resulting in warm, generally cloudless skies, with light winds. The sinking of air results in the development of stable conditions near the surface which inhibit or reduce the vertical mixing of O_3 precursors. The combination of inhibited vertical mixing and light winds minimizes the dispersal of pollutants, allowing their concentrations to build up. In addition, in some parts of the United States (*e.g.*, in Los Angeles), mountain barriers limit mixing and result in a higher frequency and duration of days with elevated O_3 concentrations. Photochemical activity involving precursors is enhanced during warmer seasons because of the greater availability of sunlight and higher temperatures.[53]

3. Spatial and Temporal Patterns in Ambient O_3 Concentrations

3.1. Diurnal and Seasonal Patterns

Since O_3 formation is a photochemical process, it is not surprising that concentration levels have strong diurnal and seasonal patterns. Concentration levels tend to be highest at times when sunlight reaches its highest intensity, namely during the afternoon hours of the late spring and summer months. However, there are other factors at work, such as the influence of biogenic VOC emissions and stratospheric intrusions during the spring months, long-range transport, and traffic patterns which often cause peak NO_X emissions to occur during the morning and evening rush hours.

Figure A-2 shows the diurnal pattern in the hourly O_3 concentrations based on ambient monitoring data from 2000 to 2015. For each monitoring site, the median (top panel) and 95th percentile (bottom panel) values for each hour of the day were calculated, and each boxplot shows the range of those values for that particular hour across all monitoring sites. The whiskers of each boxplot extend to the 5th and 95th percentiles, the box represents the inter-quartile range, and the centerline represents the median value. The median and 95th percentile values show a consistent pattern in that O_3 levels tend to be lowest during the early AM hours, increasing rapidly after sunrise. Concentrations typically reach their peak during the afternoon hours, then decrease at a fairly constant rate throughout the evening and nighttime hours.

Figure A-3 shows the seasonal pattern in the daily maximum 8-hour O_3 concentrations based on ambient monitoring data from 2000 to 2015. For each monitoring site, the median (top panel) and 95th percentile (bottom panel) values for each month of the year were calculated, and each boxplot shows the range of those values for that particular month across all monitoring sites. The whiskers of each boxplot extend to the 5th and 95th percentiles, the box represents the inter-quartile range, and the centerline represents the median value. Again, the median and 95th percentile values show a consistent pattern in that O_3 levels tend to be highest during the spring and summer months (April to September), and lower during the fall and winter months (October to March).

[53] 2013 ISA, section 3.2.

Figure A-2. Distribution of Median and 95th Percentile Hourly O_3 Concentrations by Hour of the Day based on 2000-2015 Monitoring Data

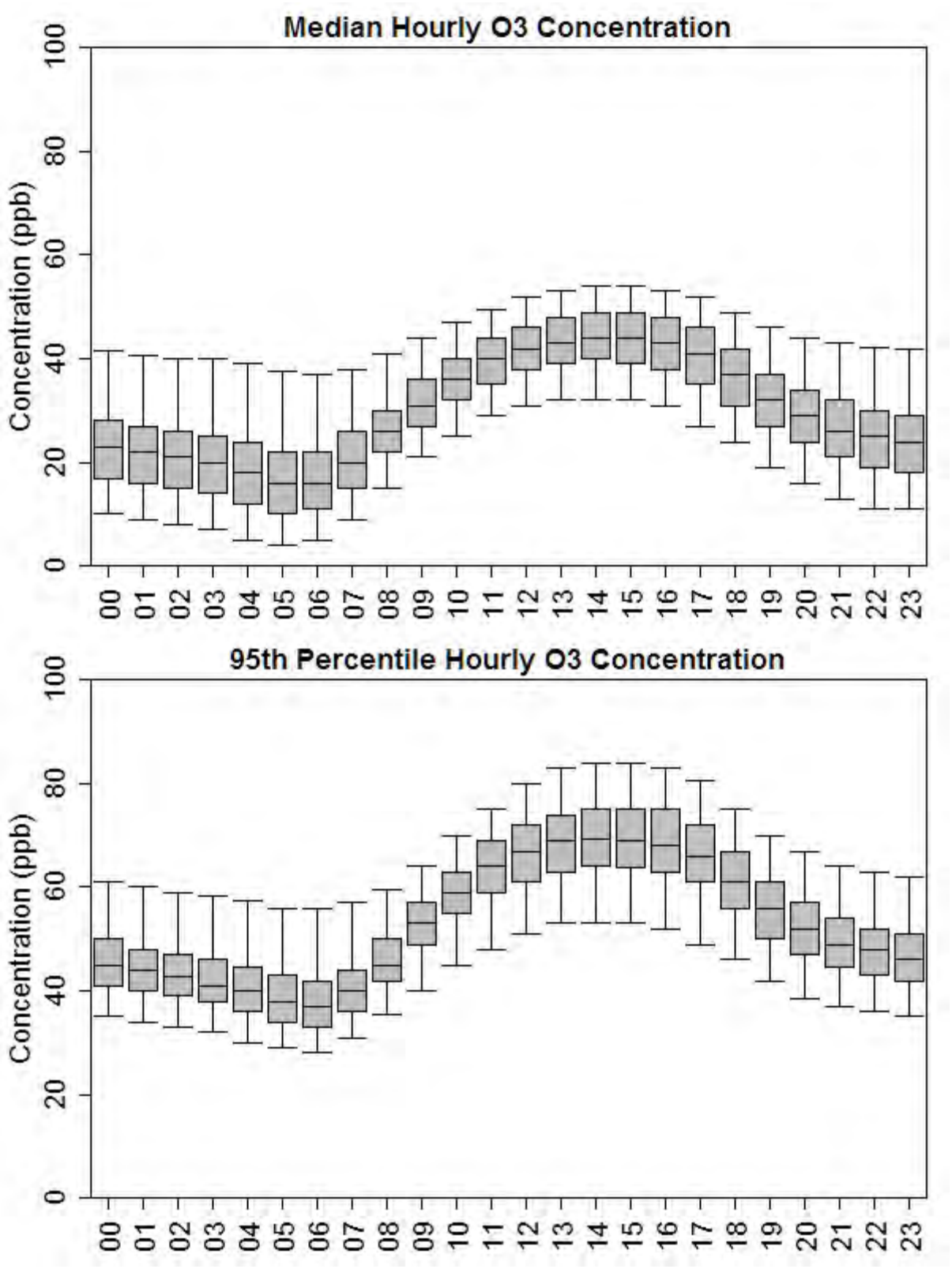
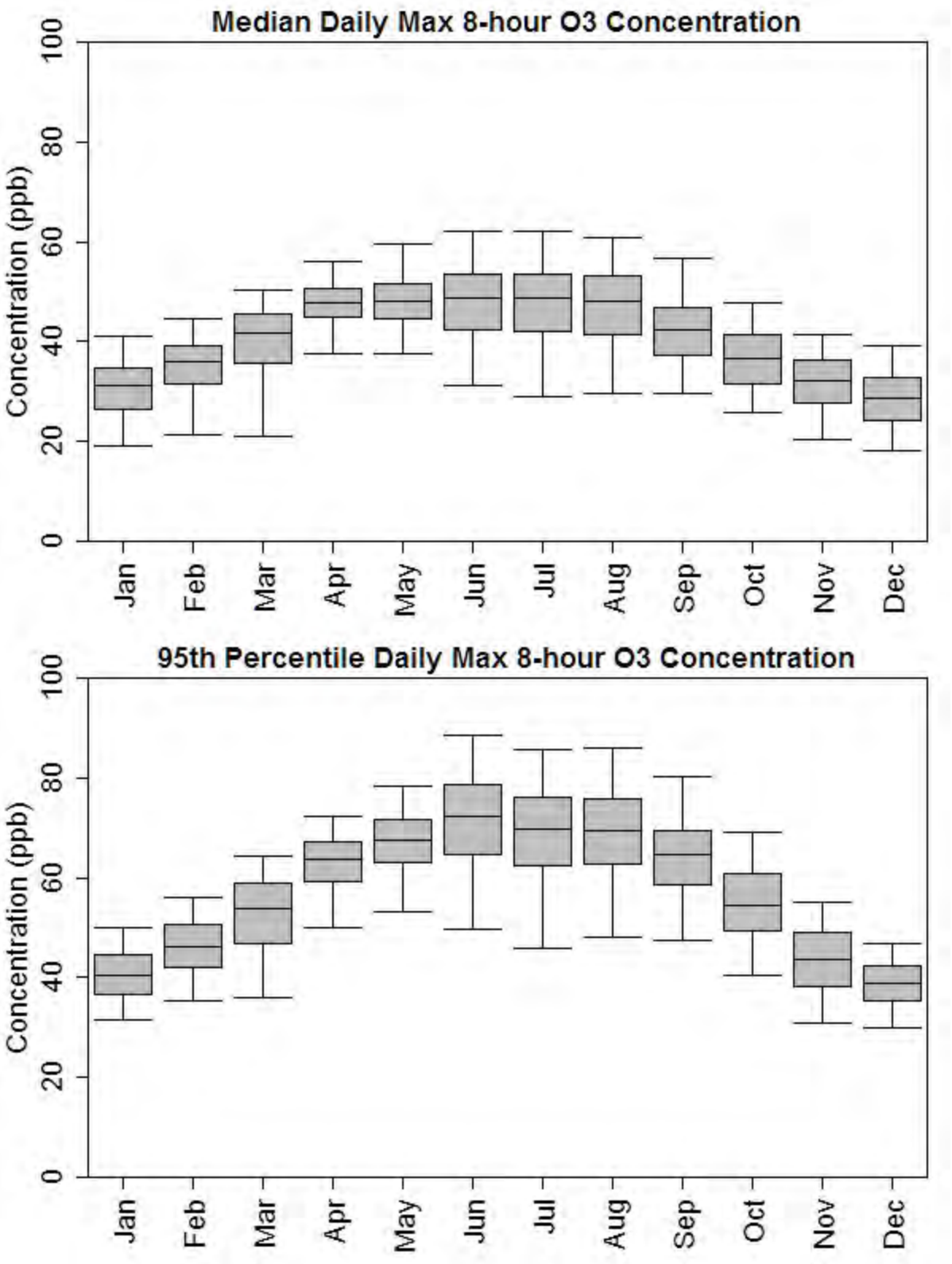


Figure A-3. Distribution of Median and 95th Percentile Daily Maximum 8-hour O_3 Concentrations by Month of the Year based on 2000-2015 Monitoring Data

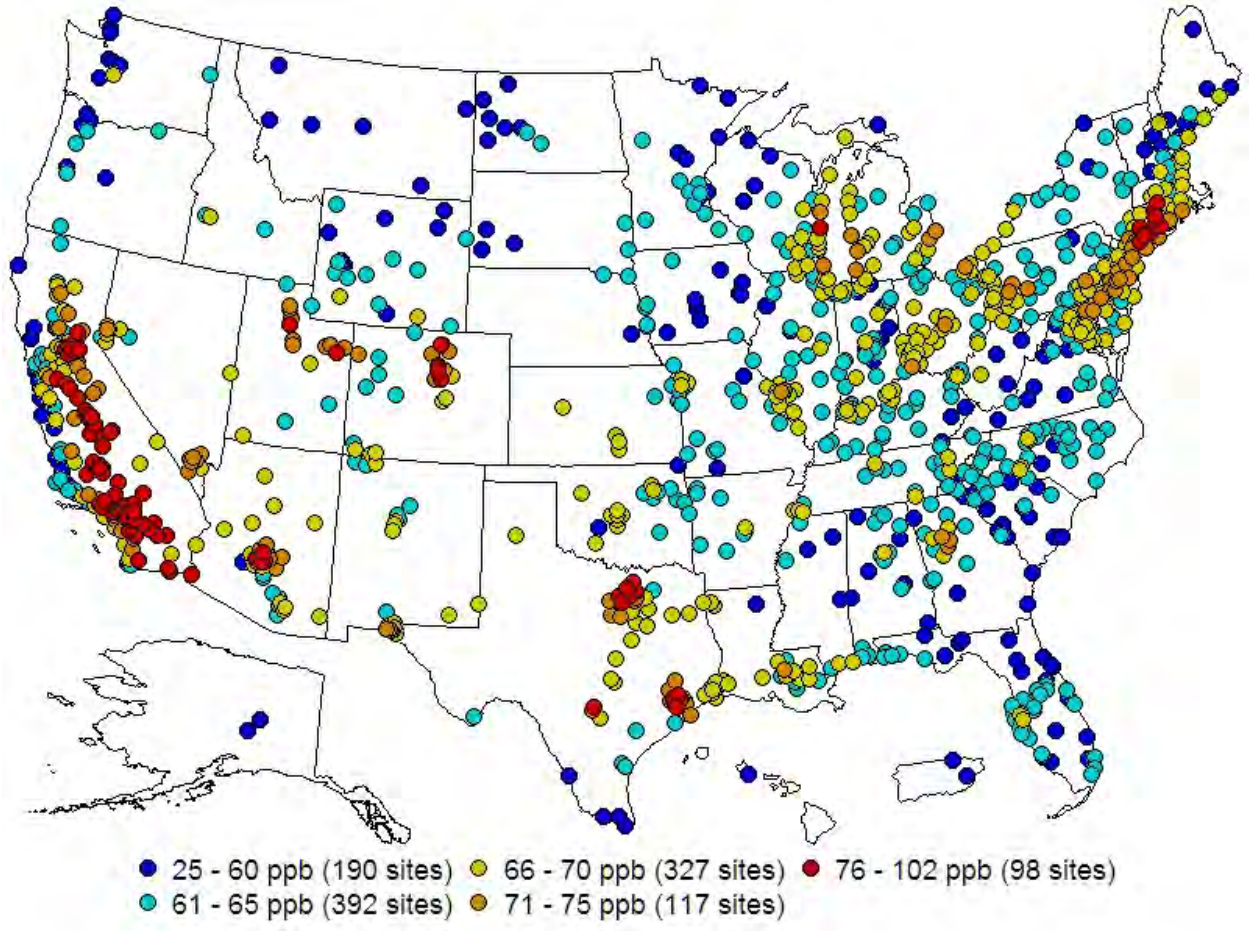


3.2. Spatial Patterns

To determine whether or not the O_3 NAAQS has been met at an ambient monitoring site, a statistic commonly referred to as a "design value" must be calculated based on three consecutive years of data collected from that site. The form of the O_3 NAAQS design value statistic is the 3-year average of the annual 4th highest daily maximum 8-hour O_3 concentration in parts per million (ppm). The O_3 NAAQS is met at an ambient monitoring site when the design value is less than or equal to 0.070 ppm. In counties or other geographic areas with multiple monitors, the area-wide design value is defined as the design value at the highest individual monitoring site, and the area is said to have met the NAAQS if all monitors in the area are meeting the NAAQS.

Figure A-4 shows a map of the O_3 design values in the U.S. based on data collected during the 2013-2015 period. The highest design values occur in California and near large metropolitan areas such as Dallas, Denver, Houston, New York City, and Phoenix. The lowest design values occur in the Pacific Northwest, the Northern Rockies, the Upper Midwest, and parts of New England and the Southeast. In general, sparsely populated areas tend to have lower design values than more urbanized areas.

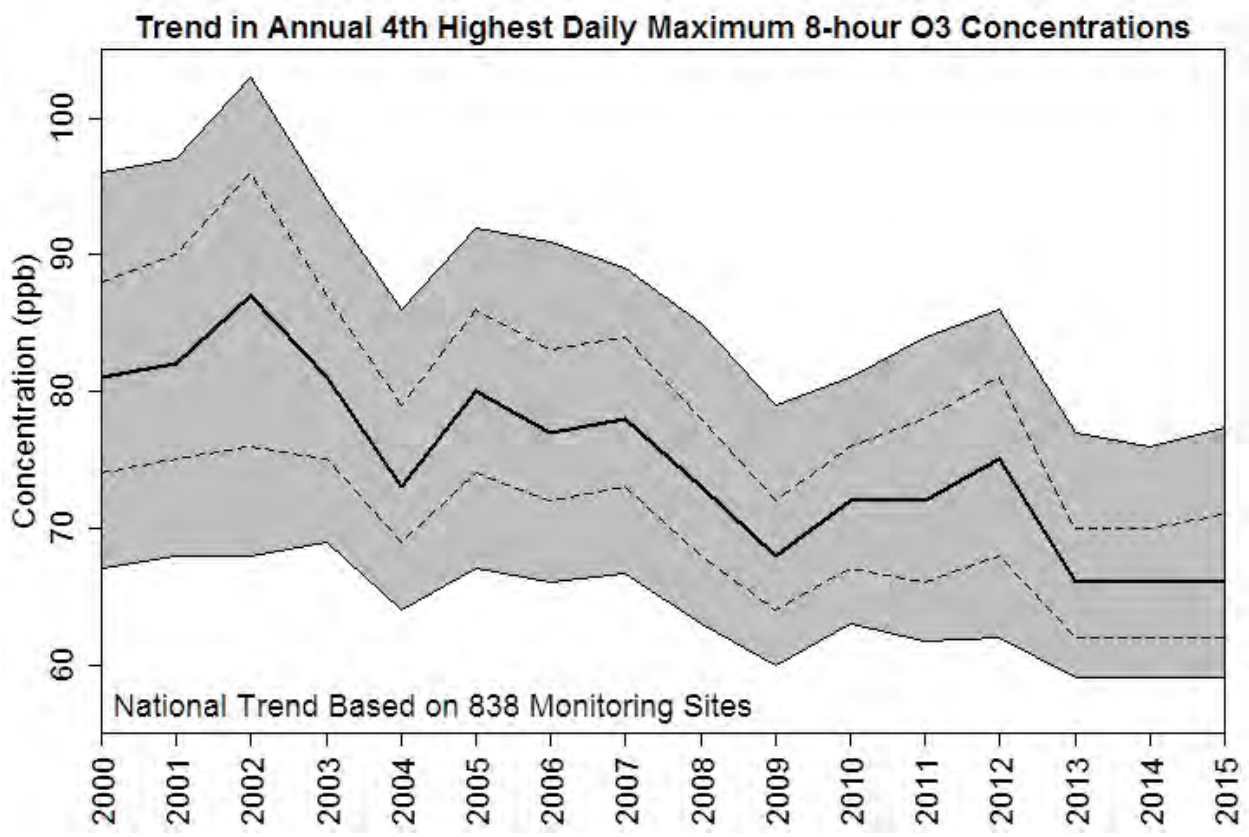
Figure A-4. Map of 2013-2015 O_3 Design Values in parts per billion (ppb)



3.3. Interannual Variability and Trends

Figure A-5 shows the national trend in the annual 4th highest daily maximum 8-hour O_3 concentration from 2000 to 2015. The solid black line represents the median value for each year based on 838 "trends" sites with complete monitoring records, the dashed lines represent the 25th and 75th percentile values for each year, and the shaded gray area covers the 10th percentile value up to the 90th percentile value for each year. While there is considerable year-to-year variability, overall the trend shows an improvement in O_3 air quality over the 15-year period. In fact, the median annual 4th highest value has decreased by 18% since the beginning of the century, and by 24% since 2002.

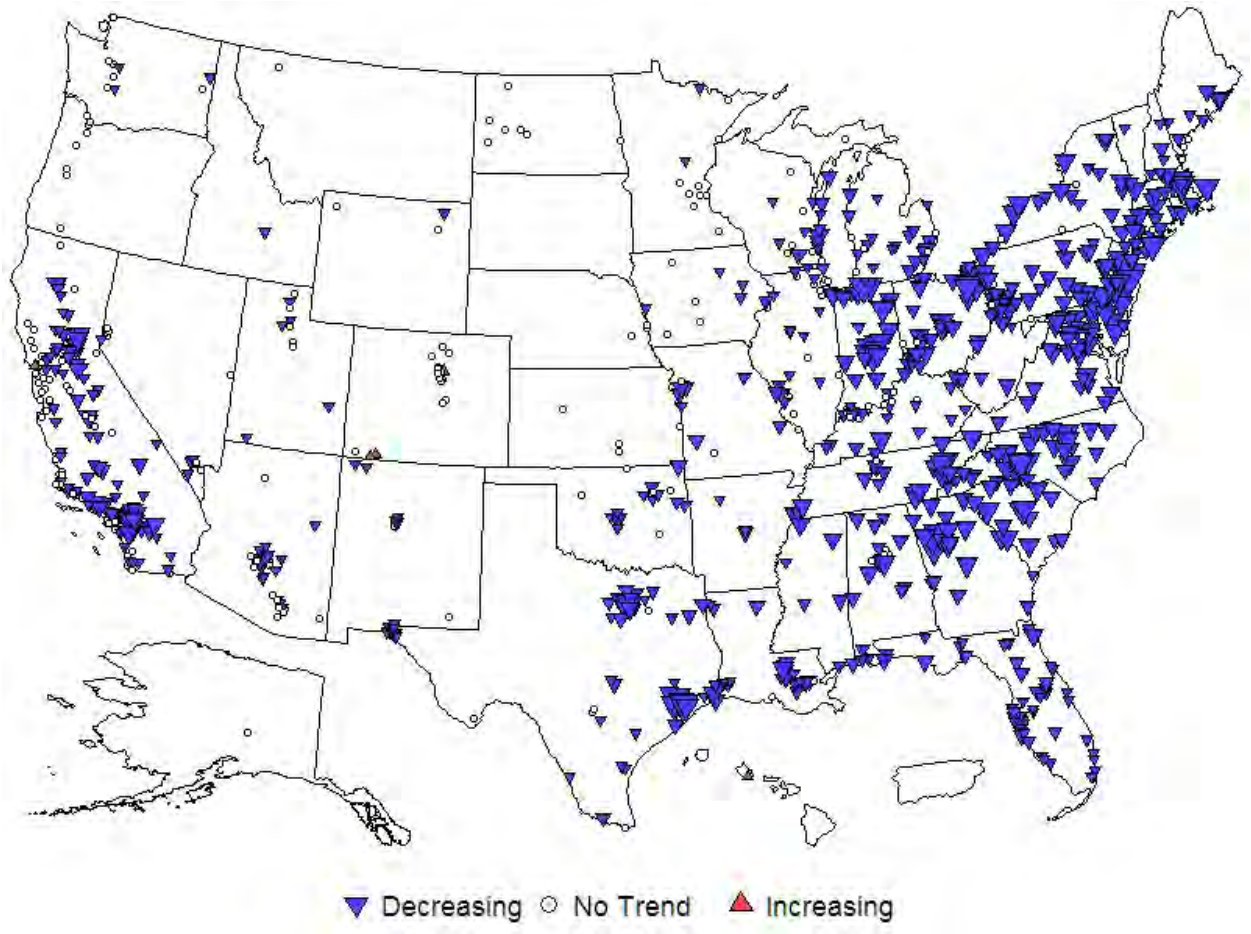
Figure A-5. National Trend in the Annual 4th Highest Daily Maximum 8-hour O_3 Concentration



Since the national trend is a simple aggregate of the site-level trends, it is also important to look at how these trends vary spatially. Figure A-6 shows a map of the trends at each monitoring site with at least 12 complete years of data from 2000-2015. The magnitude of the trend at each site is computed using the Theil-Sen slope estimator, and the Mann-Kendall statistic is calculated in order to test for statistical significance using a threshold of 0.05. The trend at each monitoring site is classified as Decreasing (p-value < 0.05, slope < 0; blue triangles), No Trend (p-value >= 0.05, white circles), or Increasing (p-value < 0.05, slope > 0; red triangles). The size of each triangle is proportional to the magnitude of the trend at each monitoring site.

Figure A-6 shows that O_3 levels have decreased across much of the eastern U.S. as a result of regional control programs such as the NOx SIP Call and the Clean Air Interstate Rule (CAIR). Large reductions have occurred near many urban areas where local control programs have been implemented in addition to the regional controls. In the western U.S., where control programs have been more localized, the reductions have occurred mostly in California and near large urban areas. In other areas most sites have not shown a significant trend, and there are only a handful of sites have shown an increasing trend.

Figure A-6. Map of site-level O_3 trends across the U.S. from 2000 to 2015



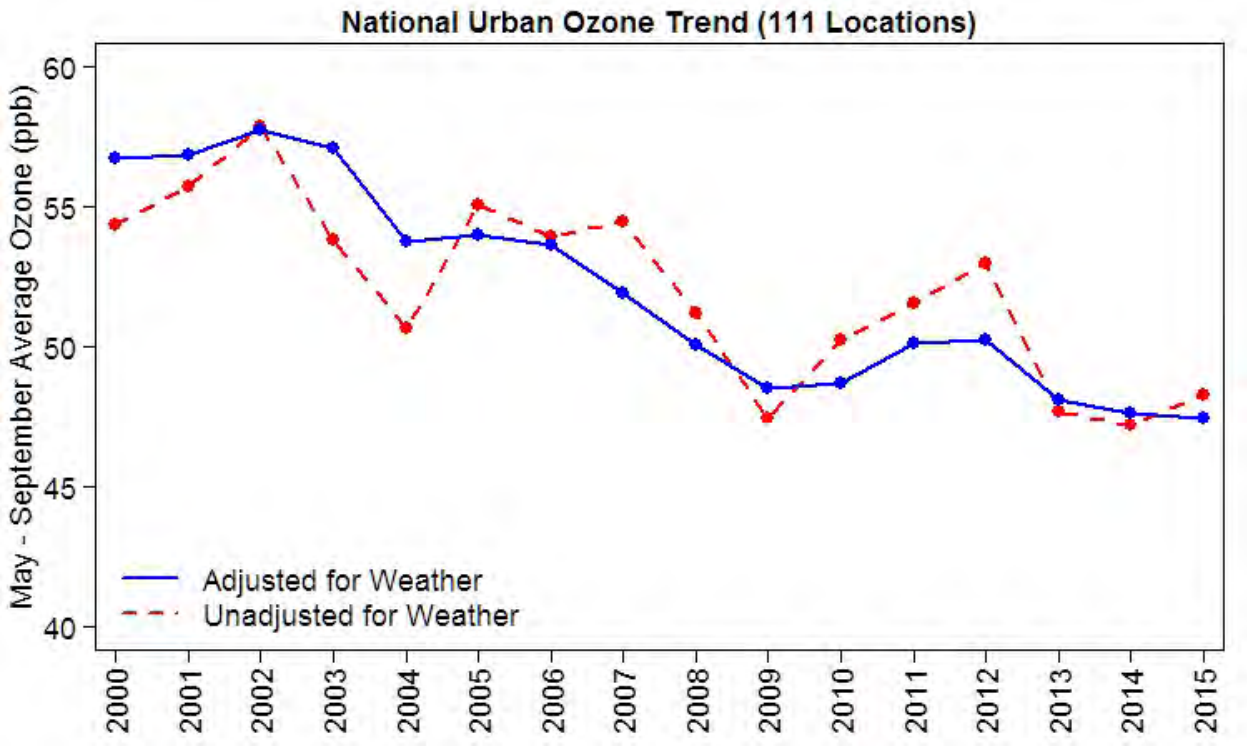
Variations in meteorological conditions play an important role in determining O_3 concentrations. Ozone is more readily formed on warm, sunny days when the air is stagnant. Conversely, O_3 generation is more limited when it is cool, rainy, cloudy, or windy. EPA uses a statistical model to adjust for the variability in seasonal average O_3 concentrations due to weather conditions to provide a more accurate assessment of the underlying trend in O_3 caused by emissions.[54] Figure A-7 shows the national trend in the May to September mean of the daily

[54] Louise Camalier, William Cox, and Pat Dolwick (2007). The Effects of Meteorology on Ozone in Urban Areas and their use in Assessing Ozone Trends. Atmospheric Environment, Volume 41, Issue 33, October 2007, pages 7127-7137.

maximum 8-hour O_3 concentrations from 2000 to 2015 in 111 urban locations. The dotted red line shows the trend in observed O_3 concentrations at selected monitoring sites, while the solid blue line shows the underlying O_3 trend at those sites after removing the effects of weather. The solid blue lines represent O_3 levels anticipated under "typical" weather conditions and serve as a more accurate assessment of the trend in O_3 due to changes in precursor emissions.

Figure A-7 shows that after adjusting for the year-to-year variability in meteorology, the overall trend in seasonal average O_3 concentrations is much smoother. The adjusted trend clearly shows that the NO_X SIP Call program resulted in a sharp decrease in summertime O_3 concentrations starting in 2004. The adjusted trend also indicates that O_3 levels decreased between 2004 and 2009, followed by a small increase from 2009 to 2012, then continued to decrease after 2012.

Figure A-7. Trend in the May to September mean of the daily maximum 8-hour O_3 concentration before (dotted red line) and after (solid blue line) adjusting for year-to-year variability in meteorology.



Conceptual Description of $PM_{2.5}$

1. $PM_{2.5}$ Monitoring Networks

1.1. PM Mass Networks

The 1997 promulgation of a fine particulate NAAQS led to deployment of over 1,500 $PM_{2.5}$ sites (about 1,000 currently in operation) used to determine whether an area complies with the standard. These sites use a Federal Reference Method (FRM) or Federal Equivalent Method (FEM), daily sampling over 24-hours, or every third or sixth day. Nearly 200 additional measurements not meeting FRM or FEM specifications are provided by the chemical speciation sites (Figure A-8). Approximately 450 stations provide indirect measurements of continuous FEM (hourly resolution) $PM_{2.5}$ mass.

1.2. Interagency Monitoring of Protected Visual Environments (IMPROVE) Program

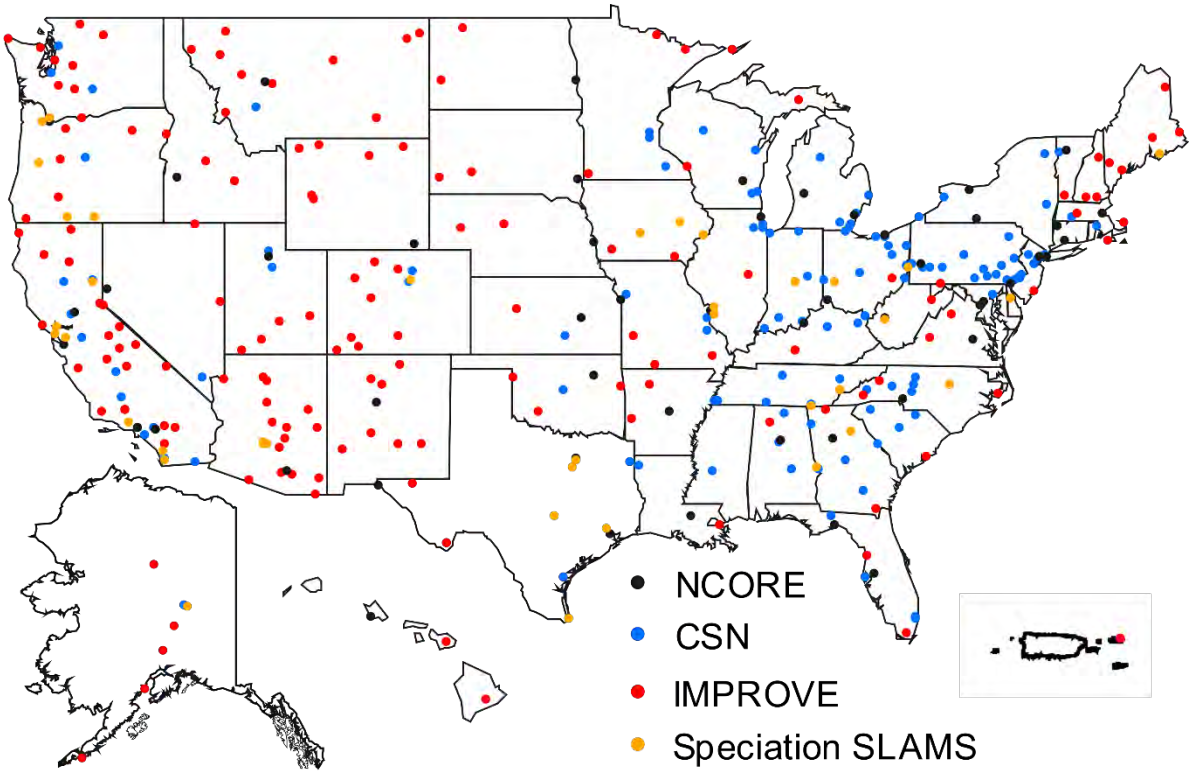
The IMPROVE network, with over 150 sites, has provided nearly a 20+ year record of major components of $PM_{2.5}$ (sulfate, nitrate, organic and elemental carbon fractions, and trace metals) in pristine areas of the United States (Figure A-8). IMPROVE is led by the National Park Service; various federal and state agencies support its operations. The primary focus of the network is to track visibility and trends in visibility.

1.3. $PM_{2.5}$ Chemical Speciation Monitoring

In addition to the IMPROVE network, approximately 200 EPA speciation sites operate in urban areas of the United States to assist $PM_{2.5}$ assessment efforts. No FRM exists for particulate speciation, which is not directly required to determine attainment, and there are slight differences between monitors and methods used in the Chemical Speciation Network (CSN). However, the network's coverage (Figure A-8) across urban and rural areas has proved essential for a wide range of research and analysis. The speciation networks typically collect a 24-hour sample every three, and sometimes six, days.

Only a handful of sites provide near continuous speciation data, usually limited to some combination of sulfate, carbon (organic and elemental splits) and nitrate. This enables insight to diurnal patterns for diagnosing various cause-effect phenomena related to emissions characterization, source attribution analysis and model evaluation.

Figure A-8. Locations of chemical speciation sites delineated by program type



2. Composition of $PM_{2.5}$

Particulate matter (PM) is a highly complex mixture of solid particles and liquid droplets distributed among numerous atmospheric gases which interact with solid and liquid phases. Particles range in size from those smaller than 1 nanometer (10^{-9} meter) to over 100 microns (1 micron is 10^{-6} meter) in diameter (for reference, a typical strand of human hair is 70 microns and particles less than about 20 microns generally are not detectable by the human eye). Particles are classified as $PM_{2.5}$ and $PM_{10-2.5}$, corresponding to their size (diameter) range in microns and referring to total particle mass under 2.5 and between 2.5 and 10 microns, respectively.

Particles span many sizes and shapes and consist of hundreds of different chemicals. Particles are emitted directly from sources and also are formed through atmospheric chemical reactions and often are referred to as primary and secondary particles, respectively. Particle pollution also varies by time of year and location and is affected by several aspects of weather such as temperature, clouds, humidity, and wind. Further complicating particles is the shifting between solid/liquid and gaseous phases influenced by concentration and meteorology, especially temperature.

Particles are made up of different chemical components. The major components, or species, are carbon, sulfate and nitrate compounds, and crustal materials such as soil and ash (Figure A-9). The different components that make up particle pollution come from specific sources and are often formed in the atmosphere. Particulate matter includes both "primary" PM, which is directly emitted into the air, and "secondary" PM, which forms indirectly from fuel

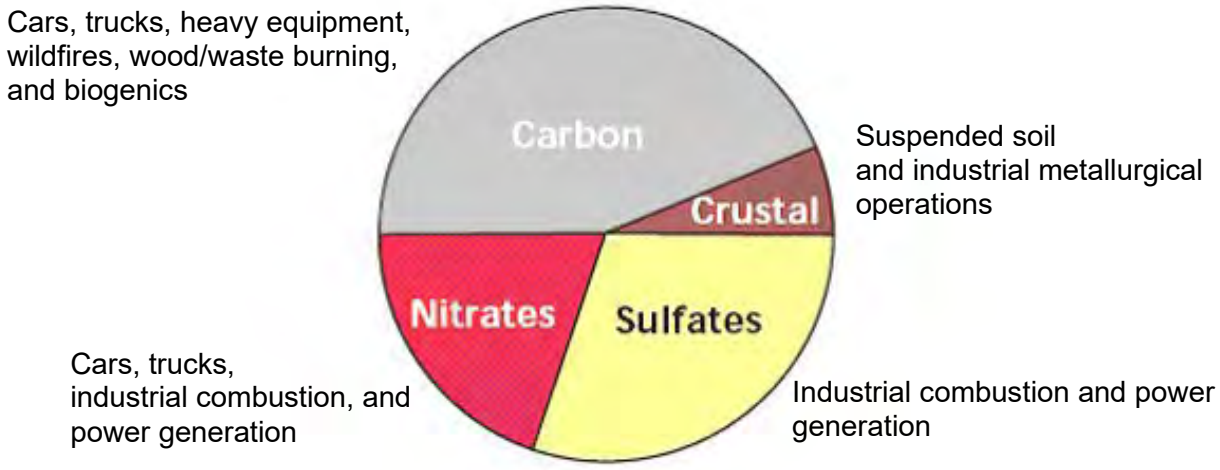
combustion and other sources. Primary PM consists of carbon (soot) emitted from cars, trucks, heavy equipment, forest fires, and burning waste and crustal material from unpaved roads, stone crushing, construction sites, and metallurgical operations. Secondary PM forms in the atmosphere from gases. Some of these reactions require sunlight and/or water vapor. Secondary PM includes:

- Sulfates formed from sulfur dioxide emissions from power plants and industrial facilities;
- Nitrates formed from nitrogen oxide emissions from cars, trucks, industrial facilities, and power plants; and
- Carbon formed from reactive organic gas emissions from cars, trucks, industrial facilities, forest fires, and biogenic sources such as trees.

In addition, ammonia from sources such as fertilizer and animal feed operations is part of the formation of sulfates and nitrates that exist in the atmosphere as ammonium sulfate and ammonium nitrate. Note that fine particles can be transported long distances by wind and weather and can be found in the air thousands of miles from where they were formed.

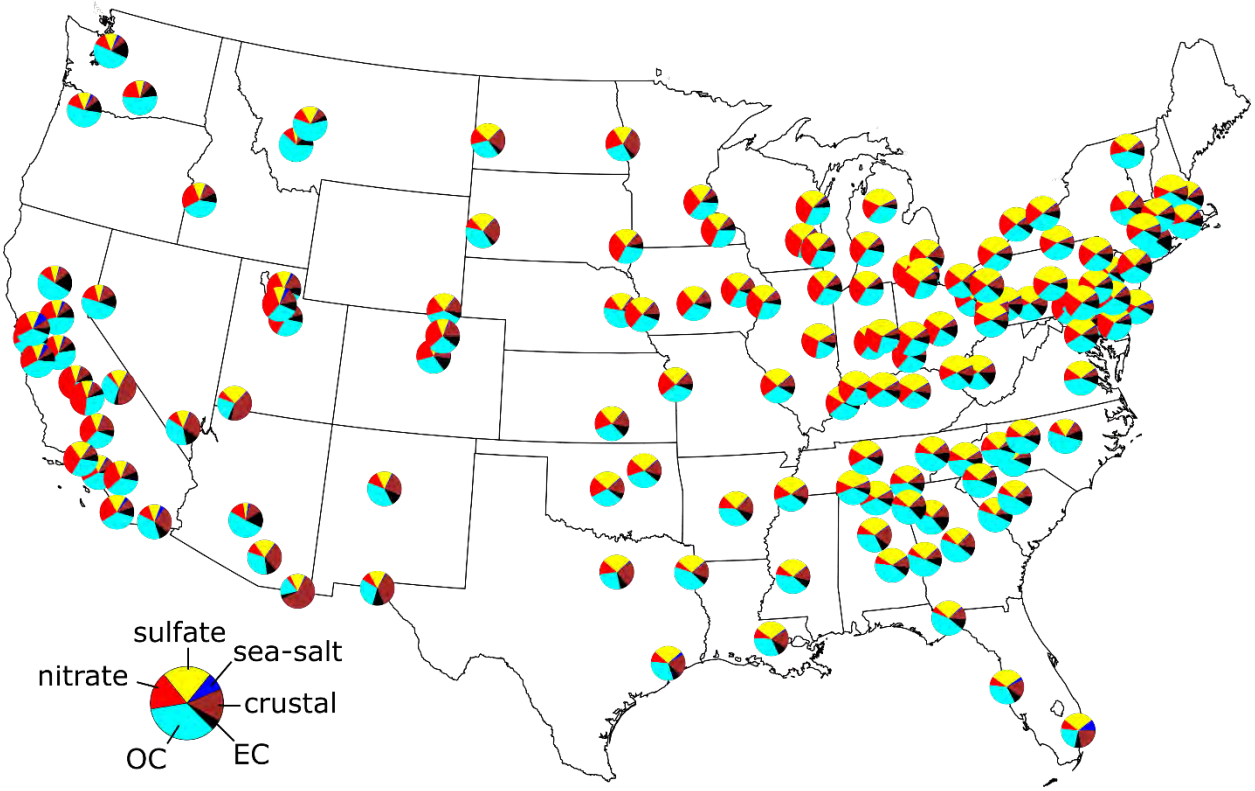
The chemical makeup of particles varies across the United States (as shown in Figure A-10). For example, fine particles in the eastern half of the United States contain more sulfates than those in the West, while fine particles in southern California contain more nitrates than other areas of the country. Organic carbon is a substantial component of fine particle mass everywhere.

Figure A-9. National Average of Source Impacts on Fine Particle Levels



Source: The Particulate Matter Report, EPA-454/R-04-002, Fall 2004. Carbon reflects both organic carbon and elemental carbon. Organic carbon accounts for automobiles, biogenics, gas-powered off-road, and wildfires. Elemental carbon is mainly from diesel powered sources.

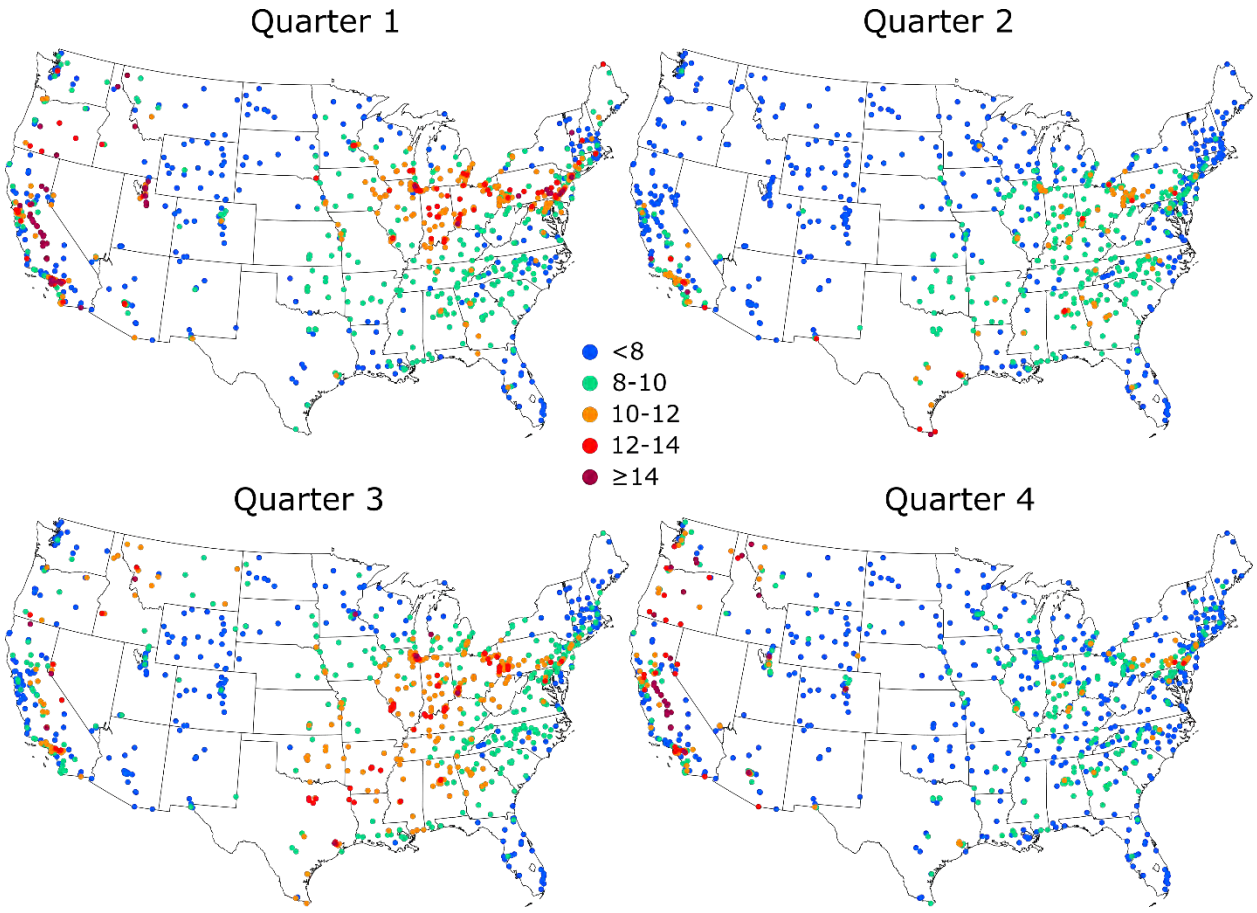
Figure A-10. Annual Average $PM_{2.5}$ Composition grouped by CBSA: 2013-2015



3. Seasonal and Daily Patterns of $PM_{2.5}$

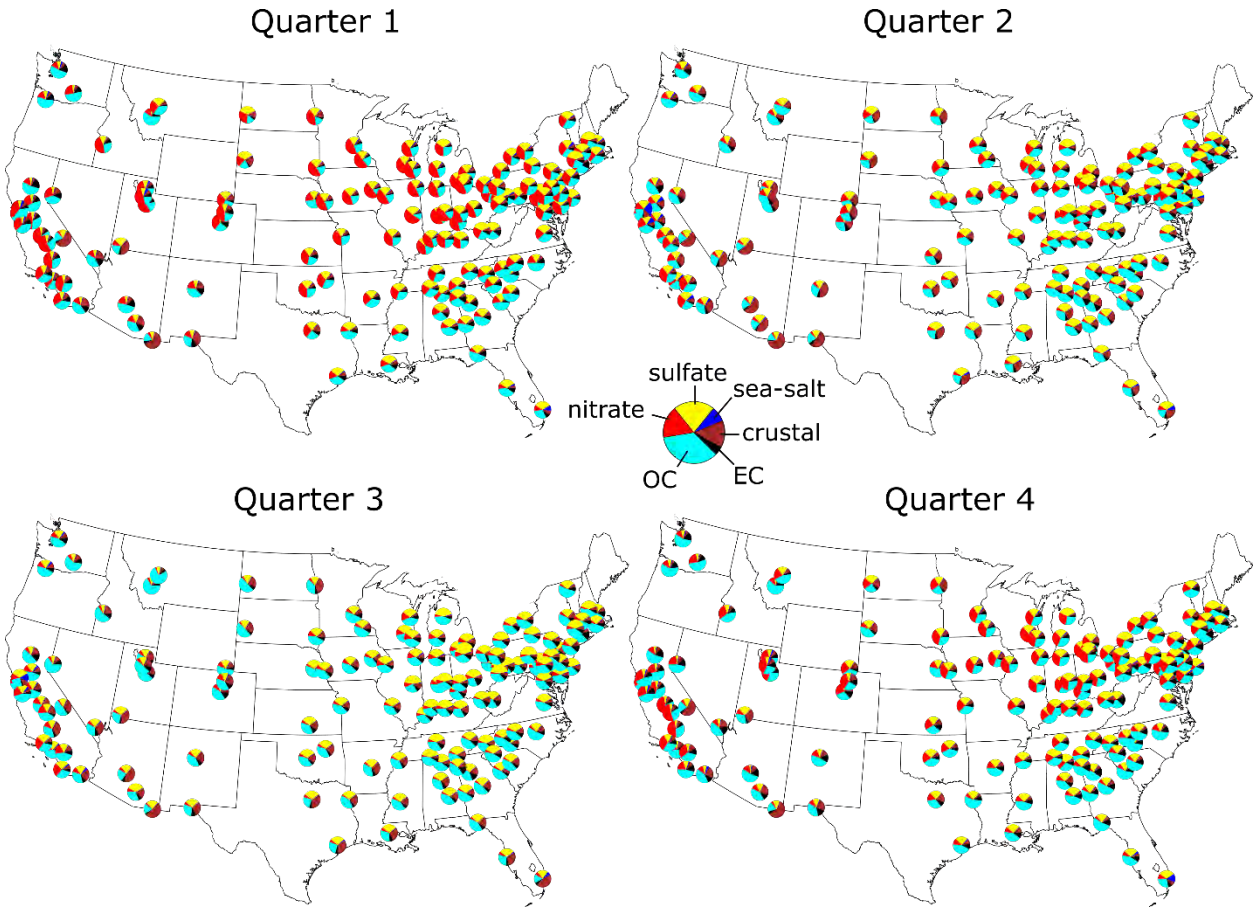
Fine particles often have a seasonal pattern. Both daily values and quarterly average of $PM_{2.5}$ also reveal patterns based on the time of year. Unlike daily O_3 levels, which are usually elevated in the summer, daily $PM_{2.5}$ values at some locations can be high at any time of the year. As shown in Figure A-11, $PM_{2.5}$ values in the eastern half of the United States are typically higher in the third calendar quarter (July-September) when sulfates are more readily formed from sulfur dioxide (SO_2) emissions from power plants in that region and when secondary organic aerosol is more readily formed in the atmosphere. Fine particle concentrations tend to be higher in the first calendar quarter (January through March) in the Midwest in part because fine particle nitrates are more readily formed in cooler weather. $PM_{2.5}$ values are high during the first (January through March) and fourth calendar quarter (October through December) in many areas of the West, in part because of fine particle nitrates and also due to carbonaceous particles which are directly emitted from wood stove and fireplace use. Average concentration from all locations reporting $PM_{2.5}$ with valid design values is shown.

Figure A-11. Quarterly Averages of $PM_{2.5}$ Concentration (µg m^{-3}): 2013-2015



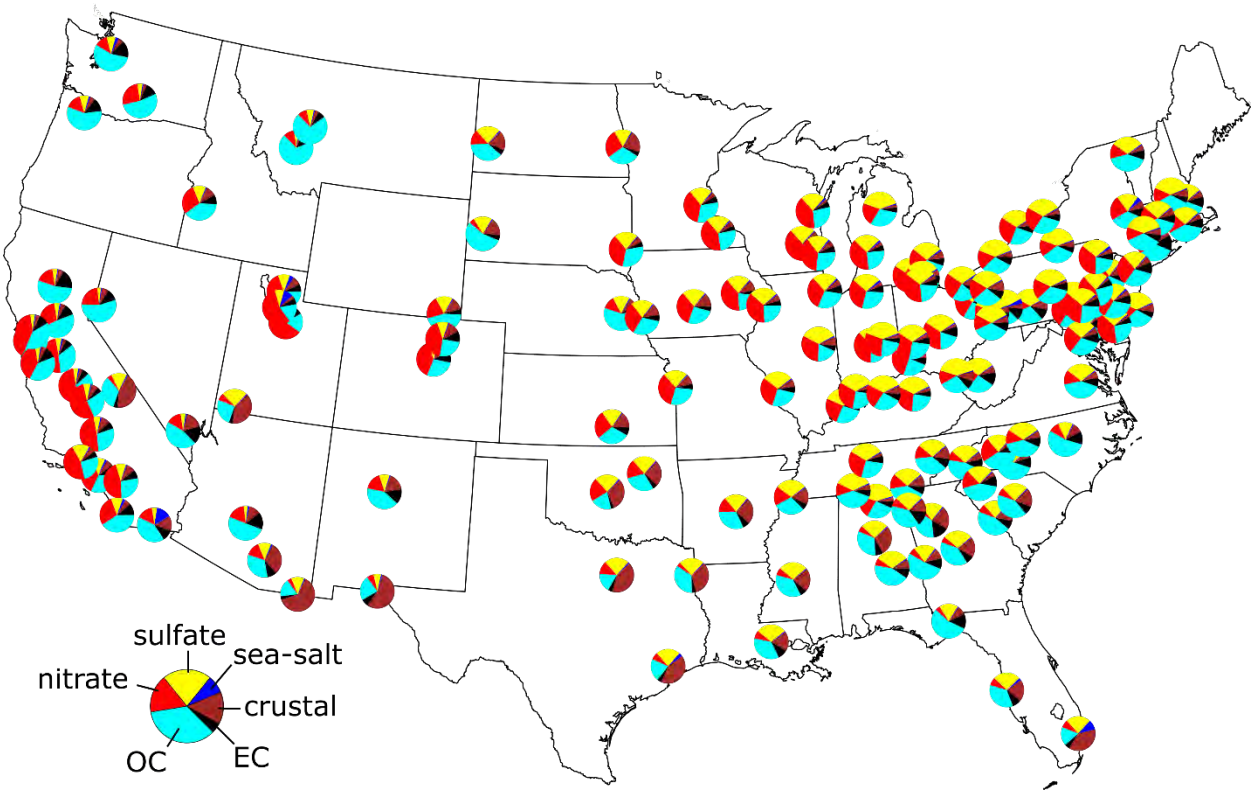
The composition of $PM_{2.5}$ also varies by season and helps explain why mass varies by season. Figure A-12 shows the average composition by season (spring, summer, fall and winter) for $PM_{2.5}$ data collected during 2013-2015. In the eastern United States, sulfate are high in the spring (March-May) and summer (July-September). Nitrates are most evident in the midwest and western cities where its percentage is moderately high in the winter and fall. Organic carbon (OC) is high throughout the year.

Figure A-12. Quarterly Average $PM_{2.5}$ Composition grouped by CBSA: 2013-2015



The composition of the highest daily $PM_{2.5}$ values may be different than that for the annual average. Figure A-13 provides 2013-2015 data $PM_{2.5}$ composition on high mass days across the United States. Mass is proportioned into six components: sulfates, nitrates, OC, elemental carbon (EC), crustal material, and sea-salt. Except for the southeast (where there is little nitrate in $PM_{2.5}$), nitrates are slightly higher in the top 10 percent of the $PM_{2.5}$ days. For the 2013-2015 measurements, the percent of sulfates is currently similar or slightly less on the top 10 percent of the days as compared to the annual averages. The portion of OC appears to be similar on the high days compared to the annual averages, except for the Northern Rockies and Upper Midwest where the high days are influenced by OC from wood stoves/fireplaces and wildfires.

Figure A-13. $PM_{2.5}$ Composition on 10% highest mass concentration days grouped by CBSA: 2013-2015



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Appendix B: General Guidance on Use of Dispersion Models for Estimating Primary $PM_{2.5}$ Concentrations

This appendix provides general guidance on the application of dispersion models for estimating ambient concentrations of $PM_{2.5}$ associated with direct emissions of primary $PM_{2.5}$. This guidance is based on and is consistent with the EPA's *Guideline on Air Quality Models*, published as Appendix W of 40 CFR part 51, and focuses primarily on the application of AERMOD, the EPA's preferred dispersion model for most situations. Appendix W is the primary source of information on the regulatory application of air quality models for State Implementation Plan (SIP) revisions for existing sources and for New Source Review (NSR) and Prevention of Significant Deterioration (PSD) programs. There will be applications of dispersion models unique to specific areas, (*i.e.*, there may be areas of the country where it is necessary to model unique specific sources or types of sources). In such cases, there should be consultation with the state or appropriate permitting authority with the appropriate EPA Regional Office modeling contact to discuss how best to model a particular source.

Recently issued EPA guidance of relevance for consideration in modeling for $PM_{2.5}$ includes:

- "Model Clearinghouse Review of Modeling Procedures for Demonstrating Compliance with $PM_{2.5}$ NAAQS" February 26, 2010 (U.S. EPA, 2010a);
- "Modeling Procedures for Demonstrating Compliance with $PM_{2.5}$ NAAQS" March 23, 2010 (U.S. EPA, 2010b); and
- "Transportation Conformity Guidance for Quantitative Hot-spot Analyses in $PM_{2.5}$ and PM_{10} Nonattainment and Maintenance Areas" November 2015 (U.S. EPA, 2015a).

The guidance listed above, in addition to other relevant support documents can be found on the SCRAM website at: https://www.epa.gov/scram.

The following sections will refer to the relevant sections of Appendix W and other existing guidance with summaries as necessary. Please refer to those original guidance documents for full discussion and consult with the appropriate EPA Regional Office modeling contact if questions arise about interpretation on modeling techniques and procedures.[55]

1. Model selection

Preferred air quality models for use in regulatory applications are addressed in Appendix A of the EPA's *Guideline on Air Quality Models*. If a model is to be used for a particular application, the user should follow the guidance on the preferred model for that application. These models may be used without an area specific formal demonstration of applicability as long as they are used as indicated in each model summary of Appendix A. Further recommendations for the application of these models to specific source problems are found in Appendix W. In

[55] A list of EPA Regional Office modeling contacts is available on the SCRAM website at: https://www.epa.gov/scram/air-modeling-regional-contacts.

2005, the EPA promulgated the American Meteorological Society/Environmental Protection Agency Regulatory Model (AERMOD) as the Agency's preferred near-field dispersion model for a wide range of regulatory applications in all types of terrain based on extensive developmental and performance evaluation. For PSD/NSR modeling under the $PM_{2.5}$ NAAQS, AERMOD should be used to model direct $PM_{2.5}$ emissions unless use of an alternative model can be justified (section 3.2, Appendix W).

The AERMOD modeling system includes the following components:

- AERMOD: the dispersion model (U.S. EPA, 2022a);
- AERMAP: the terrain processor for AERMOD (U.S. EPA, 2018a,); and
- AERMET: the meteorological data processor for AERMOD (U.S. EPA, 2022b;).

Other components that may be used, depending on the application, are:

- BPIPPRIME: the building input processor (U.S. EPA, 2004);
- AERSURFACE: the surface characteristics processor for AERMET (U.S. EPA, 2020);
- AERSCREEN: a screening version of AERMOD (U.S. EPA, 2021; U.S. EPA, 2011); and
- AERMINUTE: a pre-processor to calculate hourly average winds from Automated Surface Observing System (ASOS) 2-minute observations (U.S. EPA, 2015b).

Before running AERMOD, the user should become familiar with the user's guides associated with the modeling components listed above and the AERMOD Implementation Guide (AIG) (U.S. EPA, 2022c). The AIG lists several recommendations for applications of AERMOD that would be applicable for SIP and PSD permit modeling.

1.2. Receptor grid

The model receptor grid is unique to the particular situation and depends on the size of the modeling domain, the number of modeled sources, and complexity of the terrain. Receptors should be placed in areas that are considered ambient air (*i.e.*, outside of buildings and where the public generally has access) and placed out to a distance such that areas of violation can be detected from the model output to help determine the size of nonattainment areas. Receptor placement should be of sufficient density to provide resolution needed to detect significant gradients in the concentrations with receptors placed closer together near the source to detect local gradients and placed farther apart away from the source. In addition, the user may want to place receptors at key locations such as around facility "fence lines"[56] (which define the ambient air boundary for a particular source) or monitor locations (for comparison to monitored concentrations for model evaluation purposes). The receptor network should cover the modeling

[56] It should be noted that the term "fence line" for modeling purposes generally makes reference to a source's property boundary and may not refer literally to the existence of a fence at such boundary. The EPA's "ambient air" policy does not mandate that public access to a source's property be precluded by a fence; other measures that effectively preclude public access may be approved for establishing an ambient air exclusion for PSD modeling purposes.

domain. States may already have existing receptor placement strategies in place for regulatory dispersion modeling under NSR/PSD permit programs.

If modeling indicates elevated levels of $PM_{2.5}$ (near the standard) near the edge of the receptor grid, consideration should be given to expanding the grid or conducting an additional modeling run centered on the area of concern. As noted above, terrain complexity should also be considered when setting up the receptor grid. If complex terrain is included in the model calculations, AERMOD requires that receptor elevations be included in the model inputs. In those cases, the AERMAP terrain processor (U.S. EPA, 2018a) should be used to generate the receptor elevations and hill heights. The latest version of AERMAP (version 09040 or later) can process either Digitized Elevation Model (DEM) or National Elevation Data (NED) data files. The AIG recommends the use of NED data since it is more up to date than DEM data, which is no longer updated (Section 4.3 of the AIG).

2. Source inputs

This section provides guidance on source characterization to develop appropriate inputs for dispersion modeling with the AERMOD modeling system. Section 2.1 provides guidance on use of emission, Section 2.2 covers guidance on Good Engineering Practice (GEP) stack heights, Section 2.3 provides details on source configuration and source types, Section 2.4 provides details on urban/rural determination of the sources, and Section 2.5 provides general guidance on source grouping, which may be important for design value calculations.

2.1. Emissions

Consistent with Appendix W, dispersion modeling for the purposes of PSD permitting should be based on the use of continuous operation at maximum allowable emissions or federally enforceable permit limits (see Table 8-2 of Appendix W) for the project source for all applicable averaging periods. Also consistent with past and current guidance, in the absence of maximum allowable emissions or federally enforceable permit limits, potential to emit emissions (*i.e.*, design capacity) should be used. Maximum allowable emissions and continuous operation should also be assumed for nearby sources included in the modeled inventory for the 24-hr $PM_{2.5}$ NAAQS, while maximum allowable emissions and the actual operating factor averaged over the most recent 2 years, unless it is determined that this period is not representative, should be used for modeled nearby sources for the annual $PM_{2.5}$ NAAQS.

2.2. Good Engineering Practice (GEP) stack height

Consistent with previous modeling guidance and section 7.2.2.1 of Appendix W, for stacks with heights that are within the limits of Good Engineering Practice (GEP), actual heights should be used in modeling. Under the EPA's regulations at 40 CFR 51.100, GEP height, H_g, is determined to be the greater of:

- 65 m, measured from the ground-level elevation at the base of the stack;
- for stacks in existence on January 12, 1979, and for which the owner or operator had obtained all applicable permits or approvals required under 40 CFR parts 51 and 52

H_g=2.5H

provided the owner or operator produces evidence that this equation was actually relied on in designing the stack or establishing an emission limitation to ensure protection against downwash;

- for all other stacks,

H_g=H + 1.5L,

where H is the height of the nearby structure(s) measured from the ground-level elevation at the base of the stack and L is the lesser dimension of height or projected width of nearby structure(s); or

- the height demonstrated by a fluid model or a field study approved by the EPA or the state/local permitting agency which ensures that the emissions from a stack do not result in excessive concentrations of any air pollutant as a result of atmospheric downwash, wakes, eddy effects created by the source itself, nearby structures or nearby terrain features.

For more details about GEP, see the Guideline for Determination of Good Engineering Practice Stack Height Technical Support Document (U.S. EPA, 1985).

If stack heights exceed GEP, then GEP heights should be used with the individual stack's other parameters (temperature, diameter, exit velocity). For stacks modeled with actual heights below GEP that may be subject to building downwash influences, building downwash should be considered as this can impact concentrations near the source (section 7.2.2.1(b), Appendix W). If building downwash is being considered, the BPIPPRIME program (U.S. EPA, 2004) should be used to input building parameters for AERMOD.

2.3. Source configurations and source types

An accurate characterization of the modeled facilities is critical for refined dispersion modeling, including accurate stack parameters and physical plant layout. Accurate stack parameters should be determined for the emissions being modeled. Since modeling would be done with maximum allowable or potential emissions levels at each stack, the stack's parameters such as exit temperature, diameter, and exit velocity should reflect those emissions levels. Accurate locations (*i.e.*, latitude and longitude or Universal Transverse Mercator (UTM) coordinates and datum)[57] of the modeled emission sources are also important, as this can affect the impact of an emission source on receptors, determination of stack base elevation, and relative location to any nearby building structures. Not only are accurate stack locations needed, but accurate information for any nearby buildings is important. This information would include

[57] Latitudes and longitudes to four decimal places position a stack within 30 feet of its actual location and five decimal places position a stack within three feet of its actual location. Users should use the greatest precision available.

location and orientation relative to stacks and building size parameters (height, and corner coordinates of tiers) as these parameters are input into BPIPPRIME to calculate building parameters for AERMOD. If stack locations and or building information are not accurate, downwash will not be accurately accounted for in AERMOD.

Emission source type characterization within the modeling environment is also important. As stated in the AERMOD User's Guide (U.S. EPA, 2019a), emissions sources can be characterized as several different source types: POINT sources, capped stacks (POINTCAP), horizontal stacks (POINTHOR), VOLUME sources, OPENPIT sources, LINE sources, buoyant lines sources (BUOYLINE), rectangular AREA sources, circular area sources (AREACIRC), and irregularly shaped area sources (AREAPOLY). While most sources can be characterized as POINT sources, some sources, such as fugitive releases or nonpoint sources (emissions from ports/ships, airports, or smaller point sources with no accurate locations), may be best characterized as VOLUME or AREA type sources. Sources such as flares can be modeled in AERMOD using the parameter input methodology described in Section 2.1.2 of the AERSCREEN User's Guide (U.S. EPA, 2021). If questions arise about proper source characterization or typing, users should consult the appropriate EPA Regional Office modeling contact.

2.4. Urban/rural determination

For any dispersion modeling exercise, the urban or rural determination of a source is important in determining the boundary layer characteristics that affect the model's prediction of downwind concentrations. Figure B-1 gives example maximum 24-hour concentration profiles for a 10 meter stack (Figure B-1a) and a 100 m stack (Figure B-1b) based on urban vs. rural designation. The urban population used for the examples is 100,000. In Figure B-1a, the urban concentration is much higher than the rural concentration for distances less than 750 m from the stack but then drops below the rural concentration beyond 750 m. For the taller stack in Figure B-1b, the urban concentration is much higher than the rural concentration even as distances increase from the source. These profiles show that the urban or rural designation of a source can be quite important.

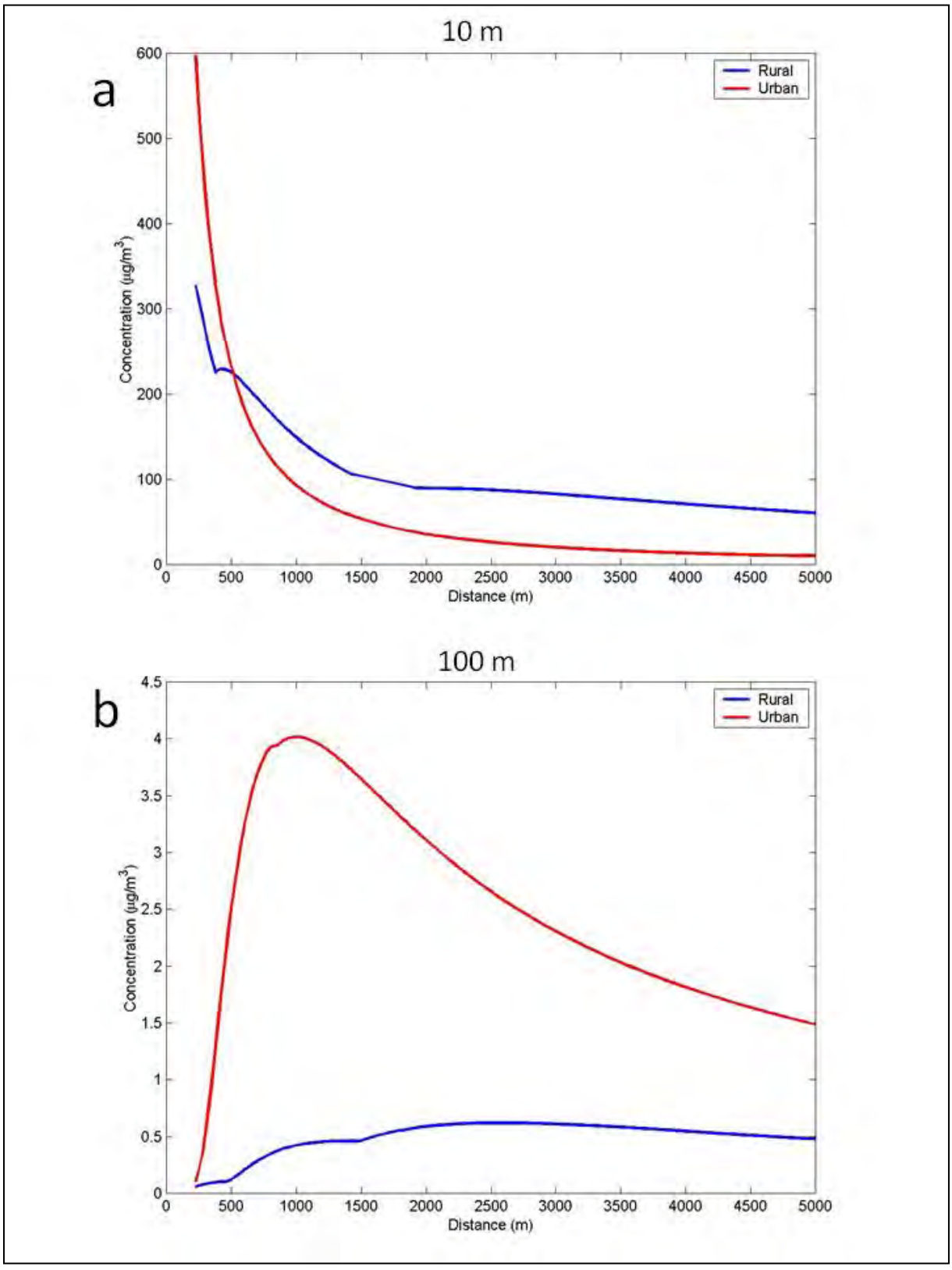
Determining whether a source is urban or rural can be done using the methodology outlined in section 7.2.1.1 of Appendix W and recommendations outlined in Sections 5.1 through 5.3 in the AIG (U.S. EPA, 2022c). In summary, there are two methods of urban/rural classification described in section 7.2.3 of Appendix W.

The first method of urban determination is a land use method (Appendix W, section 7.2.2.1.1(b)(i)). In the land use method, the user analyzes the land use within a 3 km radius of the source using the meteorological land use scheme described by Auer (1978). Using this methodology, a source is considered urban if the land use types I1 (heavy industrial), I2 (light-moderate industrial), C1 (commercial), R2 (common residential), and R3 (compact residential) are 50 percent or more of the area within the 3 km radius circle. Otherwise, the source is considered a rural source. The second method uses population density and is described in section 7.2.2.1.1(b)(ii) of Appendix W. As with the land use method, a circle of 3 km radius is used. If the population density within the circle is greater than 750 people/km^2, then the source is

considered urban. Otherwise, the source is modeled as a rural source. Of the two methods, the land use method is considered more definitive (section 7.2.1.1.b, Appendix W).

Caution should be exercised with either classification method. As stated in Section 5.1 of the AIG (U.S. EPA, 2009), when using the land use method, a source may be in an urban area but located close enough to a body of water or other non-urban land use category to result in an erroneous rural classification for the source. The AIG in Section 5.1 cautions users against using the land use scheme on a source by source basis, but advises considering the potential for urban heat island influences across the full modeling domain. When using the population density method, section 7.2.2.1.1(b)(ii)of Appendix W states, "Population density should be used with caution and should not be applied to highly industrialized areas where the population density may be low and thus a rural classification would be indicated, but the area is sufficiently built-up so that the urban land use criteria would be satisfied..." With either method, section 7.2.1.1(f) of Appendix W recommends modeling all sources within an urban complex as urban, even if some sources within the complex would be considered rural using either the land use or population density method.

Figure B-1. Urban (red) and rural (blue) concentration profiles for (a) 10 m buoyant stack release, and (b) 100 m buoyant stack release



Another consideration that may need attention by the user, and is discussed in Section 5.1 of the AIG, relates to tall stacks located within or adjacent to small to moderate size urban areas. In such cases, the stack height or effective plume height for very buoyant sources may extend above the urban boundary layer height. The application of the urban option in AERMOD for these types of sources may artificially limit the plume height. The use of the urban option may not be appropriate for these sources, since the actual plume is likely to be transported over the urban boundary layer. Section 5.1 of the AIG gives details on determining if a tall stack should be modeled as urban or rural based on comparing the stack or effective plume height to the urban boundary layer height. The 100 m stack illustrated in Figure B-1b, may be such an example as the urban boundary layer height for this stack would be 189 m (based on a population of 100,000) and equation 104 of the AERMOD formulation document (Cimorelli, et al., 2004). This equation is:

$$z_{iuc} = z_{iuo}\left(\frac{P}{P_o}\right)^{1/4} \tag{B-1}$$

where z_{iuo} is a reference height of 400 m corresponding to a reference population P_o of 2,000,000 people.

Given that the stack is a buoyant release, the plume may extend above the urban boundary layer and may be best characterized as a rural source, even if it were near an urban complex. However, beginning with version 15181 of AERMOD, a formulation bug fix was incorporated that modified the treatment of plume rise for urban sources, especially for tall stacks in urban areas. See Section 5.1 of the AIG for more information. Even with the bug fix in AERMOD 15181, exclusion of these elevated sources from application of the urban option would need to be justified on a case-by-case basis in consultation with the appropriate permitting authority.

AERMOD requires the input of urban population when utilizing the urban option. Population can be entered to one or two significant digits (*i.e.*, an urban population of 1,674,365 can be entered as 1,700,000). Users can enter multiple urban areas and populations using the URBANOPT keyword in the runstream file (U.S. EPA, 2022a). If multiple urban areas are entered, AERMOD requires that each urban source be associated with a particular urban area or AERMOD model calculations will abort. Urban populations can be determined by using a method described in Section 5.2 of the AIG (U.S. EPA, 2022c).

2.5. Source groups

In AERMOD, individual emission sources' concentration results can be combined into groups using the SRCGROUP keyword (Section 3.3.11 of the AERMOD User's Guide (U.S, EPA, 2019a). The user can automatically calculate a total concentration (from all sources) using the SRCGROUP ALL keyword. For the purposes of design value calculations, source group ALL should be used, especially if all sources in the modeling domain are modeled in one AERMOD run. Design values should be calculated from the total concentrations (all sources and background). Individual source impacts on the total concentration may be necessary to determine the culpability to any NAAQS violations.

3. Meteorological data

This section gives guidance on the selection of meteorological data for input into AERMOD. Much of the guidance from section 8.4 of Appendix W is applicable to SIP and PSD permit modeling and is summarized here. In Section 3.2.1, the use of the tool, AERMINUTE (U.S. EPA, 2015b), is introduced. AERMINUTE is an AERMET pre-processor that calculates hourly averaged winds from ASOS 1-minute winds. Section 3.2.4 discusses the use of prognostic meteorological data.

3.1. Surface characteristics and representativeness

The selection of meteorological data that are input into a dispersion model should be considered carefully. The selection of data should be based on spatial and climatological (temporal) representativeness (Appendix W, section 8.4). The representativeness of the data is based on: 1) the proximity of the meteorological monitoring site to the area under consideration, 2) the complexity of terrain, 3) the exposure of the meteorological site, and 4) the period of time during which data are collected. Sources of meteorological data are: National Weather Service (NWS) stations, site-specific or onsite data, and other sources such as universities, Federal Aviation Administration (FAA), military stations, and others. In specific cases, prognostic meteorological data may be appropriate for use and obtained from similar sources. Appendix W addresses spatial representativeness issues in sections 8.4.1.a and 8.4.2.b.

Spatial representativeness of the meteorological data can be adversely affected by large distances between the source and receptors of interest and the complex topographic characteristics of the area (Appendix W, sections 8.4.1.a and 8.4.2.b). If the modeling domain is large enough such that conditions vary drastically across the domain, then the selection of a single station to represent the domain should be carefully considered. Also, care should be taken when selecting a station if the area has complex terrain. While a source and meteorological station may be in close proximity, there may be complex terrain between them such that conditions at the meteorological station may not be representative of the source. An example would be a source located on the windward side of a mountain chain with a meteorological station a few kilometers away on the leeward side of the mountain. Spatial representativeness for off-site data should also be assessed by comparing the surface characteristics (albedo, Bowen ratio, and surface roughness) of the meteorological monitoring site and the analysis area. When processing meteorological data in AERMET (U.S. EPA, 2022b), the surface characteristics of the meteorological site or the prognostic meteorological model output grid cell should be used (section 8.4.2.b of Appendix W and the AERSURFACE User's Guide (U.S. EPA, 2020)). Spatial representativeness should also be addressed for each meteorological variable separately. For example, temperature data from a meteorological station several kilometers from the analysis area may be considered adequately representative, while it may be necessary to collect wind data near the plume height (section 8.4.2.b of Appendix W).

Surface characteristics can be calculated in several ways. For details, see Section 3.1.2 of the AIG (U.S. EPA, 2022c). The EPA has developed a tool, AERSURFACE (U.S. EPA, 2020) to aid in the determination of surface characteristics for observed meteorological data. Note that the use of AERSURFACE is not a regulatory requirement, but the methodology outlined in

Section 3.1.2 of the AIG should be followed unless an alternative method can be justified. For prognostic meteorological output, the surface characteristics of the representative grid cell should be used.

3.2. Meteorological inputs

Appendix W states in section 8.4.2.e that the user should acquire enough meteorological data to ensure that worst-case conditions are adequately represented in the model results. Appendix W states that 5 years of NWS meteorological data, at least 1 year of site-specific data, or at least 3 years of prognostic data should be used and should be adequately representative of the study area. If 1 or more years of site-specific data are available, those data are preferred. While the form of the $PM_{2.5}$ NAAQS contemplates obtaining 3 years of monitoring data, this does not preempt the use of 5 years of NWS data or at least 1 year of site-specific data in the modeling. The 5-year average based on the use of NWS data, an average across 3 or more years of prognostic data, or an average across 1 or more years of available site specific data, serves as an unbiased estimate of the 3-year average for purposes of modeling demonstrations of compliance with the NAAQS.

3.2.1. NWS data

NWS data are available from the National Climatic Data Center (NCDC) in many formats, with the most common one in recent years being the Integrated Surface Hourly data (ISH). Most available formats can be processed by AERMET. As stated in Section 3.1, when using data from an NWS station alone or in conjunction with site-specific data, the data should be spatially and temporally representative of conditions at the modeled sources. Key points regarding the use of NWS data can be found in the EPA's March 8, 2013 clarification memo "Use of ASOS meteorological data in AERMOD dispersion modeling" (U.S. EPA, 2013). The key points are:

- The EPA has previously analyzed the effects of ASOS implementation on dispersion modeling and found that generally AERMOD was less sensitive than ISCST3 to the implementation of ASOS.
- The implementation of the ASOS system over the conventional observation system should not preclude the consideration of NWS stations in dispersion modeling.
- The EPA has implemented an adjustment factor (0.5 knots) in AERMET to adjust for wind speed truncation in ASOS winds
- The EPA has developed the AERMINUTE processor (U.S. EPA, 2015b) to process 2-minute ASOS winds and calculate an hourly average for input into AERMET. The use of hourly averaged winds better reflect actual conditions over the hour as opposed to a single 2-minute observation.

3.2.2. Site-specific data

The use of site-specific meteorological data is the best way to achieve spatial representativeness. AERMET can process a variety of formats and variables for site-specific data. The use of site-specific data for regulatory applications is discussed in detail in section

8.4.4 of Appendix W. Due to the range of data that can be collected onsite and the range of formats of data input to AERMET, the user should consult Appendix W, the AERMET User's Guide (U.S. EPA, 2022b), and Meteorological Monitoring Guidance for Regulatory Modeling Applications (U.S. EPA, 2000). Also, when processing site-specific data for an urban application, Section 3.3 of the AERMOD Implementation Guide offers recommendations for data processing. In summary, the guide recommends that site-specific turbulence measurements should not be used when applying AERMOD's urban option in order to avoid double counting the effects of enhanced turbulence due to the urban heat island.

3.2.3. Upper air data

AERMET requires full upper air soundings to calculate the convective mixing height. For AERMOD applications in the U.S., the early morning sounding, usually the 1200 UTC (Universal Time Coordinate) sounding, is typically used for this purpose. Upper air soundings can be obtained from the Radiosonde Data of North America CD for the period 1946-1997. Upper air soundings for 1994 through the present are also available for free download from the Radiosonde Database Access website. Users should choose all levels or mandatory and significant pressure levels[58] when selecting upper air data. Selecting mandatory levels only would not be adequate for input into AERMET as the use of just mandatory levels would not provide an adequate characterization of the potential temperature profile.

3.2.3. Prognostic data

In specific situations where it is infeasible or cost prohibitive to collect adequately representative site-specific data or there is not a representative NWS or comparable meteorological station available, it may be appropriate to use prognostic meteorological data, if deemed adequately representative. However, if prognostic data are not representative of the transport and dispersion conditions in the area of concern, the collection of site-specific data is necessary (section 8.4.5.1 of Appendix W). To facilitate the use of prognostic meteorological data, EPA has developed a processor, Mesoscale Model Interface Program, MMIF (Environ, 2015), to process MM5 (Mesoscale Model 5) or WRF (Weather Research Forecast) model data for input to various models including AERMOD. MMIF can process data for input to AERMET or AERMOD for a single grid cell or multiple grid cells. For regulatory applications, MMIF should be run to create inputs for AERMET input as described in section 8.4.5.1.b of Appendix W and MMIF guidance (U.S. EPA, 2018b). Specific guidance on running MMIF for AERMOD applications can be found in U.S. EPA, 2018b.

4. Running AERMOD and implications for design value calculations

Recent enhancements to AERMOD include options to aid in the calculation of design values for comparison with the $PM_{2.5}$ NAAQS and to aid in determining whether emissions from the project source caused or contributed to any modeled violations. These enhancements include:

[58] By international convention, mandatory levels are in millibars: 1,000, 850, 700, 500, 400, 300, 200, 150, 100, 50, 30, 20, 10, 7 5, 3, 2, and 1. Significant levels may vary depending on the meteorological conditions at the upper-air station.

- The MAXDCONT option, which shows the impact of each user-specified source group to the high ranked values for a specified target source group paired in time and space. The user can specify a range of ranks to analyze or specify an upper bound rank, *i.e.*, 8th highest, corresponding to the 98th percentile for the 24-hour $PM_{2.5}$ NAAQS, and a lower threshold concentration value, such as the NAAQS for the target source group. The model will process each rank within the range specified, but will stop after the first rank (in descending order of concentration) that is below the threshold value if specified by the user. A warning message will be generated if the threshold is not reached within the range of ranks analyzed (based on the range of ranks specified on the RECTABLE keyword). This option may be needed to aid in determining which sources should be considered for controls.

For more details about the enhancements, see the AERMOD User's Guide (U.S. EPA, 2022a).

Ideally, all explicitly modeled sources, receptors, and background should be modeled in one AERMOD run for all modeled years. In this case, one of the above output options can be used in AERMOD to calculate design values for comparison to the NAAQS and determine the area's attainment status and/or inform attainment/nonattainment boundaries. The use of these options in AERMOD allows AERMOD to internally calculate concentration metrics that can be used to calculate design values and, therefore, lessen the need for large output files, *i.e.*, hourly POSTFILES.

However, there may be situations where a single AERMOD run with all explicitly modeled sources is not possible. These situations often arise due to runtime or storage space considerations during the AERMOD modeling. Sometimes separate AERMOD runs are done for each facility or group of facilities, or by year, or the receptor network is divided into separate sub-networks. In some types of these situations, the MAXDCONT output option may not be an option for design value calculations, especially if all sources are not included in a single run. If the user wishes to utilize one of the three output options, then care should be taken in developing the model inputs to ensure accurate design value calculations.

Situations that would effectively preclude the use of the MAXDCONT option to calculate meaningful AERMOD design value calculations include the following examples:

- Separate AERMOD runs for each source or groups of sources.
    - SIP modeling includes 10 facilities for 5 years of NWS data and each facility is modeled for 5 years in a separate AERMOD run, resulting in ten separate AERMOD runs.
- Separate AERMOD runs for each source and each modeled year.
    - 10 facilities are modeled for 5 years of NWS data. Each facility is modeled separately for each year, resulting in fifty individual AERMOD runs.

In the two situations listed above, the MAXDCONT option would not be useful as the different AERMOD runs do not include a total concentration with impacts from all facilities. In these situations, the use of 24-hour POSTFILES, which can be quite large, and external post-processing would be needed to calculate design values.

Situations in which the MAXDCONT options may be used but may necessitate some external post-processing afterwards to calculate a design value include:

- The receptor network is divided into sections and an AERMOD run, with all sources and years, is made for each sub-network.
    - A receptor network of 1,000 receptors is divided into four 250 receptor sub-networks. 10 facilities are modeled with 5 years of NWS data in one AERMOD run for each receptor network, resulting in four AERMOD runs. After the AERMOD runs are complete, the MAXDCONT results for each network can be re-combined into the larger network.
- All sources and receptors are modeled in an AERMOD run for each year.
- Ten facilities are modeled with 5 years of NWS data. All facilities are modeled with all receptors for each year individually, resulting in five AERMOD runs. MAXDCONT output can be used and post-processed to generate the necessary design value concentrations. The receptor network is divided and each year is modeled separately for each sub-network with all sources.
- Ten facilities are modeled with 5 years of NWS data for 1,000 receptors. The receptor network is divided into four 250 receptor networks. For each sub-network, all ten facilities are modeled for each year separately, resulting in twenty AERMOD runs. MAXDCONT output can be used and post-processed to generate the necessary design value concentrations.

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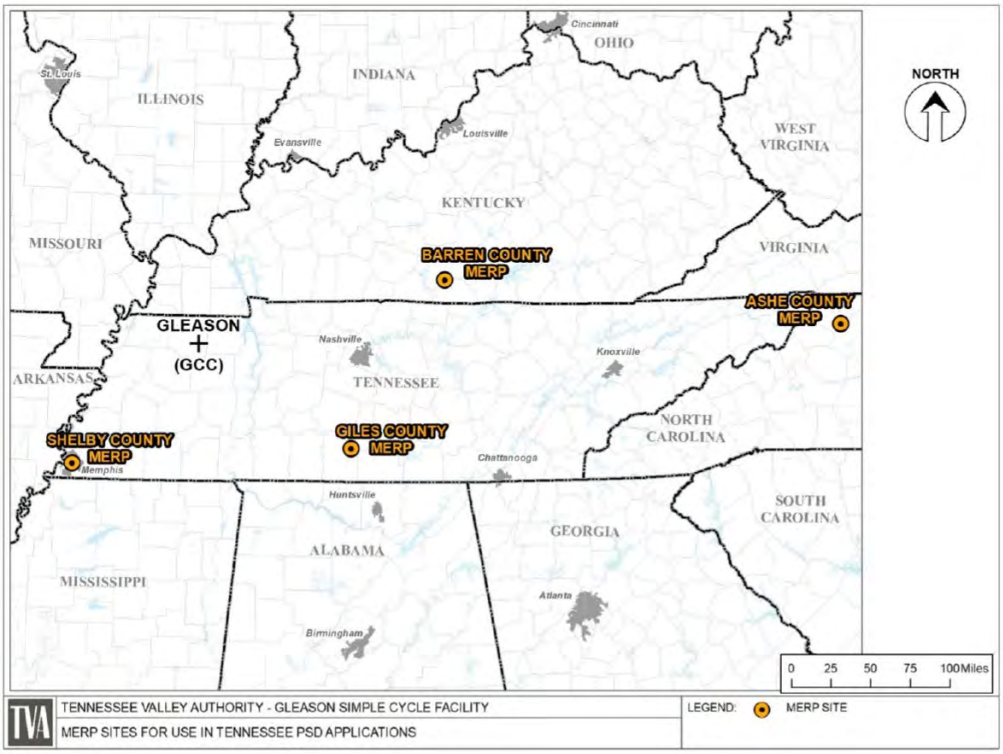
Appendix C: Example of a Tier 1 Demonstration of the Potential for O_3 and Secondary $PM_{2.5}$ Formation

In 2018, a permit applicant, the Tennessee Valley Authority (TVA) Gleason Combustion Turbine Plant (GCC), worked closely with the Tennessee Department of Environment and Conservation (TDEC) and EPA Region 4 to develop a compliance demonstration for a major facility modification, including the use of a Tier 1 assessment of O_3 and secondary $PM_{2.5}$ impacts. This Tier 1 assessment was based on the application of Modeled Emission Rates for Precursors (MERPs) and related modeling guidance released by the EPA. In April 2018, the TDEC published state modeling guidance that can be used by PSD applicants in Tennessee that largely restated the technical aspects of the guidance presented in the EPA's 2016 Draft MERPs Guidance.[59] In support of the 2016 Draft MERPs Guidance and subsequently the 2019 MERPs Guidance, the EPA performed photochemical modeling for four hypothetical sources from within Tennessee or in close proximity to Tennessee (Shelby County, TN, Giles County, TN, Barren County, KY and Ashe County, NC), that can be used to represent the O_3 and secondary $PM_{2.5}$ pollutant formation from other large sources in Tennessee (Figure 1).

FIGURE 1



[59] The EPA released a draft version of the "Guidance on the Development of Modeled Emission Rates for Precursors (MERPs) as a Tier 1 Demonstration Tool for Ozone and $PM_{2.5}$ under the PSD Permitting Program" on December 2, 2016, for public review and comment. Based on the feedback gained from this draft, the EPA released a non-draft or final version of the "MERPs Guidance" on April 30, 2019. The information in the 2016 draft MERPs Guidance from which the TDEC based their April 2018 modeling guidance did not substantively change and is representative of information contained in the current 2019 final version of the MERPs Guidance. The 2019 final MERPs Guidance is available at: https://www.epa.gov/sites/production/files/2020-09/documents/epa-454_r-19-003.pdf.

Assessment of $PM_{2.5}$

Based on information in the EPA's MERPs Guidance, the lowest, most conservative MERPs from these four hypothetical source locations were established in the TDEC state modeling guidance as the default MERPs that can be used throughout Tennessee without the need for further justification (Table 1). The TVA used these default MERPs to assess secondary $PM_{2.5}$ impacts for the proposed modification at the GCC facility.

TABLE 1
Default MERPs for Use in TN PSD Applications

Precursor	MERPs for 8-hr O_3 (tons/yr)	MERPs for Daily $PM_{2.5}$ (tons/year)	MERPs for Annual $PM_{2.5}$ (tons/year)
NO_X	156	4,000	7,407
SO_2	-	667	6,061
VOC	1,339	-	-

The combined primary and secondary impacts of $PM_{2.5}$ for the source impact analysis were assessed using the highest (AERMOD) modeled primary $PM_{2.5}$ concentration (HMC), the Class II SIL, precursor emissions, and the default MERPs. If the sum of the ratios in Equation 1 below is less than 1, then the combined $PM_{2.5}$ impacts are below the $PM_{2.5}$ SIL, an adequate compliance demonstration has been performed, and no additional analyses are necessary.

The following equation was used for this assessment:

EQUATION 1

$$\left(\frac{HMC}{SIL}\right) + \left(\frac{NO_X\_Em}{NO_X\_MERP}\right) + \left(\frac{SO_2\_Em}{SO_2\_MERP}\right) < 1$$

Where:

HMC = Highest modeled primary $PM_{2.5}$ impact using AERMOD and project related $PM_{2.5}$ emissions ($\mu g/m^3$)
SIL = Significant Impact Level ($\mu g/m^3$)
NO_X _Em = Project related NOx Emissions (tons per year – tpy)
NO_X _MERP = NO_X Emissions from Table 1 (tpy)
SO_2_Em = Project related SO_2 Emissions (tpy)
SO_2_MERP = SO_2 Emissions from Table 1 (tpy)

The TVA's 24-hour and annual $PM_{2.5}$ inputs to Equation 1 are provided in Table 2 below, and the resulting combined $PM_{2.5}$ impacts are calculated in Equation 2 and Equation 3 below, respectively.

TABLE 2
Primary and Secondary $PM_{2.5}$ Inputs for the SILs in Class II Areas

Secondary $PM_{2.5}$ Impacts	24-hr Average	Annual Average
Highest Modeled Primary $PM_{2.5}$ Concentration ($\mu g/m^3$) [1]	0.49	0.053
SILs for the NAAQS and PSD Increments in Class II areas ($\mu g/m^3$) [2]	1.2	0.2
GCC NO_x Emissions (tons/yr) [3]	2,270	2,270
Default NO_x MERPs [4]	4,000	7,407
GCC SO_2 Emissions (tons/yr) [3]	14.2	14.2
Default SO_2 MERPs [4]	667	6,061

Notes:

1. TVA GCC facility project primary $PM_{2.5}$ modeling results.
2. SILs for the NAAQS in Class I and Class II areas and for PSD increments in Class II areas. Based on the April 17, 2018 EPA memo, *Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program*.
3. TVA GCC facility project emissions.
4. Default MERPs information from Table 1

Combined Impacts for 24-hour $PM_{2.5}$ for the SIL in Class II Areas:

EQUATION 2

$$\left(\frac{0.49}{1.2}\right) + \left(\frac{2{,}270}{4{,}000}\right) + \left(\frac{14.2}{667}\right) = 0.997$$

Combined Impacts for Annual $PM_{2.5}$ for the SIL in Class II Areas:

EQUATION 3

$$\left(\frac{0.053}{0.2}\right) + \left(\frac{2{,}270}{7{,}407}\right) + \left(\frac{14.2}{6061}\right) = 0.573$$

Both the 24-hour and annual $PM_{2.5}$ combined impacts as presented in Equation 2 and Equation 3 were less than 1, which indicated that 24-hour and annual $PM_{2.5}$ impacts were expected to be below the Class II SILs for the NAAQS and PSD increments. From this source impact $PM_{2.5}$ assessment, it was determined that emissions from TVA GCC facility would not cause or contribute to a violation of the $PM_{2.5}$ NAAQS in Class II areas.

Assessment of O_3

A somewhat more refined analysis was performed to assess the impacts of the proposed project on O_3 concentrations in the area around the TVA GCC facility. Application of the TDEC default NO_X and VOC MERPs for O_3 shown in Table 1 above indicated that O_3 impacts would be greater than the 8-hour O_3 SIL of 1 ppb and that a cumulative O_3 assessment would be necessary to demonstrate whether the facility modification would cause or contribute to a violation of a the O_3 NAAQS.

The O_3 assessment first examined ambient O_3 concentrations in the region surrounding the TVA GCC facility. There are no ambient O_3 monitors in the immediate vicinity of GCC, but there are six monitors within 150 km of the facility (Figure 2 and Tables 3 and 4). The Cadiz, KY, monitor was selected as the most representative background site due to its proximity to GCC, its comparable levels of precursor emissions in the county, and it has the largest measurement scale indicating it is representative of regional air quality. The three-year average (2015- 2017) of the fourth-highest 8-hour O_3 concentration was 61 ppb, well below the 70 ppb NAAQS.

FIGURE 2

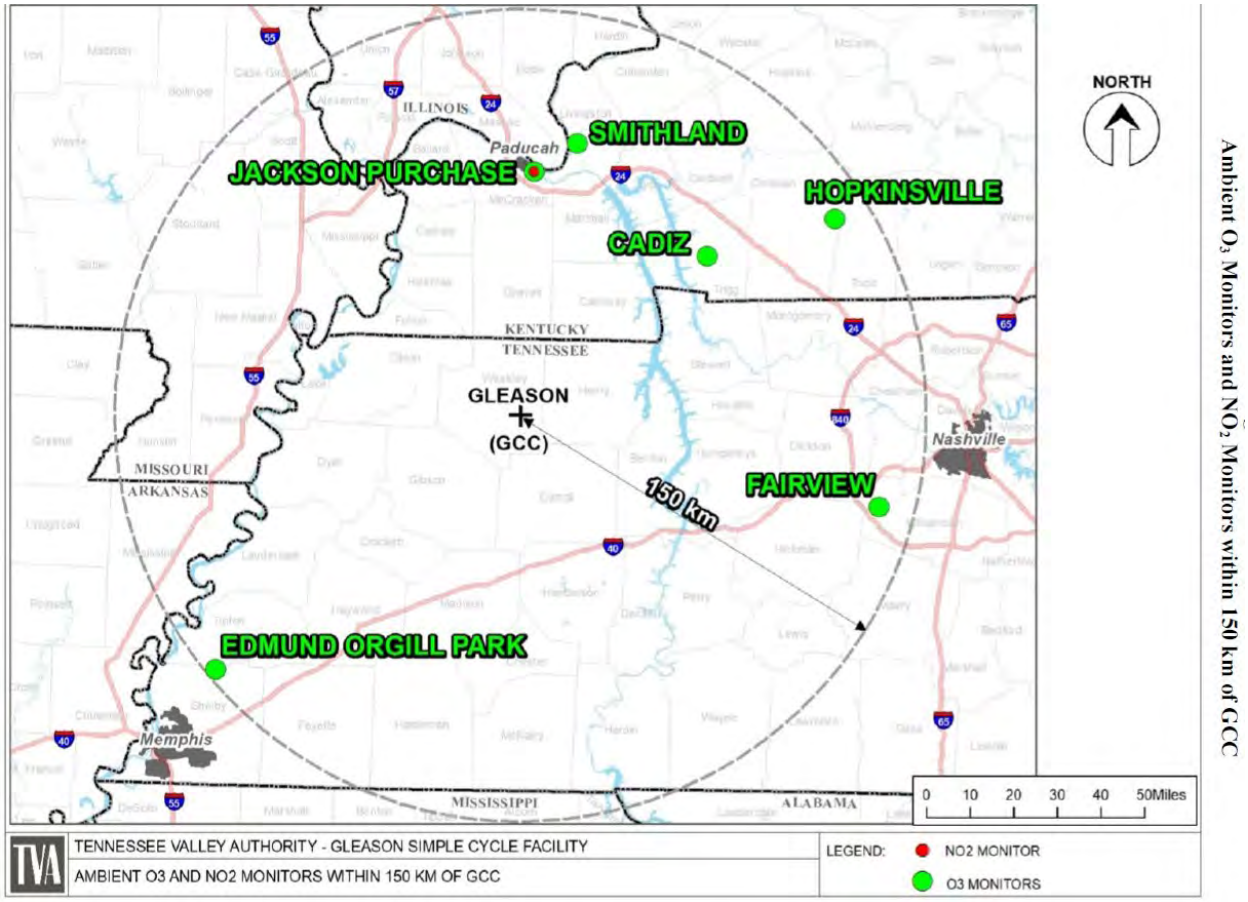


TABLE 3
Ambient O_3 Monitors within 150 km of GCC

Site Name	Site ID	Distance to GCC (km)	Measurement Scale (km)	County NO_X Emissions (tons/year) [1]	County VOC Emissions (tons/year) [1]
Weakley County	NA	0	NA	1,216	9,061
Jackson Purchase	21-145-1024	90	0.5 to 4	15,395	6,542
Cadiz	21-221-9991	91	50 to 100	1,424	14,173
Smithland	21-139-0003	103	4 to 50	1,441	5,933
Fairview	47-187-0106	137	4 to50	5,721	13,557
Hopkinsville	21-047-0006	138	50 to 100	3,589	11,806
Edmund Orgill Park	47-157-1004	147	4 to 50	32,260	38,104

Notes:

1. EPA's National Emissions Inventory, 2014 v.2.

TABLE 4
2015-2017 Ambient O_3 Monitoring Data

Site Name	Site ID	3 Year Avg. 4th High 8-Hr Ozone Conc. (ppb) [1]
Jackson Purchase	21-145-1024	62
Cadiz	21-221-9991	61
Smithland	21-139-0003	64
Fairview	47-187-0106	60
Hopkinsville	21-047-0006	61
Edmund Orgill Park	47-157-1004	65

Notes:

1. EPA Air Quality System (AQS) Data Mart: https://www.epa.gov/outdoor-air-quality-data.

As previously discussed, in April 2018, TDEC published modeling guidance on the use of EPA's MERPs in Tennessee that identified four hypothetical sites, located in Shelby County, TN, Giles County, TN, Barren County, KY and Ashe County, NC, to represent Tennessee sources (Figure 1). Precursor emissions in these four counties were compared to Weakley County, where the TVA GCC facility is located. Weakley County precursor emissions are comparable to emissions in the three rural counties (Giles, Barren and Ashe) and are much lower than Shelby County which is urban (Table 5). Ashe County is much further from GCC and is located in mountainous terrain, unlike the relatively flat terrain around GCC. Both Giles County and Barren County have similar terrain features to Weakley County. NO_X MERPs at these two sites are also lower than in Shelby County and Ashe County, which makes the analysis more conservative as ozone impacts from GCC are dominated by NO_X emissions.

TABLE 5
Comparison of Weakley County O_3 MERPs Sites for Use in TN

County	Distance to GCC (km)	Urban/ Rural	Elevation (m)	County NO_X Emissions (tons/year) [1]	County VOC Emissions (tons/year) [1]	NO_X MERP (ton/year) [2]	VOC MERP (ton/year) [2]
Weakly, TN	--	Rural	110	1,216	9,061	NA	NA
Shelby, TN	177	Urban	94	32,260	38,104	714	1,339
Giles, TN	188	Rural	240	1,913	11,298	156	4,000
Barren, KY	257	Rural	256	2,122	7,580	169	3,333
Ashe, NC	650	Rural	926	730	6,507	267	8,333

Notes:

1. EPA's National Emissions Inventory, 2014 v.2.
2. Lowest, most conservative MERP at each site.

For the two most representative hypothetical sources selected, as part of EPA's MERPs Guidance, the EPA performed photochemical modeling for two hypothetical source heights (low and high stack releases) and three hypothetical emission rates (500, 1000, and 3000 tons per year). As can be seen in Table 6 below, predicted O_3 impacts are nonlinear with respect to precursor emissions. At these hypothetical sources, the amount of O_3 formed from 3,000 tons of NO_X is substantially less than six times the amount formed from 500 tons of NO_X on a per ton basis, so using a MERP based on 500 tons of NO_X would significantly over-estimate the O_3 impacts from GCC. Therefore, this analysis used the most conservative MERPs based on emission rates most similar to emissions from GCC (hypothetical source emissions of 3,000 tons per year for NO_X and 500 tons per year for VOCs) at the two most representative sites (Giles County and Barren County) (Table 7).

TABLE 6

Precursor	Pollutant	State	County	FIPS	TPY	Stack Height (m)	Conc. (ppb)	MERP (tons/year)
NO_X	O_3	Kentucky	Barren	21009	500	10	2.908	172
NO_X	O_3	Kentucky	Barren	21009	500	90	2.946	170
NO_X	O_3	Kentucky	Barren	21009	1000	90	5.026	199
NO_X	O_3	Kentucky	Barren	21009	3000	90	10.687	281
NO_X	O_3	Tennessee	Giles	47055	500	10	2.616	191
NO_X	O_3	Tennessee	Giles	47055	500	90	3.208	156
NO_X	O_3	Tennessee	Giles	47055	1000	90	5.387	186
NO_X	O_3	Tennessee	Giles	47055	3000	90	10.356	290

TCA GCC project emissions are 2,270 for NO_X and 158 tpy for VOC.

TABLE 7
O3 MERPs for Various Emissions Rates in Giles County and Barren County

County	Stack	NO_X Emissions (tons/year)	NO_X MERP (ton/year)	VOC Emissions (tons/yr)	VOC MERP (ton/year)
Giles, TN	Low	500	163	500	12,500
Giles, TN	High	500	156	500	NA
Giles, TN	Low	1,000	NA	1,000	11,111
Giles, TN	High	1,000	186	1,000	10,000
Giles, TN	High	3,000	290	3,000	4,000
Barren, KY	Low	500	172	500	8,333
Barren, KY	High	500	169	500	8,333
Barren, KY	High	1,000	199	1,000	7,692
Barren, KY	High	3,000	281	3,000	3,333
Most Conservative for Emissions Similar to GCC [1]			281		8,333

Notes:

1. Hypothetical sources with NO_X emissions of 3,000 tons per year and VOC emissions of 500 tons per year.

The O_3 impacts for the source impact assessment were calculated as the sum of the ratio of precursor emissions to the MERPs. If the sum of the ratios is less than 1, then the O_3 impacts are below the O_3 SIL and no cumulative analysis is necessary.

EQUATION 4

$$\left(\frac{NO_X\_Em}{NO_X\_MERP}\right) + \left(\frac{VOC\_Em}{VOC\_MERP}\right) < 1$$

Where:

NO_X _Em = Project related NOx Emissions (tons per year – tpy)
NO_X _MERP = NO_X Emissions from Table 7 (tpy)
VOC_Em = Project related VOC Emissions (tpy)
VOC_MERP = VOC Emissions from Table 7 (tpy)

The TVA GCC facility's ozone inputs to Equation 4 are provided in Table 8, and the resulting impacts are calculated in Equation 5 below.

TABLE 8
O3 Inputs for the SIL in Class II Areas

O_3 Precursor	GCC Emissions (tons/year) [1]	MERP (tons/year) [1]
NO_X	2,270	281 [2]
VOC	158	8,333 [3]

Notes:

1. TVA GCC facility project emissions.
2. Most conservative MERP for NO_X emissions of 3,000 tons per year at Giles County or Barren County.
3. Most conservative MERP for VOC emissions of 500 tons per year at Giles County or Barren County.

Combined Impacts for O_3 for the SIL in Class II Areas:

EQUATION 5

$$\left(\frac{2{,}270}{281}\right) + \left(\frac{158}{8{,}333}\right) = 8.10$$

According to Equation 5, the sum of the ratios was greater than 1, and the combined O_3 impacts were above the SIL. Therefore, a cumulative O_3 analysis was necessary and performed, which added background O_3 and compared the combined impacts to the NAAQS, as shown in Equation 6.

EQUATION 6

$$Background\ O_3 + \left(\left(\left(\frac{NOx\_Em}{NOx\_MERP}\right) + \left(\frac{VOC\_Em}{VOC\_MERP}\right)\right) \times SIL\right) \leq NAAQS$$

Where:

Background Ozone = 2015-2017 8-hour O_3 design value (ppb) for Cadiz monitor
NO_X _Em = Project related NOx Emissions (tons per year – tpy)
NO_X _MERP = NO_X Emissions from Table 7 (tpy)
VOC_Em = Project related VOC Emissions (tpy)
VOC_MERP = VOC Emissions from Table 7 (tpy)
SIL = 1 ppb O_3
NAAQS = 8-hour O_3 NAAQS (70 ppb)

The cumulative O_3 impacts from the TCA GCC facility are calculated in Equation 7 below.

Cumulative O_3 Impacts:

EQUATION 7

$$61\ ppb\ + \left(\left(\left(\frac{2{,}270}{281} \right) + \left(\frac{158}{8{,}333} \right) \right) \times 1 \right) = 69.1\ ppb$$

Using the 3-year 8-hour O_3 design value of 61 ppb from Cadiz, KY, the ratios defined in Equation 5, and the O_3 SIL of 1 ppb, the cumulative O_3 impacts was calculated to be 69.1 ppb and did not exceed the O_3 NAAQS. From this cumulative O_3 assessment, it was determined that emissions from the TCA GCC facility would not cause or contribute to a violation of the O_3 NAAQS.

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Appendix D: Example of the background monitoring data calculations for a Second Level 24-hour modeling analysis

This appendix provides an illustrative example of the calculations and data sorting recommendations for the background monitoring data to be used in a Second Level 24-hour $PM_{2.5}$ modeling analysis. In this example, it was determined through discussion and coordination with the appropriate permitting authority that the impacts from the project source's direct $PM_{2.5}$ emissions were most prominent during the cool season and were not temporally correlated with background $PM_{2.5}$ levels that were typical highest during the warm season. So, combining the modeled and monitored levels through a First Level 24-hour $PM_{2.5}$ modeling analysis was determined to be potentially overly conservative. Extending the compliance demonstration to a Second Level analysis allows for a more refined and appropriate assessment of the cumulative impacts on the direct $PM_{2.5}$ emissions in this particular situation.

The example provided is from an idealized Federal Reference Method (FRM) $PM_{2.5}$ monitoring site that operates on a daily (1-in-1 day) frequency with 100% data completeness. In this case, the annual 98^{th} percentile concentration is the 8^{th} highest concentration of the year. In most cases, the FRM monitoring site will likely operate on a 1-and-3 day frequency and will also likely have missing data due to monitor maintenance or collected data not meeting all of the quality assurance criteria. Please reference Appendix N to 40 CFR part 50 to determine the appropriate 98^{th} percentile rank of the monitored data based on the monitor sampling frequency and valid number of days sampled during each year.

The appropriate seasonal (or quarterly) background concentrations to be included as inputs to the AERMOD model per a Second Level 24-hour $PM_{2.5}$ modeling analysis are as follows:

- Step 1 – Start with the most recent 3-years of representative background $PM_{2.5}$ ambient monitoring data that are being used to develop the monitored background $PM_{2.5}$ design value. In this example, the 3-years of 2008 to 2010 are being used to determine the monitored design value.

- Step 2 – For each year, determine the appropriate rank for the daily 98^{th} percentile $PM_{2.5}$ concentration. Again, this idealized example is from a 1-in-1 day monitor with 100% data completeness. So, the 8^{th} highest concentration of each year is the 98^{th} percentile $PM_{2.5}$ concentration. The 98^{th} percentile $PM_{2.5}$ concentration for 2008 is highlighted in Table D-1. The full concentration data from 2009 and 2010 are not shown across the steps in this Appendix for simplicity but would be similar to that of 2008.

- Step 3 – Remove from further consideration in this analysis the $PM_{2.5}$ concentrations from each year that are greater than the 98^{th} percentile $PM_{2.5}$ concentration. In the case presented for a 1-in-1 day monitor, the top 7 concentrations are removed. If the monitor were a 1-in-3 day monitor, only the top 2 concentrations would be removed. The resultant dataset after the top 7 concentrations have been removed from further consideration in this analysis for 2008 is presented in Table D-2.

- Step 4 – For each year, divide the resultant annual dataset of the monitored data equal to or less than the 98th percentile $PM_{2.5}$ concentration into each season (or quarter). For 2008, the seasonal subsets are presented in Table D-3.

- Step 5 – Determine the maximum $PM_{2.5}$ concentration from each of the seasonal (or quarterly) subsets created in Step 4 for each year. The maximum $PM_{2.5}$ concentration from each season for 2008 is highlighted in Table D-3.

- Step 6 – Average the seasonal (or quarterly) maximums from Step 5 across the three years of monitoring data to create the four seasonal background PM2.5 concentrations to be included as inputs to the AERMOD model. These averages for the 2008 to 2010 dataset used in this example are presented in Table D-4. As noted above, the full concentration data from 2009 and 2010 are not shown across the steps in this Appendix for simplicity, but the seasonal maximums from 2009 and 2010 presented in Table D-4 were determined by following the previous five steps similar to that of 2008.

Table D-1. 2008 Daily $PM_{2.5}$ Concentrations

Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.
1-Jan	10.4	16-Feb	15.1	2-Apr	10.5	18-May	11.1	3-Jul	17.1	18-Aug	18.7	3-Oct	12.3	18-Nov	4.4
2-Jan	5.4	17-Feb	11.8	3-Apr	8.2	19-May	7.7	4-Jul	19.8	19-Aug	21.5	4-Oct	19.5	19-Nov	8.2
3-Jan	10.0	18-Feb	3.4	4-Apr	9.7	20-May	13.6	5-Jul	14.3	20-Aug	20.1	5-Oct	23.7	20-Nov	11.1
4-Jan	16.4	19-Feb	4.5	5-Apr	6.9	21-May	12.1	6-Jul	11.5	21-Aug	18.4	6-Oct	19.8	21-Nov	5.3
5-Jan	11.2	20-Feb	4.8	6-Apr	6.3	22-May	10.0	7-Jul	14.3	22-Aug	16.7	7-Oct	21.7	22-Nov	8.9
6-Jan	11.1	21-Feb	11.9	7-Apr	7.9	23-May	13.3	8-Jul	12.2	23-Aug	13.8	8-Oct	12.2	23-Nov	14.0
7-Jan	10.2	22-Feb	20.1	8-Apr	9.8	24-May	11.2	9-Jul	11.1	24-Aug	19.0	9-Oct	5.1	24-Nov	12.7
8-Jan	11.4	23-Feb	11.4	9-Apr	16.5	25-May	17.7	10-Jul	9.7	25-Aug	17.6	10-Oct	10.2	25-Nov	9.7
9-Jan	8.1	24-Feb	19.3	10-Apr	13.3	26-May	14.2	11-Jul	16.4	26-Aug	15.4	11-Oct	10.7	26-Nov	12.8
10-Jan	9.4	25-Feb	18.2	11-Apr	11.0	27-May	15.4	12-Jul	21.5	27-Aug	12.6	12-Oct	5.6	27-Nov	16.6
11-Jan	5.7	26-Feb	12.8	12-Apr	8.8	28-May	13.9	13-Jul	25.1	28-Aug	12.1	13-Oct	5.9	28-Nov	17.2
12-Jan	8.9	27-Feb	5.5	13-Apr	6.3	29-May	9.3	14-Jul	11.7	29-Aug	10.1	14-Oct	9.7	29-Nov	16.6
13-Jan	18.1	28-Feb	9.7	14-Apr	5.1	30-May	14.5	15-Jul	18.9	30-Aug	17.2	15-Oct	12.8	30-Nov	4.5
14-Jan	11.0	29-Feb	12.1	15-Apr	7.9	31-May	20.5	16-Jul	28.9	31-Aug	19.9	16-Oct	16.4	1-Dec	7.5
15-Jan	11.8	1-Mar	9.6	16-Apr	8.2	1-Jun	15.3	17-Jul	27.6	1-Sep	19.4	17-Oct	12.0	2-Dec	10.6
16-Jan	10.7	2-Mar	5.6	17-Apr	14.7	2-Jun	11.5	18-Jul	12.8	2-Sep	18.2	18-Oct	7.9	3-Dec	16.7
17-Jan	10.0	3-Mar	12.5	18-Apr	22.5	3-Jun	17.9	19-Jul	6.2	3-Sep	24.0	19-Oct	6.6	4-Dec	12.5
18-Jan	15.6	4-Mar	7.1	19-Apr	12.8	4-Jun	21.1	20-Jul	20.1	4-Sep	15.4	20-Oct	8.1	5-Dec	7.3
19-Jan	18.0	5-Mar	4.9	20-Apr	6.9	5-Jun	17.9	21-Jul	26.5	5-Sep	12.4	21-Oct	12.2	6-Dec	10.4
20-Jan	6.6	6-Mar	9.9	21-Apr	7.5	6-Jun	17.6	22-Jul	16.9	6-Sep	12.5	22-Oct	4.6	7-Dec	13.4
21-Jan	7.4	7-Mar	11.2	22-Apr	6.0	7-Jun	15.0	23-Jul	12.8	7-Sep	15.8	23-Oct	6.1	8-Dec	10.5
22-Jan	13.5	8-Mar	5.5	23-Apr	9.1	8-Jun	22.3	24-Jul	7.9	8-Sep	23.4	24-Oct	4.6	9-Dec	9.3
23-Jan	16.0	9-Mar	8.8	24-Apr	10.3	9-Jun	27.9	25-Jul	15.7	9-Sep	11.5	25-Oct	4.5	10-Dec	6.5
24-Jan	9.4	10-Mar	11.0	25-Apr	12.0	10-Jun	21.6	26-Jul	24.9	10-Sep	6.0	26-Oct	10.5	11-Dec	3.0
25-Jan	12.6	11-Mar	12.1	26-Apr	12.5	11-Jun	19.4	27-Jul	22.2	11-Sep	11.8	27-Oct	6.4	12-Dec	3.5
26-Jan	13.6	12-Mar	9.7	27-Apr	11.3	12-Jun	21.2	28-Jul	17.5	12-Sep	10.7	28-Oct	4.6	13-Dec	10.2
27-Jan	16.1	13-Mar	15.1	28-Apr	7.6	13-Jun	29.1	29-Jul	19.1	13-Sep	7.6	29-Oct	5.6	14-Dec	17.6
28-Jan	10.0	14-Mar	21.6	29-Apr	7.4	14-Jun	15.6	30-Jul	21.1	14-Sep	7.5	30-Oct	7.6	15-Dec	12.4
29-Jan	10.4	15-Mar	16.6	30-Apr	11.4	15-Jun	14.8	31-Jul	18.0	15-Sep	7.1	31-Oct	11.2	16-Dec	9.7
30-Jan	6.9	16-Mar	7.9	1-May	12.6	16-Jun	17.8	1-Aug	16.3	16-Sep	7.7	1-Nov	16.2	17-Dec	7.0
31-Jan	4.9	17-Mar	9.6	2-May	10.0	17-Jun	12.6	2-Aug	19.3	17-Sep	11.3	2-Nov	17.3	18-Dec	7.9
1-Feb	5.4	18-Mar	10.3	3-May	11.2	18-Jun	10.5	3-Aug	17.9	18-Sep	16.8	3-Nov	18.3	19-Dec	6.9
2-Feb	7.1	19-Mar	8.4	4-May	10.4	19-Jun	15.0	4-Aug	25.1	19-Sep	14.8	4-Nov	8.9	20-Dec	8.1
3-Feb	10.9	20-Mar	4.9	5-May	15.7	20-Jun	22.7	5-Aug	29.3	20-Sep	8.0	5-Nov	5.8	21-Dec	4.9
4-Feb	12.1	21-Mar	8.7	6-May	16.1	21-Jun	18.7	6-Aug	19.1	21-Sep	10.8	6-Nov	8.6	22-Dec	7.7
5-Feb	17.1	22-Mar	13.3	7-May	16.8	22-Jun	15.2	7-Aug	14.0	22-Sep	14.5	7-Nov	15.0	23-Dec	7.7
6-Feb	10.3	23-Mar	12.2	8-May	14.5	23-Jun	16.8	8-Aug	10.8	23-Sep	21.2	8-Nov	8.3	24-Dec	10.5
7-Feb	4.0	24-Mar	10.3	9-May	11.7	24-Jun	15.1	9-Aug	15.0	24-Sep	8.6	9-Nov	10.0	25-Dec	6.5
8-Feb	9.7	25-Mar	11.9	10-May	9.0	25-Jun	20.7	10-Aug	21.7	25-Sep	1.2	10-Nov	12.8	26-Dec	7.6
9-Feb	11.5	26-Mar	20.1	11-May	6.7	26-Jun	23.0	11-Aug	14.3	26-Sep	16.0	11-Nov	11.8	27-Dec	13.3
10-Feb	3.0	27-Mar	22.5	12-May	7.9	27-Jun	17.8	12-Aug	14.7	27-Sep	12.1	12-Nov	14.8	28-Dec	6.4
11-Feb	5.5	28-Mar	18.2	13-May	8.3	28-Jun	12.4	13-Aug	13.0	28-Sep	18.0	13-Nov	14.5	29-Dec	3.7
12-Feb	18.9	29-Mar	10.8	14-May	12.2	29-Jun	12.7	14-Aug	13.5	29-Sep	17.8	14-Nov	7.7	30-Dec	4.7
13-Feb	17.6	30-Mar	6.4	15-May	13.1	30-Jun	8.9	15-Aug	17.5	30-Sep	16.4	15-Nov	3.6	31-Dec	4.4
14-Feb	11.2	31-Mar	3.3	16-May	8.8	1-Jul	7.1	16-Aug	23.9	1-Oct	12.3	16-Nov	4.6		
15-Feb	14.4	1-Apr	7.8	17-May	8.2	2-Jul	13.8	17-Aug	18.4	2-Oct	8.2	17-Nov	7.8		

Annual 98th Percentile Concentration = 25.1 µg/m^3

Table D-2. 2008 Daily $PM_{2.5}$ Concentrations Less Than or Equal to the 98th Percentile

Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.	Date	Conc.
1-Jan	10.4	16-Feb	15.1	2-Apr	10.5	18-May	11.1	3-Jul	17.1	18-Aug	18.7	3-Oct	12.3	18-Nov	4.4
2-Jan	5.4	17-Feb	11.8	3-Apr	8.2	19-May	7.7	4-Jul	19.8	19-Aug	21.5	4-Oct	19.5	19-Nov	8.2
3-Jan	10.0	18-Feb	3.4	4-Apr	9.7	20-May	13.6	5-Jul	14.3	20-Aug	20.1	5-Oct	23.7	20-Nov	11.1
4-Jan	16.4	19-Feb	4.5	5-Apr	6.9	21-May	12.1	6-Jul	11.5	21-Aug	18.4	6-Oct	19.8	21-Nov	5.3
5-Jan	11.2	20-Feb	4.8	6-Apr	6.3	22-May	10.0	7-Jul	14.3	22-Aug	16.7	7-Oct	21.7	22-Nov	8.9
6-Jan	11.1	21-Feb	11.9	7-Apr	7.9	23-May	13.3	8-Jul	12.2	23-Aug	13.8	8-Oct	12.2	23-Nov	14.0
7-Jan	10.2	22-Feb	20.1	8-Apr	9.8	24-May	11.2	9-Jul	11.1	24-Aug	19.0	9-Oct	5.1	24-Nov	12.7
8-Jan	11.4	23-Feb	11.4	9-Apr	16.5	25-May	17.7	10-Jul	9.7	25-Aug	17.6	10-Oct	10.2	25-Nov	9.7
9-Jan	8.1	24-Feb	19.3	10-Apr	13.3	26-May	14.2	11-Jul	16.4	26-Aug	15.4	11-Oct	10.7	26-Nov	12.8
10-Jan	9.4	25-Feb	18.2	11-Apr	11.0	27-May	15.4	12-Jul	21.5	27-Aug	12.6	12-Oct	5.6	27-Nov	16.6
11-Jan	5.7	26-Feb	12.8	12-Apr	8.8	28-May	13.9	13-Jul	RC	28-Aug	12.1	13-Oct	5.9	28-Nov	17.2
12-Jan	8.9	27-Feb	5.5	13-Apr	6.3	29-May	9.3	14-Jul	11.7	29-Aug	10.1	14-Oct	9.7	29-Nov	16.6
13-Jan	18.1	28-Feb	9.7	14-Apr	5.1	30-May	14.5	15-Jul	18.9	30-Aug	17.2	15-Oct	12.8	30-Nov	4.5
14-Jan	11.0	29-Feb	12.1	15-Apr	7.9	31-May	20.5	16-Jul	RC	31-Aug	19.9	16-Oct	16.4	1-Dec	7.5
15-Jan	11.8	1-Mar	9.6	16-Apr	8.2	1-Jun	15.3	17-Jul	RC	1-Sep	19.4	17-Oct	12.0	2-Dec	10.6
16-Jan	10.7	2-Mar	5.6	17-Apr	14.7	2-Jun	11.5	18-Jul	12.8	2-Sep	18.2	18-Oct	7.9	3-Dec	16.7
17-Jan	10.0	3-Mar	12.5	18-Apr	22.5	3-Jun	17.9	19-Jul	6.2	3-Sep	24.0	19-Oct	6.6	4-Dec	12.5
18-Jan	15.6	4-Mar	7.1	19-Apr	12.8	4-Jun	21.1	20-Jul	20.1	4-Sep	15.4	20-Oct	8.1	5-Dec	7.3
19-Jan	18.0	5-Mar	4.9	20-Apr	6.9	5-Jun	17.9	21-Jul	RC	5-Sep	12.4	21-Oct	12.2	6-Dec	10.4
20-Jan	6.6	6-Mar	9.9	21-Apr	7.5	6-Jun	17.6	22-Jul	16.9	6-Sep	12.5	22-Oct	4.6	7-Dec	13.4
21-Jan	7.4	7-Mar	11.2	22-Apr	6.0	7-Jun	15.0	23-Jul	12.8	7-Sep	15.8	23-Oct	6.1	8-Dec	10.5
22-Jan	13.5	8-Mar	5.5	23-Apr	9.1	8-Jun	22.3	24-Jul	7.9	8-Sep	23.4	24-Oct	4.6	9-Dec	9.3
23-Jan	16.0	9-Mar	8.8	24-Apr	10.3	9-Jun	RC	25-Jul	15.7	9-Sep	11.5	25-Oct	4.5	10-Dec	6.5
24-Jan	9.4	10-Mar	11.0	25-Apr	12.0	10-Jun	21.6	26-Jul	24.9	10-Sep	6.0	26-Oct	10.5	11-Dec	3.0
25-Jan	12.6	11-Mar	12.1	26-Apr	12.5	11-Jun	19.4	27-Jul	22.2	11-Sep	11.8	27-Oct	6.4	12-Dec	3.5
26-Jan	13.6	12-Mar	9.7	27-Apr	11.3	12-Jun	21.2	28-Jul	17.5	12-Sep	10.7	28-Oct	4.6	13-Dec	10.2
27-Jan	16.1	13-Mar	15.1	28-Apr	7.6	13-Jun	RC	29-Jul	19.1	13-Sep	7.6	29-Oct	5.6	14-Dec	17.6
28-Jan	10.0	14-Mar	21.6	29-Apr	7.4	14-Jun	15.6	30-Jul	21.1	14-Sep	7.5	30-Oct	7.6	15-Dec	12.4
29-Jan	10.4	15-Mar	16.6	30-Apr	11.4	15-Jun	14.8	31-Jul	18.0	15-Sep	7.1	31-Oct	11.2	16-Dec	9.7
30-Jan	6.9	16-Mar	7.9	1-May	12.6	16-Jun	17.8	1-Aug	16.3	16-Sep	7.7	1-Nov	16.2	17-Dec	7.0
31-Jan	4.9	17-Mar	9.6	2-May	10.0	17-Jun	12.6	2-Aug	19.3	17-Sep	11.3	2-Nov	17.3	18-Dec	7.9
1-Feb	5.4	18-Mar	10.3	3-May	11.2	18-Jun	10.5	3-Aug	17.9	18-Sep	16.8	3-Nov	18.3	19-Dec	6.9
2-Feb	7.1	19-Mar	8.4	4-May	10.4	19-Jun	15.0	4-Aug	25.1	19-Sep	14.8	4-Nov	8.9	20-Dec	8.1
3-Feb	10.9	20-Mar	4.9	5-May	15.7	20-Jun	22.7	5-Aug	RC	20-Sep	8.0	5-Nov	5.8	21-Dec	4.9
4-Feb	12.1	21-Mar	8.7	6-May	16.1	21-Jun	18.7	6-Aug	19.1	21-Sep	10.8	6-Nov	8.6	22-Dec	7.7
5-Feb	17.1	22-Mar	13.3	7-May	16.8	22-Jun	15.2	7-Aug	14.0	22-Sep	14.5	7-Nov	15.0	23-Dec	7.7
6-Feb	10.3	23-Mar	12.2	8-May	14.5	23-Jun	16.8	8-Aug	10.8	23-Sep	21.2	8-Nov	8.3	24-Dec	10.5
7-Feb	4.0	24-Mar	10.3	9-May	11.7	24-Jun	15.1	9-Aug	15.0	24-Sep	8.6	9-Nov	10.0	25-Dec	6.5
8-Feb	9.7	25-Mar	11.9	10-May	9.0	25-Jun	20.7	10-Aug	21.7	25-Sep	1.2	10-Nov	12.8	26-Dec	7.6
9-Feb	11.5	26-Mar	20.1	11-May	6.7	26-Jun	23.0	11-Aug	14.3	26-Sep	16.0	11-Nov	11.8	27-Dec	13.3
10-Feb	3.0	27-Mar	22.5	12-May	7.9	27-Jun	17.8	12-Aug	14.7	27-Sep	12.1	12-Nov	14.8	28-Dec	6.4
11-Feb	5.5	28-Mar	18.2	13-May	8.3	28-Jun	12.4	13-Aug	13.0	28-Sep	18.0	13-Nov	14.5	29-Dec	3.7
12-Feb	18.9	29-Mar	10.8	14-May	12.2	29-Jun	12.7	14-Aug	13.5	29-Sep	17.8	14-Nov	7.7	30-Dec	4.7
13-Feb	17.6	30-Mar	6.4	15-May	13.1	30-Jun	8.9	15-Aug	17.5	30-Sep	16.4	15-Nov	3.6	31-Dec	4.4
14-Feb	11.2	31-Mar	3.3	16-May	8.8	1-Jul	7.1	16-Aug	23.9	1-Oct	12.3	16-Nov	4.6		
15-Feb	14.4	1-Apr	7.8	17-May	8.2	2-Jul	13.8	17-Aug	18.4	2-Oct	8.2	17-Nov	7.8		

Annual 98th Percentile Concentration = 25.1 µg/m^3
RC = Above 98th Percentile and Removed from Consideration

Table D-3. 2008 Daily $PM_{2.5}$ Concentrations Less Than or Equal to the 98th Percentile by Quarter

Season / Quarter 1			
Date	Conc.	Date	Conc.
1-Jan	10.4	16-Feb	15.1
2-Jan	5.4	17-Feb	11.8
3-Jan	10.0	18-Feb	3.4
4-Jan	16.4	19-Feb	4.5
5-Jan	11.2	20-Feb	4.8
6-Jan	11.1	21-Feb	11.9
7-Jan	10.2	22-Feb	20.1
8-Jan	11.4	23-Feb	11.4
9-Jan	8.1	24-Feb	19.3
10-Jan	9.4	25-Feb	18.2
11-Jan	5.7	26-Feb	12.8
12-Jan	8.9	27-Feb	5.5
13-Jan	18.1	28-Feb	9.7
14-Jan	11.0	29-Feb	12.1
15-Jan	11.8	1-Mar	9.6
16-Jan	10.7	2-Mar	5.6
17-Jan	10.0	3-Mar	12.5
18-Jan	15.6	4-Mar	7.1
19-Jan	18.0	5-Mar	4.9
20-Jan	6.6	6-Mar	9.9
21-Jan	7.4	7-Mar	11.2
22-Jan	13.5	8-Mar	5.5
23-Jan	16.0	9-Mar	8.8
24-Jan	9.4	10-Mar	11.0
25-Jan	12.6	11-Mar	12.1
26-Jan	13.6	12-Mar	9.7
27-Jan	16.1	13-Mar	15.1
28-Jan	10.0	14-Mar	21.6
29-Jan	10.4	15-Mar	16.6
30-Jan	6.9	16-Mar	7.9
31-Jan	4.9	17-Mar	9.6
1-Feb	5.4	18-Mar	10.3
2-Feb	7.1	19-Mar	8.4
3-Feb	10.9	20-Mar	4.9
4-Feb	12.1	21-Mar	8.7
5-Feb	17.1	22-Mar	13.3
6-Feb	10.3	23-Mar	12.2
7-Feb	4.0	24-Mar	10.3
8-Feb	9.7	25-Mar	11.9
9-Feb	11.5	26-Mar	20.1
10-Feb	3.0	27-Mar	22.5
11-Feb	5.5	28-Mar	18.2
12-Feb	18.9	29-Mar	10.8
13-Feb	17.6	30-Mar	6.4
14-Feb	11.2	31-Mar	3.3
15-Feb	14.4		
Seasonal / Quarterly Maximum			22.5

Season / Quarter 2			
Date	Conc.	Date	Conc.
1-Apr	7.8	17-May	8.2
2-Apr	10.5	18-May	11.1
3-Apr	8.2	19-May	7.7
4-Apr	9.7	20-May	13.6
5-Apr	6.9	21-May	12.1
6-Apr	6.3	22-May	10.0
7-Apr	7.9	23-May	13.3
8-Apr	9.8	24-May	11.2
9-Apr	16.5	25-May	17.7
10-Apr	13.3	26-May	14.2
11-Apr	11.0	27-May	15.4
12-Apr	8.8	28-May	13.9
13-Apr	6.3	29-May	9.3
14-Apr	5.1	30-May	14.5
15-Apr	7.9	31-May	20.5
16-Apr	8.2	1-Jun	15.3
17-Apr	14.7	2-Jun	11.5
18-Apr	22.5	3-Jun	17.9
19-Apr	12.8	4-Jun	21.1
20-Apr	6.9	5-Jun	17.9
21-Apr	7.5	6-Jun	17.6
22-Apr	6.0	7-Jun	15.0
23-Apr	9.1	8-Jun	22.3
24-Apr	10.3	9-Jun	RC
25-Apr	12.0	10-Jun	21.6
26-Apr	12.5	11-Jun	19.4
27-Apr	11.3	12-Jun	21.2
28-Apr	7.6	13-Jun	RC
29-Apr	7.4	14-Jun	15.6
30-Apr	11.4	15-Jun	14.8
1-May	12.6	16-Jun	17.8
2-May	10.0	17-Jun	12.6
3-May	11.2	18-Jun	10.5
4-May	10.4	19-Jun	15.0
5-May	15.7	20-Jun	22.7
6-May	16.1	21-Jun	18.7
7-May	16.8	22-Jun	15.2
8-May	14.5	23-Jun	16.8
9-May	11.7	24-Jun	15.1
10-May	9.0	25-Jun	20.7
11-May	6.7	26-Jun	23.0
12-May	7.9	27-Jun	17.8
13-May	8.3	28-Jun	12.4
14-May	12.2	29-Jun	12.7
15-May	13.1	30-Jun	8.9
16-May	8.8		
Seasonal / Quarterly Maximum			23.0

Season / Quarter 3			
Date	Conc.	Date	Conc.
1-Jul	7.1	16-Aug	23.9
2-Jul	13.8	17-Aug	18.4
3-Jul	17.1	18-Aug	18.7
4-Jul	19.8	19-Aug	21.5
5-Jul	14.3	20-Aug	20.1
6-Jul	11.5	21-Aug	18.4
7-Jul	14.3	22-Aug	16.7
8-Jul	12.2	23-Aug	13.8
9-Jul	11.1	24-Aug	19.0
10-Jul	9.7	25-Aug	17.6
11-Jul	16.4	26-Aug	15.4
12-Jul	21.5	27-Aug	12.6
13-Jul	RC	28-Aug	12.1
14-Jul	11.7	29-Aug	10.1
15-Jul	18.9	30-Aug	17.2
16-Jul	RC	31-Aug	19.9
17-Jul	RC	1-Sep	19.4
18-Jul	12.8	2-Sep	18.2
19-Jul	6.2	3-Sep	24.0
20-Jul	20.1	4-Sep	15.4
21-Jul	RC	5-Sep	12.4
22-Jul	16.9	6-Sep	12.5
23-Jul	12.8	7-Sep	15.8
24-Jul	7.9	8-Sep	23.4
25-Jul	15.7	9-Sep	11.5
26-Jul	24.9	10-Sep	6.0
27-Jul	22.2	11-Sep	11.8
28-Jul	17.5	12-Sep	10.7
29-Jul	19.1	13-Sep	7.6
30-Jul	21.1	14-Sep	7.5
31-Jul	18.0	15-Sep	7.1
1-Aug	16.3	16-Sep	7.7
2-Aug	19.3	17-Sep	11.3
3-Aug	17.9	18-Sep	16.8
4-Aug	25.1	19-Sep	14.8
5-Aug	RC	20-Sep	8.0
6-Aug	19.1	21-Sep	10.8
7-Aug	14.0	22-Sep	14.5
8-Aug	10.8	23-Sep	21.2
9-Aug	15.0	24-Sep	8.6
10-Aug	21.7	25-Sep	1.2
11-Aug	14.3	26-Sep	16.0
12-Aug	14.7	27-Sep	12.1
13-Aug	13.0	28-Sep	18.0
14-Aug	13.5	29-Sep	17.8
15-Aug	17.5	30-Sep	16.4
Seasonal / Quarterly Maximum			25.1

Season / Quarter 4			
Date	Conc.	Date	Conc.
1-Oct	12.3	16-Nov	4.6
2-Oct	8.2	17-Nov	7.8
3-Oct	12.3	18-Nov	4.4
4-Oct	19.5	19-Nov	8.2
5-Oct	23.7	20-Nov	11.1
6-Oct	19.8	21-Nov	5.3
7-Oct	21.7	22-Nov	8.9
8-Oct	12.2	23-Nov	14.0
9-Oct	5.1	24-Nov	12.7
10-Oct	10.2	25-Nov	9.7
11-Oct	10.7	26-Nov	12.8
12-Oct	5.6	27-Nov	16.6
13-Oct	5.9	28-Nov	17.2
14-Oct	9.7	29-Nov	16.6
15-Oct	12.8	30-Nov	4.5
16-Oct	16.4	1-Dec	7.5
17-Oct	12.0	2-Dec	10.6
18-Oct	7.9	3-Dec	16.7
19-Oct	6.6	4-Dec	12.5
20-Oct	8.1	5-Dec	7.3
21-Oct	12.2	6-Dec	10.4
22-Oct	4.6	7-Dec	13.4
23-Oct	6.1	8-Dec	10.5
24-Oct	4.6	9-Dec	9.3
25-Oct	4.5	10-Dec	6.5
26-Oct	10.5	11-Dec	3.0
27-Oct	6.4	12-Dec	3.5
28-Oct	4.6	13-Dec	10.2
29-Oct	5.6	14-Dec	17.6
30-Oct	7.6	15-Dec	12.4
31-Oct	11.2	16-Dec	9.7
1-Nov	16.2	17-Dec	7.0
2-Nov	17.3	18-Dec	7.9
3-Nov	18.3	19-Dec	6.9
4-Nov	8.9	20-Dec	8.1
5-Nov	5.8	21-Dec	4.9
6-Nov	8.6	22-Dec	7.7
7-Nov	15.0	23-Dec	7.7
8-Nov	8.3	24-Dec	10.5
9-Nov	10.0	25-Dec	6.5
10-Nov	12.8	26-Dec	7.6
11-Nov	11.8	27-Dec	13.3
12-Nov	14.8	28-Dec	6.4
13-Nov	14.5	29-Dec	3.7
14-Nov	7.7	30-Dec	4.7
15-Nov	3.6	31-Dec	4.4
Seasonal / Quarterly Maximum			23.7

Seasonal / Quarterly Maximum Concentration
RC = Above 98th Percentile and Removed from Consideration

Table D-4. Resulting Average of Seasonal (or Quarterly) Maximums for Inclusion into AERMOD

Seasonal / Quarterly Average Highest Monitored Concentration

(From Annual Datasets Equal To and Less Than the 98th Percentile)

	Q1	Q2	Q3	Q4
2008	22.5	23.0	25.1	23.7
2009	21.1	20.7	21.2	19.8
2010	20.7	22.6	23.5	20.7
Average	**21.433**	**22.100**	**23.267**	**21.400**

(Note, the complete datasets for 2009 and 2010 are not shown in Appendix D but would follow the same steps as for 2008)

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